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Figure 1: Vicinity Map

## SECTION 1 - PROJECT SUMMARY

The Beckley Z-Way design study includes developing feasible alternates along four segments of roadway in Raleigh County, WV. The alternates will be further studied through the NEPA process with final alternates being selected for future design and construction projects. The segment numbering methodology maintains the segments identified in the original traffic study (Phase I). Three of the four segments involve potential improvements to the existing roadway. Segment 8 will be a new facility which connects US 19 directly to l-64. The construction of this segment helps alleviate congestion on the existing network by providing a convenient access to the City of Beckley and the commercial areas along Eisenhower and Robert C. Byrd Drives as well as the East Beckley Bypass. This study was developed assuming a connection from Shady Springs to a new interchange with I-64. An interstate system access change study may be required for the Segment 8 alternate. See Figure 1 for the project Vicinity Map.

## Segment 1 (US 19 from WV 3 to WV 307)

Segment 1 starts in the Shady Springs area at the intersection of WV 3 and ends near WV 307 (Airport Road) in Beaver. A traffic study was conducted to determine the most feasible configuration for US 19. The analysis shows that a 3-lane typical section, two through lanes (one lane in each direction) and a continuous center turn lane, is appropriate. The speed limit for this segment is at 40 mph from the US 19/WV 3 Intersection north to Lewis Drive just to the southeast of Daniels. The speed limit varies from 40 to 50 mph along the alignment. The speed limit is 40 mph in the vicinity of the WV 3 intersection and in the vicinity of the WV 307 intersection. The intersections of US 19 with WV 3 and WV 307 are currently signalized.

The design criterion on US 19 is based upon Urban Arterial Functional Classification, with a minimum of 45 mph design speed for Alternates 3 through 6. Alternate 2 widens the existing roadway so no changes were made to the existing horizontal and vertical alignments. The typical section includes 12 -foot wide through lanes and a 14 -foot wide continuous center turn lane. A summary of the design criteria is shown in the appendix.

There are six potential alternates for widening US 19 (Segment 1):

1. No Build;
2. Widening along both sides using the existing alignment. (Less than 45 mph design speed);
3. Widening and reducing the sharpness of the existing horizontal and vertical curves;
4. Widening on the sides opposite of alternate 3;
5. Same alignment as Alternate \#3, but uses a curb and gutter typical roadway section;
6. Same alignment as Alternate \#4, but uses a curb and gutter typical roadway section.

To achieve the 45 mph design speed, vertical alignment adjustments were made to Alternates 3 through 6. If any of alternates 3 through 6 are selected to proceed into the design phase, special attention to the temporary traffic control design is required in the areas of vertical alignment adjustments.

Each of these alternates will be evaluated for cost and environmental impacts with a preferred option selected for final design. Extensive utility relocations will be required for Alternatives 2 through 6. A new signal will be added at the US 19 and Segment 8 intersection.


Figure 2: View Looking North on US 19

The land use along US 19 includes numerous commercial properties and a high demand for access. The three-lane typical section will provide better traffic flow by separating the left turning traffic from the through traffic. Table 1 shows the accident rates for various segments along US19. Table 2 shows the accident rates at selected intersections. The accident statistics show a predominance (60\%) of rear-end type collisions all along this roadway segment. Another $15 \%$ of the accidents were either Access Conflict or Left turn. A three lane typical section reduces these accidents by separating left-turning traffic from the traffic flow. The highest concentration of accidents occurs on the section of US 19 between C\&O Dam Road and Old Crow Road. The higher than average accident rate consists mostly of rear end type collisions. This area has closely spaced intersections and driveways along with a $6 \%$ grade and deficient sag vertical curve. The addition of the continuous left turn lane and increasing the sag vertical curve to a 45 mph design speed in alternates 3 thru 6 will help reduce these accidents. Access management also would help eliminate the turning conflicts. The US 19/WV3 intersection has the highest accident rate. However, the accident data was collected prior to the installation of a signal at this intersection. The signal should decrease the accident rate.

Table 1: US 19 Segment Accident Summary

| Route Name | County | Start | Stop | $\begin{gathered} \text { Milepost } \\ \text { (Start) } \end{gathered}$ | $\begin{gathered} \text { Milepost } \\ \text { (Stop) } \end{gathered}$ | $\begin{gathered} \text { Distance } \\ (\text { miles }) \end{gathered}$ | $\begin{gathered} \text { Number } \\ \text { of } \\ \text { occidents } \end{gathered}$ | $\begin{gathered} \text { Time } \\ \text { Period } \\ \text { (yrs.) } \end{gathered}$ | Volume (AADT) | $\begin{gathered} \text { (section) } \end{gathered}$ | $\begin{gathered} \text { Versus } \\ \text { Average } \\ \text { (\%) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| US 19 | Raleigh | WV3 | $4^{\text {TH }}$ Street $/$ Hampton Drive | 8.78 | 9.78 | 1.00 | 14 | 3.5 | 15,650 | 70.0 | 34.0\% |
| US 19 | Raleigh | $4^{\text {TH }}$ Street / Hampton Drive | $\begin{gathered} \text { WV } 307 \\ \text { Grandview Road } \end{gathered}$ | 9.78 | 10.45 | 0.67 | 23 | 3.5 | 17,200 | 156.2 | 75.8\% |
| US 19 | Raleigh | $\begin{gathered} \text { WV } 307 \\ \text { Grandview Road } \end{gathered}$ | CR 19/15 4-H Lake Road | 10.45 | 11.56 | 1.11 | 33 | 3.5 | 15,850 | 146.8 | 71.3\% |
| US 19 | Raleigh | CR 19/15 4-H Lake Road | $\begin{gathered} \text { CR } 19 / 13 \mathrm{C} \text { \& O O } \\ \text { Dam Road } \end{gathered}$ | 11.56 | 12.17 | 0.61 | 17 | 35. | 19,265 | 113.2 | 55.0\% |
| US 19 | Raleigh | CR 19/13 C \& O Dam Road | $\begin{gathered} \hline \text { CR 119/36 } \\ \text { Old Crow Road } \end{gathered}$ | 12.17 | 12.49 | 0.32 | 35 | 3.5 | 18,375 | 465.9 | 226.2\% |
| US 19 | Raleigh | $\begin{gathered} \hline \text { CR 119/36 } \\ \text { Old Crow Road } \end{gathered}$ | $\begin{gathered} \text { WV } 307 \\ \text { Airport Road } \end{gathered}$ | 12.49 | 12.90 | 0.41 | 25 | 3.5 | 21,600 | 221.0 | 107.3\% |

Table 2: US 19 Intersection Accident Summary

| Route Name | Real <br> Milepost | County | Intersection | Number of <br> Accidents | Time Period <br> (yrs.) | Intersection <br> DEV | R(spot) | Route Name |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WV 3 | 8.78 | Raleigh | WV 3 | 33 | 3.5 | 14,700 | 1.76 |  |
| WV 307 | 10.45 | Raleigh | WV 307 | 6 | 3.5 | 14,850 | 0.32 | Rite Aid/ IGA Parking |
| CR 19/15 4-H Lake Road | 11.56 | Raleigh | CR 19/15 <br> (4-H Lake Road) | 12 | 3.5 | 16,850 | 0.56 | CR 19/37 (Dan Mont Vista) |
| CR 19/13 C \& O Dam Road | 12.17 | Raleigh | CR 19/13 | 14 | 3.5 | 14,800 | 0.74 | CR 19/99 (Price Street) |
| WV 307 | 12.90 | Raleigh | WV 307 <br> (Airport Road) | 25 | 3.5 | 21,200 | 0.92 | Walgreens / KFC Parking |

## Segment 2 WV 307 from US 19 to l-64

This segment of roadway has existing 10 foot lanes, little development, and a rural character. The 10 -foot travel lanes do not meet lane width requirements for a roadway with an AADT>2000 vpd. Therefore this roadway will be widened to have 12 -foot wide travel lanes with 8 -foot wide shoulders. These wider travel lanes and shoulders helps increase the safety and increase capacity by reducing side friction. The horizontal and vertical alignments will remain intact. The speed limit for this segment is 45 mph .

There are two potential alternates for widening WV 307:

1. No Build;
2. Widen the typical section to 12 -foot wide lanes with 8 -foot wide shoulders. Six feet of the 8 -foot wide shoulder should be paved.

The traffic demand for this segment will be reduced once Segment 8 is constructed. This lower demand will reduce the need for a continuous left turn lane. Additionally, there are few driveways and intersections within the middle of the alignment, which reduces the need for a turn lane. On this segment, the accident rate is lower than the statewide average. The accidents were concentrated at the two ends of the segment. The accidents were located within a quarter-mile of the US 19 Intersection and at the CR 9/9 intersection. Only two accidents occurred along the remaining segment length.

Table 3: WV 307 Segment Accident Summary

| Route Name | Real <br> Milepost | County | Intersection | Number of <br> Accidents | Time Period <br> (yrs.) | Intersection <br> DEV | R(spot) | Route Name |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WV 307 Airport Road | 1.32 | Raleigh | CR $9 / 9$ | 6 | 3.5 | 8,250 | 0.57 | Orchard Hill Road |

Table 4: WV 307 Intersection Accident Summary

| Route Name | County | Start | Stop | $\underset{\substack{\text { Milepost } \\ \text { (Start) }}}{\text { Stand }}$ | $\begin{gathered} \text { Milepost } \\ \text { (Stop) } \end{gathered}$ | $\begin{gathered} \text { Distance } \\ \text { (miles) } \end{gathered}$ | Number of Accidents | $\underset{\substack{\text { Time } \\ \text { Period } \\ \text { (yrs.) }}}{ }$ | $\begin{aligned} & \text { Volume } \\ & \text { (AADT) } \end{aligned}$ | $\underset{\text { (section) }}{\text { R }}$ | $\begin{gathered} \text { Versus } \\ \text { Average } \\ \text { (\%) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WV 307 | Raleigh | US 19 | CR 9/9 Orchard Hill Road | 0.10 | 1.32 | 1.22 | 27 | 3.5 | 12,950 | 133.8 | 64.9\% |

## Segment 7 (Airport Road (CR 9/9) from l-64 to the Beckley - Raleigh County <br> Airport)

This segment of roadway has existing 10 foot lanes, little development, and a rural character. The 10 -foot travel lanes do not meet lane width requirements for a roadway with an AADT>2000 vpd. Therefore this roadway will be widened to have 12 -foot wide travel lanes with 8 -foot wide shoulders. These wider travel lanes and shoulders helps increase the safety and increases capacity by reducing side friction. The speed limit for segment 7 is 50 mph .

1. No Build;
2. Widening to 12 -foot wide lanes and 6 -foot wide paved shoulders and an 8 -foot wide shoulders.

A continuous center turn lane option is not supported by the traffic volumes. Additionally, the driveways are located at a reasonable spacing, which diminishes the effect of the turn lane.

The accident rate for Airport Road is well below the statewide rate for county roads. However, there were 11 accidents over the 3.5 year period, which occurred near the entrance of the Mine Health and Safety Academy. The accidents were classified as single vehicle for 6 of the accidents. This section of the alignment has several horizontal and vertical curves. The horizontal curves have a minimum design speed of 45 mph , whereas one of the vertical curves has a design speed of 25 mph . The milepost location of these vertical curves does not correspond to the accident locations. The vertical curve in the vicinity of the Academy is 50 mph .

Table 5: CR 9/9 Segment Accident Summary

| Route | County | Start | Stop | $\begin{gathered} \text { Milepost } \\ \text { (Start) } \end{gathered}$ | $\begin{aligned} & \text { Milepost } \\ & \text { (Stop) } \end{aligned}$ | $\begin{gathered} \text { Distance } \\ \text { (miles) } \end{gathered}$ | $\begin{gathered} \text { Number } \\ \text { of } \\ \text { Accidents } \end{gathered}$ | $\begin{gathered} \text { Time } \\ \begin{array}{c} \text { Period } \\ \text { (yrs.) } \end{array} \end{gathered}$ | Volume (AADT) | $\underset{\text { (section) }}{\text { R }}$ | $\begin{gathered} \text { Versus } \\ \text { Average } \\ (\%) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CR 9/9 Airport Road | Raleigh | WV 307 | Interstate 64 Interchange | 0.00 | 0.81 | 0.81 | 6 | 3.5 | 9,350 | 62.0 | 19.3\% |
| CR 9/9 Airport Road | Raleigh | Interstate 64 Interchange | Raleigh County Airport | 0.81 | 1.81 | 1.00 | 16 | 3.5 | 8,550 | 146.5 | 45.5\% |

Table 6: CR 9/9 Intersection Accident Summary

| Route Name | Real Milepost | County | Intersection | Number of <br> Accidents | Time Period <br> (yrs.) | Intersection <br> DEV | R(spot) | Route Name |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CR $9 / 9$ | 0.11 to 0.37 | Raleigh | Interstate 64 Interchange <br> Ramps (EB $\&$ WB) | 5 | 3.5 | 9,320 | 0.42 | Airport Road |

## Segment 8 (Eisenhower Drive Extension from US 19 to I-64)

This is new roadway from just southeast of the WV 307 intersection up to the existing I-64 interchange. This roadway segment will include a crossing of Little Beaver Creek. The traffic demand model showed an increase of the level of service on the existing roadways with the inclusion of this segment. This segment has a design speed of 45 mph . The typical section for this roadway will be a three lane, with a continuous center turn lane. An access modification study will be required for the I-64 interchange at milepost 124.

There are three potential alternates for the Eisenhower extension. The alignment studied for alternate 2 is closer to US 19 and does not allow a suitable connection to US 19. Both versions of Alternate 1 provide a feasible connection to US 19

1. Alignment Alternate 1-Grade separated intersection with WV 307
2. Alignment Alternate 1 - At-grade intersection with WV 307.
3. Alignment Alternate 2 - Grade separated intersection with 307, with different starting point.

The I-64 Interchange will need to be modified to accommodate the southern access. This study presents a feasible option which will include;

- Providing I-64 eastbound off-ramp left turn lane and providing two southbound left turn lanes.
- Signalizing the eastbound ramps.
- Providing two receiving lanes on I-64 on-ramp.
- Signalizing the I-64 westbound ramps to accommodate northbound left turn and westbound left turn traffic.


## Traffic Analysis Recommendations

Based on the analysis results associated with the construction of the Beckley Z-Way, the following roadway improvements should also be considered.

## US 19 (South of East Beckley Bypass Connector)

- For unsignalized intersections with approximately 50 or more right turning vehicles for the mainline, right turn lanes should be considered. In most cases 100 feet of storage should be adequate.


## US 19 Unsignalized Intersections (South of East Beckley Bypass Connector)

- As needed, signalize if and when volumes meet signal warrants. The US 19 Connector intersection with the Bypass Extension, the at-grade intersection with WV 307 and the Bypass Extension and the I-64 Interchange ramp intersections would likely meet signal warrants


## US 19/East Beckley Bypass Connector Intersection

- Provide separate eastbound left turn lane and channelized right turn lane with an added lane southbound on US 19. The additional southbound lane can be dropped prior to CR 119/36 (Old Crow Road). Provide two northbound left turn lanes on US 19. The additional lane may be dropped prior to Trenton Lane.


## East Beckley Bypass and Jersey Avenue

- Increase northbound left turn storage length as needed by restriping existing Two-Way Left Turn Lane


## Incident Management

Reducing traffic congestion and improving roadway safety are high priorities. Traffic incidents are a major source of both highway congestion and safety problems. Incidents are estimated to cause approximately half of all traffic delay. Crashes that result from other incidents account for approximately 16 percent of all crashes and cause 18 percent of freeway deaths. For these reasons, FHWA strongly endorses the establishment and use of good traffic incident management. Effective transportation system management and operations depends on the aggressive management of temporary disruptions (caused by traffic incidents, work zones, weather, special events, etc.) in order to reduce the consequences of these disruptions and return the system to full capacity. The FHWA publication "Simplified Guide to the Incident Command System for TRANSPORTATION PROFESSIONALS, February 2006" outlines procedures and stakeholders for implementing a workable incident management plan and an incident command system.


Figure 3: View Looking North on WV 307


Figure 4: Segment Location Map

## SECTION II - GEOTECHNICAL OVERVIEW

The purpose of this project is to improve accessibility through an area known as the Beckley ZWay and to route more traffic through Beckley, West Virginia. The study limits for the Beckley ZWay are shown on Figure 6. The corridor improvements are anticipated to include the following:

- widening along approximately 4.25 miles of US 19 ;
- widening about 1.5 miles of Airport Road to the north of I-64;
- widening about 1 mile of WV 307 to the south of I-64; and
- about 1.5 miles of new alignment from I-64 at Exit 124 to the south to US 19.


## Objective

The primary objective of this geotechnical overview study was to review readily available site data and to identify potential geotechnical and/or geological features that may impact the planning, design, and/or construction of new or modified roadways in the corridor.

## Site Conditions

A site visit has not been made by CDM Smith's geotechnical personnel. However, a review of readily available aerial mapping, topographic mapping, and site photos has been made

The topography of the study area may be characterized by rugged terrain where wooded hills typically overlook relatively narrow lowlands occupied by rivers, creeks and branches. Several branches or creeks extend under existing roadways within the study area. The elevations along most of the affected alignments range between about $+2,200$ feet near the intersection of US 19 and WV 307 and about $+2,700$ feet near the southern extent of the study area.

From this data review effort, it appears that a majority of the properties adjacent to US 19, which is primarily a two-lane facility within the study limits, are either residential or commercial. Overhead
power lines typically parallel one or both sides of the roadway. Existing cuts and fills along US 19 are unknown; however, thicknesses less than 10 feet appear common as the topography along the roadway often appears to be gently to moderately rolling. Some notable exceptions to this includes several cut slopes in rock and several retaining walls apparently built off the roadway shoulder to accommodate the West Virginia Department of Highways right of way. Several box culverts provide passage over Sand Branch, Beaver Creek and Little Beaver Creek. A bridge is also present on US 19 to allow access over WV 307.

The land use along existing WV 307, which is a two lane facility, was observed to be a mix of residential, commercial and undeveloped woodlands. This section of roadway from about US 19 to just west of $\mathrm{I}-64$ at Exit 125B is winding and rises steadily to the north. Several large slopes, especially near the roadway's horizontal curves, were observed. A sizable rock cut slope is present on the uphill side of the section of greatest horizontal curvature.

Airport Road extends north from I-64 at Exit 125B to Raleigh County Airport. Based on aerial mapping, this area is mostly undeveloped with some wooded areas. The ground surface elevations along this roadway and adjacent properties are about $+2,500$ feet and are relatively flat.

The proposed new roadway from US 19 and extending northwest towards I-64 at Exit 124 is mostly wooded and presently undeveloped although a portion of this area has been subject to past coal mining activities as described further below. It is anticipated that a new bridge over Beaver Creek may be required. The relief along this future roadway corridor is quite rolling with ground surface elevations increasing from south to north.

## Geologic Overview

Based on the published geologic mapping, the study area is located in the Allegheny Plateau, which is comprised of Pennsylvanian and Permian strata containing minable coal beds. The rock strata in this area are likely comprised of cyclic sequences of sandstone, shale, clay, coal and limestone. No faults were identified within the limits of the corridor study.

It is anticipated that the study area has a very low karst potential (i.e., karst features are rare or absent). However, detailed geologic quadrangles containing the study area have not been reviewed

Based on materials reviewed for this study, springs have not been identified within the study area Regardless, it is possible that some locations contain wet weather springs.


Figure 5: MSHA Entrance


Figure 6: Geological Feature Map

## SECTION III - ENVIRONMENTAL OVERVIEW

The Beckley Z-Way design study includes developing feasible alternates along four segments of roadway in Raleigh County, WV. See Figure 4: Segment Location Map. The alternates will be further studied through the National Environmental Policy Act (NEPA) process with a recommended alternate being selected for future design and construction projects

This Environmental Overview is a level of documentation that identifies environmentally sensitive areas within the project area to aid in planning activities. This type of documentation provides a framework to identify environmentally sensitive areas and develop a scope to assist with the NEPA process. No in-depth research is warranted at this stage of project development. A field visit was conducted in July 2011 to view the project area. The primary area of concern will be focused on 250 feet of either side of the existing centerline for a tota corridor of 500 feet as shown in Figure 9. This study corridor is typically referred to as Area of Potential Effect (APE).

Data was gathered using the Geographic Names Information System (GNIS) for all known places, features, and areas in the United States that are identified by a proper name. Each feature is located by state, county, and geographic coordinates; and referenced to Statewide Mapping Aerials.


Figure 7: US 19 North of WV 3


Figure 8: WV 307 North of US 19


Figure 9: Area of Potential Effect Map

## I. Environmental Inventory

## A. Historic and Archaeological Resources

The National Register of Historic Places is a listing of historic and archaeological resources. Historic and archaeological resources can include districts, archaeological sites, buildings, structures and objects. Listed resources are generally at least fifty years old and possess historic and culture significance and integrity. Archival research at the West Virginia Division of Culture and History (WVDCH), Historic Preservation Unit was not conducted at this time. As this project is advanced through the development process, a thorough investigation into cultural resources will be completed at the WVDCH and the West Virginia State Historic Preservation Office (WVSHPO) utilizing their expansive reserves of documents, mapping, reports and files.


Figure 10: Little Beaver Dam

## Archaeological Resources

The likelihood of archaeological resources in this area is small due to previous disturbance resulting from the construction of I-64, US 19 and adjacent industrial commercial and
residential development. Any previous deposits of archaeological resources have likely been impacted or removed by construction.

## Historic Resources

A search for National Register of Historic Places listed properties was conducted by utilizing Historic West Virginia, The National Register of Historic Places, published by the WVDCH. Within the entirety of Raleigh County there are eight National Register of Historic listings.

| Community | Name of Listing | Location |
| :--- | :--- | :--- |
| Beckley | Beckley Courthouse Square Historic District | Prince, Kanawha, Church, Lebanon, <br> Howe, McCreery and Earwood <br> Sreest and Alaska and First <br> Avenues |
| Beckley | Beckley Feed and Hardware Company | Prince Street |
| Crow | Little Beaver Dam | Little Beaver Creek |
| Beckley | Phillips-Sprague Mine | Beckley Exhibition Coal Mine |
| Sandstone | St. Coleman's Roman Catholic Church and Cemetery | New River |
| Hinton | $\underline{\text { Trump-Lilly Farmstead }}$ |  |
| Sophia | Sophia Historic District | Laurel Terrace |
| Beckley | $\underline{\text { Wildwood }}$ |  |

Figure 11: National Register Listings in Raleigh County
There are no properties listed on the National Register of Historic Places within or near the project area. A site visit didn't identify any potential historic sites within the APE. An historic survey will be conducted during the scoping of the NEPA process to further determine if the project will impact potential historic structures.

## B. Rare and Threatened Species

The West Virginia Department of Natural Resources (WVDNR), Wildlife Resources Section will be contacted to obtain information on any rare, threatened or endangered species (RTE) within the project area of potential effect. There have been several Indiana Bat Mist Net Surveys conducted to the north of this project. As of this study, there have been no bats found. During the next phase of the project, the US Fish and Wildlife service will additionally be contacted concerning potential RTE species.

## C. Cemeteries and Burial Grounds

A query of the GNIS mapping database and examination of USGS topographical maps were conducted to identify locations of cemeteries and burial grounds within the project area. No cemeteries or burial grounds were found to be located within the project APE utilizing these resources. Further investigation into the cemeteries will be conducted during the course of this study.

## D. Hazardous Waste, Underground Storage Tanks, Superfund Sites

Correspondence with the West Virginia Department of Environmental Protection will be initiated for information on any underground storage tanks, superfund sites or hazardous waste sites. Potential Sites Identified during a field investigation are listed.

| Alternate | Station | Description |
| :---: | :---: | :---: |
| 1 | RT $1014+00$ US 19 | Active Service Station |
| 1 | LT 1025+50 US 19 | Historic Service Station |
| 1 | RT 1037+00 US 19 | Historic Service Station |
| 1 | RT 1054+00 US 19 | Active Service Station |
| 1 | RT 1109+00 US 19 | Active Service Station |
| 1 | LT 1127+00 US 19 | Active Service Station |
| 1 | LT 1194+00 US 19 | Active Service Station |
| 1 | LT 1223+50 US 19 | Dry Cleaners |
| 1 | LT 2004+00 WV 307 | Active Service Station |
| 1 | LT 2100+00 WV 307 | Active Service Station |

Figure 12: Potentially Contaminated Soil Locations


Figure 13: Citgo Station at US 19 and WV 3 Intersection
In addition to correspondence with the WVDEP, the United States Environmental Protection Agency (www.epa.gov) website was consulted. This website revealed a total of four Superfund sites are located in Raleigh County. These sites are listed below in Figure 14.

| Site Name | EPA ID | NPL Status | City | County | Zip |
| :--- | :--- | :---: | :--- | :--- | :---: |
| Glen Morgan Drum Dump | WVD988767455 | Non | Glen Morgan | Raleigh | 25847 |
| Hoffman Metal Removal | WVN000305643 | Non | Mabscott | Raleigh | 25827 |
| Holly Hill Subdivision | WV0001095421 | Non | Fairdale | Raleigh | 25839 |
| Sophia Battery Dump | WVSFN0305434 | Non | Sophia | Raleigh | 25921 |

Figure 14: EPA listed Superfund Sites
More detailed investigations will be conducted when alternates have been chosen. These investigations will determine if the sites listed in Figure 14 will be impacted. Also available
on the EPA website are Comprehensive Environmental Response, Compensation and Liability Information System (CERCLIS) Hazardous Waste Sites listings. Within Raleigh County, federally listed CERCLIS sites are shown in Figure 15. The exact locations of these sites are not known. General locations were provided by the EPA website, however their specific locations were not given and cannot be shown on project mapping due to the possibility of misidentification or mislabeling of a property. Upon establishment of alternatives and determination of a preferred alignment, further investigations to determine precise locations of the CERCLIS sites will need to be conducted

| EPA ID | Site Name | City | County | State | Non-NPL <br> Status Code | Non-NPL <br> Status Date | NPL Status <br> Code |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WVD016138760 | Barker Junk Co., <br> Inc. | Mabscott | Raleigh | WV | OS | $7 / 2 / 2002$ | N |
| WVSFN0305434 | Sophia Battery <br> Dump | Sophia | Raleigh | WV | RW | $4 / 24 / 2008$ | N |
| WV0002326486 | Walton Mtn. Road <br> Home | Rhodell | Raleigh | WV | RO | $1 / 12 / 2000$ | N |

Figure 15: CERCLIS Sites in Raleigh County

## E. Wetlands

Within the study area, wetlands are present in areas where existing roadways traverse streams or rivers. United States Department of the Interior, National Wetland Inventory Maps has been reviewed for any locations of previously identified wetlands within the project area. The wetland boundaries are shown in Figure 9. The primary wetland area relates to Little Beaver Creek. The Z-Way project crosses the floodplain near the intersection of WV 307 and US 19. The other wetlands will be classified as the project progresses. Depending on the preferred alternate for the project, further investigations into registered wetlands within the APE will be warranted.

## F. Air Quality \& Noise

At this level of documentation air and noise monitoring is not required. Upon determination of a preferred alternate, these areas of concern will be examined in more detail.

## G. Groundwater Resources \& Existing Well Records

The underlying groundwater aquifer of the Beckley area is the New River Formation of the Pottsville Group, which is of Pennsylvanian Age. This geologic formation consists of thick layers of sandstone separated by thinner beds of shale, siltstone, and coal. Primary permeability, the movement of water directly through the pore spaces of rocks, is low throughout the area. Therefore, movement of groundwater is mostly by secondary permeability through the fractures, joints, and separations of the geologic formation. Wells that penetrate these few fractures generally have yields less than 1 gallon per minute per foot of drawdown. Yields are highly variable depending on the number of water-bearing openings penetrated by the well. In the Beckley area, this variability can result in wells located near each other having vastly different yields. Additionally, the United States Geological Survey (USGS) describes groundwater discharge to the many small streams in this area as insufficient to maintain flow during drought periods.

The State of West Virginia Department of Health and Human Resources, Bureau of Health reported that the Beckley Water Company provides public water for the entire study area, and their water sources are from one surface water plant and one groundwater plant. The surface water plant is located to the east of the project area at Glade Creek Reservoir, and the groundwater plant is located outside of the study area at Sweeneysburg. The only items within the study area related to public water supply are distribution lines and tanks. The Beckley-Raleigh County Board of Health reported that to their knowledge, there are no private water wells within the study area. The State of West Virginia Division of Environmental Protection, Office of Water Resources (WVDEP-OWR) stated that state law does not protect aquifer recharge areas.

## H. Other State and Federal Actions Required

Other federal and state agency actions may be required when it has been determined what the preferred alternate will be. At this point, coordination with these agencies is not warranted, as this level of investigation is an overview and may include:

- Section 404 permit approval by the U.S. Army Corps of Engineers (Huntington District) for stream and wetland encroachment required for roadway construction,
- Section 401 Water Quality Certification from the West Virginia Department of Environmental Protection,
- The US Fish and Wildlife Service and Marine Fisheries Service,
- National Pollution Discharge Elimination System (NPDES) Permit from the West Virginia Department of Environmental Protection,
- Contact any public land holders in the area and,
- Federal Emergency Management Agency (FEMA) for permits and coordination,
- Public Land Corporation easements.


## II. Socioeconomic Impacts

## A. Social

The City of Beckley is centrally located in southern West Virginia. It is situated about 60 miles ( 96 km ) southeast of Charleston, West Virginia and 45 miles ( 72 km ) north of Bluefield, West Virginia. Beckley serves as the seat of government for Raleigh County and is its largest municipality. Beckley is the commercial center of the rural, coal mining area of southern West Virginia. Several counties border Raleigh County: Boone and Wyoming on the west, Kanawha and Fayette on the north, Summers on the east and Mercer on the south. The New River shapes the eastern edge of the county.

Several major highways serve the Beckley and Raleigh County area. These highways include Interstate 77 (West Virginia Turnpike), Interstate 64 (I-64), and US Route 19 (Appalachian Corridor L).
The subject project is limited to a 250 -foot wide buffer zone area on either side of the existing roadways. By utilizing the GNIS maps and the project field visit, it has been determined that there are no schools, libraries, parks or recreational facilities located within
the APE. Also established was the lack of public services within the APE, such as emergency services, waste disposal facilities and other similar services. Industrial/commercial and residential are the two primary land uses within the project area.

Further correspondence with the Natural Resources Conservation Service will determine if there are Prime and Statewide Important Farmlands present in the project area.

Travel patterns will be modified and improved, because this project provides an additional access to I-64 and a connection from the Shady Springs area to the downtown Beckley area. Additionally, because the widening of the roadway is located at or near its current location, pedestrian and/or bicycle facilities will be improved by the construction of paved shoulders.

Effects on social groups will be minimal due to this project's location with respect to the location of the existing roadway, the amount of roadway being affected, and the limits of the project. Since this project is along an existing interstate, no impact will occur to social groups

There will be no 4(f) impacts associated with this project. Any potential 4(f) properties are outside the APE of this project. Section 4(f) of the Department of Transportation Act of 1966 (49 USC 1653 (f)), that declares it a national policy that special effort be made to preserve the natural beauty of the countryside, public park and recreation lands, wildlife and waterfowl refuges, and historic sites.

In accordance with the Presidential Executive Order on Environmental Justice, this project will be analyzed to determine the likelihood of impacts to minorities or disadvantaged populations. The project area may involve substantial relocations depending on the preferred alternate. Nevertheless, it is unlikely that any alignment chosen would have a disproportionate impact on environmental justice populations


Figure 16: Farmlands Within Project Area

| MAP LEGEND |  |  |  |  |  | MAP INFORMATION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Area of In <br> Soils | terest (AOI) <br> Area of Interest (AOI) | $\square$ | Prime farmland if subsoiled, completely removing the root iting soil laye | $\cong$ | Major Roads | Map Scale: 1:30,200 if printed on $B$ size ( $11^{\prime \prime} \times 17^{\prime \prime}$ ) sheet. <br> The soil surveys that comprise your AOI were mapped at 1:24,000. |
| $\square$ | Soil Map Units ings |  | Prime farmland if irrigated and the product of I (soil erodibility) $\times \mathrm{C}$ (climate |  |  | Please rely on the bar scale on each map sheet for accurate map measurements. |
| $\begin{aligned} & \square \\ & \square \end{aligned}$ | Not prime farmland <br> All areas are prime farmland | $\square$ | factor) does notexceed 60 Prime farmland if ifigated salts and sodium salts and sodium |  |  | Source of Map: Natural Resources Conservation Service Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov Coordinate System: UTM Zone 17N NAD83 |
| $\square$ | Prime farmland if drained <br> Prime farmland if |  | Famland of statewide imporance |  |  | This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. |
| $\square$ | proiected from flooding or not treauenty flooded during the growing season Prime farmland if irrigated | $\begin{aligned} & \square \\ & \square \end{aligned}$ | Farmland of local importance Farmland of unique importance |  |  | Soil Survey Area: Fayette and Raleigh Counties Area, West Virginia <br> Survey Area Data: Version 3, Mar 9, 2011 |
| $\square$ | Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season $\qquad$ |  | Not rated or not available <br> atures <br> Cities <br> ures |  |  | Date(s) aerial images were photographed: 8/25/2007 <br> The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. |
| $\square$ | Prime farmland if irrigated and drained <br> Prime farmland if irrigated and either protected from flooding or not frequently flooded during the growing season season |  | Streams and Canals <br> tion <br> Rails <br> Interstate Highways <br> US Routes |  |  |  |

Figure 17: Farmland Legends

## B. Economic

Beckley is the most populated municipality within Raleigh County. For decades Beckley and Raleigh County were known as an area of major coal production. While the coal mining industry is no longer at its peak, the city has grown into a regional commercial center providing wholesale, retail and services to the surrounding counties in southern West Virginia.

The economy of the project area should not be adversely impacted by the widening of US
19. There will be some temporary impacts caused by business relocations and during
construction. There are numerous commercial properties which lie along US 19 that could be impacted depending on which alternate is chosen. The economy should not be detrimentally affected by the implementation of the project.


Figure 18: Example of existing service related industries.

## REFERENCES

## Kozar, Mark D. and Melvin V. Mathes

2001 Aquifer-Characteristics Data for West Virginia, Water-Resources Investigations Report 01-4036. United States Department of the Interior \& United States Geological Survey. Charleston, West Virginia.
West Virginia Division of Culture and History, State Historic Preservation Office
2011 Historic West Virginia, The National Register of Historic Places. Charleston, West Virginia.

## GIS DataDepot

2011 Wetlands and Deepwater Habitats Classification.
Online at http://www.gisdatadepot.com/readme/nwi/nwicodes.html (Accessed September 2011)

## NRCS

2011 Web Soil Survey.
Online at http://websoilsurvey.nrcs.usda.gov/app/ (Accessed October 2011)
Map WV
2011 WV Geologic and Economic Survey Interactive Mapping Portal Online at http://ims.wvgs.wvnet.edu/index.html (Accessed September 2011)
U.S. Department of Transportation, Federal Highway Administration

Simplified Guide to the Incident Command System for TRANSPORTATION PROFESSIONALS, February 2006

## Appendix A - Evaluation Matrices

Beckley Z-Way Alignment Alternative Evaluation/Cost Matrix - FINAL

| Impact Category |  | Alternative No. 1 | Alternative No. 2 | Alternative No. 3 | Alternative No. 4 | Alternative No. 5 | Alternative No. 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Engineering |  |  |  |  |  |  |  |
| Prelim. Length of US 19/WV3 Improvements | Feet | Existing Conditions | 23,000 | 23,000 | 23,000 | 23,000 | 23,000 |
|  | Miles | Existing Conditions | 4.36 | 4.36 | 4.36 | 4.36 | 4.36 |
| Roadway Configuration |  | Existing Conditions Average 2 (11' Lanes). Many areas have less than a 2 ' Shoulder | 2 (12' Lanes) $14^{\prime}$ Continuous Left Turn Lane 6' Paved Shoulders | 2 (12' Lanes) 14' Continuous Left Turn Lane 6' Paved Shoulders | 2 (12' Lanes) 14' Continuous Left Turn Lane 6' Paved Shoulders | 2 (12' Lanes) 14' Continuous Left Turn Lane 2' Gutter with Curb | 2 (12' Lanes) 14' Continuous Left Turn Lane 2' Gutter with Curb |
| Horizontal Geometry (Min Radius) |  | ${ }^{716}$ | $716^{\prime}$ | 822' | $8^{22}$ | 822' | 822' |
| Financial / Costs |  |  |  |  |  |  |  |
| Estimated Right of Way Acquisition Costs |  | \$0 | \$27,270,000 | \$24,770,000 | \$20,675,000 | \$25,050,000 | \$27,690,000 |
| Estimated Utility Relocation cost |  | \$0 | \$5,250,000 | \$5,25,000 | \$5,25,000 | \$5,25,000 | \$5,25,000 |
| Estimated Construction Cost |  | \$0 | \$20,393,290 | \$19,767,010 | \$19,865,290 | \$23,498,898 | \$23,503,698 |
| Estimated Total Project cost |  | 50 | \$52,913,290 | \$49,787,010 | \$45,790,290 | \$53,798,898 | \$56,443,698 |
| Traffic Operations |  |  |  |  |  |  |  |
| Number of Local Roadways Severed |  | None | None | None | None | None | None |
| Safety Constraints / Impacts |  | Existing Conditions | Increased safety in comparison to Alternative 1 due to the addition of a continuous left turn lane and widened template. The horizontal alignment follows the existing alignment and widening occurs to both sides of the existing roadway. | Increased safety in comparison to Alternative 1 due to the addition of a continuous left turn lane and widened template. Improved Horizontal Alignment. | Increased safety in comparison to Alternative 1 due to the addition of a continuous left turn lane and widened template. Improved Horizontal Alignment | Increased safety in comparison to Alternative 1 due to the addition of a continuous left turn lane and widened template. Improved Horizontal Alignment. | Increased safety in comparison to Alternative 1 due to the addition of a continuous left turn lane and widened template. Improved Horizontal Alignment |
| Human Environment |  |  |  |  |  |  |  |
| Historic Resource Impacts |  | None | to be determined | to be determined | to be determined | to be determined | to be determined |
| Cemeter Impacts |  | None | None | None | None | None | None |
| Industrial Facilities Impacts (e.g. Chemical Plant) |  | None | None | to be determined | to be determined | to be determined | to be determined |
| Commercial Facilities Impacts (e.g. Businesses) |  | None | 75 | ${ }^{6}$ | 54 | ${ }^{63}$ | 54 |
| Residential Displacement (\# houses) |  | None | 52 | 28 | ${ }_{3}$ | 28 | 35 |
| Potential Land Development |  | to be determined | to be determined | to be determined | to be determined | to be determined | to be determined |
| Physical Impacts |  |  |  |  |  |  |  |
| Potential Hazard Waste Site(s) |  | None | Impacts to Existing and listoric Serice Stations | Impacts to Existing and Historic Service Stations | Impacts to Existing and Historic Serice Stations | Impacts to Existing and Historic Service Stations | Impacts to Existing and Historic Service Stations |
| Major (Public) Utility Conflicts / mpacts |  | None | Major Utility Relocations Required | Major Utility Relocations Required | Major Utility Relocations Required | Major Utility Relocations Required | Major Utility Relocations Required |
| Major (Private) Utility Conflicts / Impacts |  | None | to be determined | to be determined | to be determined | to be determined | to be determined |
| Potential Stream Impacts |  | None | 101 LF | 266 LF | 158 LF | 258 LF | 196 LF |


| Beckley Z-Way Alignment Alternative Evaluation/Cost Matrix Segments 2 and 7 - FINAL |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Impact Category |  | Alternative No. 1 | Alternative No. 2 | Alternative No. 3 |
| Engineering |  |  |  |  |
| Prelim. Length of Airport Road | Feet | Existing Conditions | 16,800 | 16,800 |
|  | Miles | Existing Conditions | 3.18 | 3.18 |
| Roadway Configuration |  | Existing Conditions Average 2 (11' Lanes). Many areas have less than a 2' Shoulder | $2\left(12^{\prime}\right.$ Lanes) $6^{6}$ ' Paved Shoulders | 2 (12' Lanes) $14^{\prime}$ Continuous Left Turn Lane $6^{\prime}$ Paved |
| Horizontal Geometry (Min Radius) |  | 292.96' | 292.96' | 292.96' |
| Financial / Costs |  |  |  |  |
| Estimated Right of Way Acquisition Costs |  | 50 | \$5,410,000 | \$5,50,000 |
|  |  | S0 | \$5,25,000 | \$5,25,000 |
| Estimated Construction Cost |  | 50 | \$9,18, 242 | \$16,490,746 |
| Estimated Total Project Cost |  | 50 | \$19,848,242 | \$27,240,746 |
| Traffic Operations |  |  |  |  |
| Number of Local Roadways Severed |  | None | None | None |
| Safety Constraints / / mpacts |  | Existing Conditions | Widened driving lanes and shoulder | Widened driving lanes, shoulder, and added a continious left turn lane |
| Human Environment |  |  |  |  |
| Historic Resource Impacts |  | None | None | None |
| Cemetery Impacts |  | None | None | None |
| Industrial Facilities Impacts (e.g. Chemical Plant) |  | None | None | None |
| Commercial Facilities Impacts (e.g. Businesses) |  | None | None | None |
| Residential Displacement(\# houses) |  | None | None | None |
| Potential Land Development |  | None | to be determined | to be determined |
| Physical Impacts |  |  |  |  |
| Potential Hazard Waste Site(s) |  | None | Impacts to Existing and historic Serice Stations | Impacts to Existing and Historic Serice Stations |
| Major (Public) Utility Conflicts / Impacts |  | None | Major Utility Relocations Required | Major Utility Relocations Required |
| Major (Pirivate) Utility Cofficts / Impacts |  | None | Major Utility Relocations Required | Major Utility Relocations Required |
| Potential Stream Impacts |  | None | 101 LF | 266 LF |



## Appendix B - Design Criteria Summary

## Beckley Z-Way

Functional Classification - Urban Arterial
Design Speed
Minimum Design Speed 45 mph - Mountainous Terrain

## Horizontal Geometry

Maximum Radius of Curvature $=444$

## Vertical Geometry

Minimum ' K ' Vertical Crest $=61$
Minimum ' K ' Vertical Sag $=79$
Maximum Grade $=9 \%$
Minimum Vertical Clearance to Structures $=16$ feet $\mathrm{w} / 6$ " allowance for Overlay Minimum Vertical Clearance to Pedestrian Overpass = 17,

## Typical Section

Lane Widths $($ DHV $>400)=12$ feet
Continuous Left Turn Lane Width = 14 fee
Usable (Paved) Outside Shoulders $=6$ feet
Travel Lane Cross-Slope $=2 \%$
houlder Cross Slope $=4 \%$
Maximum Allowable Breakover (Outside Shoulder) $=3 \%$ (High-Side Superelevation)
Clear Zone Distance (DHV>1500) $=30$
Roadside (Foreslope) $=1 \mathrm{~V}: 4 \mathrm{H}$
Roadside (Ditch) Width $=$ 4 $^{\prime}$ Flat Bottom in Rock Cut
Roadside ( (Backs Ridepe) $=1 \mathrm{~V}: 3 \mathrm{H}$
Horizontal Clearance to Obstacles $=10$ fee

## Superelevation

Maximum Superelevation Rate $=8.0 \%$

## Design Vehicles

From Arterial to Local Road = SU
From Arterial to Industrial Plants = WB-50

## Control Acces

## Structures

Full Width for Approach Roadway

## Bridge Design Loading

HL93 using AASHTO LRFD Bridge Design Specifications

## Design Exceptions

Segment 1 Alternate 2 Horizontal and Vertical Geometry Does Not Meet 45 mph Design Speed Segment 2 and 7 Alternates 2 and 3 Horizontal and Vertical Geometry Does Not Meet 45 mph Design Speed

## Appendix C - Cost Estimates

| Segment 1 Alignment Atternative No. 2 Cost Summary - FINAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| пем мо. | descripton | ESTIMATED UUANTIT | UnT | Untr Price | TOTAL |
|  |  |  |  |  |  |
| 001-000 | Clearing and grubeng romeway | 1 | $\stackrel{\text { Ls }}{ }$ | 8250.000.00 | ${ }^{\text {s }}$ |
| 202001.00 | BuILDING Demoltion | 127 | $\stackrel{\text { Ls }}{ }$ | \$10.000.00 | 1.270.000 |
| 2001-000 | мOBILİATON | 1 | $\stackrel{\text { Ls }}{ }$ | 8150.000.00 | \$ 150,000 |
| 207001.01 | UNCLASSFIED EXCAVATION | 110,000 | cr | \$1200 | \$ 1,320.000 |
| 207002-000 207034-000 | SUBGRADE <br> FABRIC FOR SEPARATION <br> OPEN GRADED FREE DRAINING BASE COURSE | 18.663 | cr | \$5200 |  |
|  |  | ${ }_{\text {111,988 }}^{11242}$ | ${ }_{\text {sY }}^{\text {cr }}$ | S1.50 |  |
| 401 TEMS | SUPERPAVE HMA | ${ }_{73,905}$ | ton | S10500 | \$ 7,760,025 |
|  |  |  |  |  |  |
|  | ${ }^{\text {PPREE ENO SECTONS }}$ | 1 |  |  |  |
|  |  | 1 | ${ }_{\text {LS }}$ |  |  |
|  | MINOR DRAINGEE (PIPES < 36") |  |  |  |  |
| 604.TEMS | MINOR DRANAGEE PPIES | 1 | ${ }^{15}$ | 870.000 0 | ¢ 70.000 |
|  | DRAINAGE INLETS FREE DRAINING BASE TRENCH |  |  |  |  |
|  |  |  |  |  | $\begin{array}{\|lr\|} \hline \$ & 15,000 \\ \hline \$ & 552,000 \\ \hline \$ & 110 \end{array}$ |
|  | FREE DRANMG BASE TRENCH | ${ }_{\substack{46,000 \\ 9,200}}$ | ${ }_{\text {FT }}^{\text {FT }}$ | S1200 |  |
| 60701 | TPPE 1 GUAADDAL - CLASS 1 | 4.075 | ${ }_{\text {fT }}$ | \$12,00 | 48,900 |
|  | GUARDRALL END TERMINAL |  |  |  | ¢ 19,200 |
|  |  | 2 |  |  |  |
| 08002 | RIGGHT OF WAY FENCE, FAAM FIELO TPPE | 0 | FT | S4.00 | $\square$ |
| 610 TEMS | CONCRETE CUPB ANO GUITER | 0 | LF | \$75.00 |  |
| 333-IEMS | OUMPED ROCK GUITER | 1 | Ls | \$50,000.00 | \$ 50,00 <br> \$ 1.500 .00 |
| 686-TEMS | MANTIENANCE OF TRAFFIC | 1 | Ls | \$1,50,000.00 |  |
| 337-IEMS | WAIER FOR DUST PALLATVE | 1.240 | MGAL | s10.00 | 12.400 |
| 63\%.IEMS | PROUECT, RIGHT-OFWAY, SUAVEY MARERRS | 1 | เs | \$25,000.00 | ¢ 25.00 |
| 639.TEMS | Construcctoon lavout stakes | 1 | $\stackrel{\text { Ls }}{ }$ | \$50,000.00 | ¢ 50.000 |
| S40.TEMS | FIELL OFFICE AND STORAGE BULILNG | 1 | Ls | \$50.000.00 | 50,000 |
| 642-TEMS | TEMPORAAY PROUECT WAIER POLLUTION CONTROL | 1 | Ls | \$150.000.00 | ¢ 150,000 |
| 65-ITEMS | SEEDNG AND MULCHNG | 1 | Ls | \$60,000.00 | ¢ 60,000 |
| 665.TEMS | mating | 1 | Ls | \$20,000.00 | \$ 20,000 |
| 660-IEMS | TRAFFIC SIINALS PER LOCATON | 2 | EA | \$135.000.00 | \$ 270,000 |
|  | SIGNING \& PAVEMENT MARKINGS |  |  |  |  |
| 657-ITEMS | ROAOSIIE MOUNIED SIGN SUPPOATS | 1 | $\stackrel{15}{ }$ | 850.000.00 | \$ 50.000 |
| 66-TEMS | TRAFFIC SIGNS AND DELINEATORS | 1 | $\stackrel{\text { LS }}{ }$ | \$390.000.00 |  |
| 663-IEMS | MISCELLANEOUS PAVEMENT MARKINGS | 1 | $\stackrel{\text { LS }}{ }$ | S60.000.00 |  |
|  | STRUCTURES |  |  |  |  |
|  |  | 0 | Ls |  | s |
|  |  |  |  |  |  |
| Constructoon subiotal |  |  |  |  | $16,994,408$ |
| Construction Estmate |  |  |  |  | - |
|  | RIGHT OF WAY AND UTLITIES |  |  |  |  |
|  |  | 1 | ${ }^{\text {Ls }}$ |  | S27.270.000.00 |
|  |  |  | ${ }^{\text {LS }}$ | 85,250.000.00 | S 5,250,000.00 |
| RW ANO UTIUTV ESTMMATE |  |  |  |  | \$ 32,520,000 |
| TOTAL PROJECT |  |  |  |  | s 52,913,200 |


| Segment 1 Alignment Atterative No. 3 Cost Summary - FiNAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| тем мо. | descripton | (estimated | unt | UnIt Price | тотal |
|  | ROADWAY |  |  |  |  |
| 20001000 | ClEAANG ANV GUuBBNG | 1 | Ls | S12500000 | \& 125,000 |
| 20001.000 | BUllome demolmon | 91 | Ls | s10,000.0 | 910.00 |
| 204001.000 | Mobilzaton | 1 | Ls | \$150.000.00 | 150.00 |
| 200001.01 | UnCLASSSFIEE EXCAVATION | 108,000 | cr | S1200 | 1.29 |
| 20702200 | SUBGARAEE | ${ }^{18.663}$ | cr | ${ }_{8520}$ | ${ }^{\text {s }}$ - 970.476 |
|  |  | ${ }_{\text {che }}^{111,9748}$ | ${ }_{\text {sy }}^{\text {cr }}$ | si.5 |  |
| 4011 IEMS | SUUPEPPAVE HMA | ${ }_{73,95}$ | Ton | s105.0 | \$ 7.760 .005 |
|  |  |  |  |  |  |
|  | Prip Evo SECTONS | 1 | ${ }^{\text {LS }}$ | Sse.0000 | S |
|  |  |  |  |  |  |
|  | MINOR DRANNAEE (PIPES - 36) |  |  |  |  |
| S004IEMS | MNOOR DPANAGE PPESS | 1 | Ls | s70.000.00 | ¢ 70,000 |
| S05.ITMS | OPANAGE MEETS | 10 | EA. | S1.500.00 | ${ }^{\text {s }}$ 15,00e |
| biobeseor | Pree oramic base inelch | 46,000 | $\stackrel{\text { rT }}{\text { FT }}$ | (intion |  |
| 60701 | TMPE 1 GUAADPALI -CLASS 1 | 3.600 | ft | S1200 | 43,200 |
|  | GUAADORAL END TERMNAL | 12 | EA. | s1,0000 | 12.000 |
| 60802 |  | 0 | FT | ${ }_{84} 40$ |  |
| 600.EEMS | CONCREIE CURE AND GUTIER | 0 | LF | 857500 | s |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| E33.1.1EMS | OUMPED ROCK GUTIER | 1 | Ls | S50,000 | \% 50,000 |
| E66.ITEMS | MANTENANCE OF TRAFFIC | 1 | Ls | \$1.50,00000 | \$ 1.50,000 |
| 687.ITEMS | WATER FOR OUS P Pallative | ${ }_{1.240}$ | MGAL | s10.00 | ${ }^{5} \quad 12.4{ }^{12}$ |
| 688.1TEMS | Proulct, RIGHTOF-WAV, SUAVEY MAAKERS | 1 | เs | S22,00, 0 | ¢ 25.000 |
| 639.1EMS | Constructoo Lavour stakes | 1 | $\stackrel{15}{ }$ | S56,000.0 | s 50,000 |
| 800-ITMS | FELLO OFFCE AND STOAAGE UULOUNG | 1 | Ls | \$55,000.0 | s 50,000 |
| 642-IEMS | TEMPOAAAY PROUECT WATER POLLUTION CONTROL | 1 | Ls | \$150,00.00 | ¢ 150,000 |
| E52-ITEMS | SEEDNG ANOMLCHMG | 1 | Ls | S60,00.00 | s 60.000 |
| E65.1ENS | MAtING | 1 | Ls | 320.000.00 | s 20.00 |
| 600-TEMS | Traffic Silanlis Per Locaton | 2 | EA | \$135000.00 | \$ 270.000 |
|  |  |  |  |  |  |
|  | SIGNING \& PAVEMENT MARKINGS |  |  |  |  |
| E57.1EMS | RoADSIEE MOUNIES SILN SUPPORIS | 1 | Ls | S50,00.00 | s 50.000 |
| 661-1/EMS | Traf Fic Slins Ano delineators | 1 | Ls | S340,000 | S 340,000 |
| 663.1EMS | MSCELLANEOUS PAvement Markncs | 1 | Ls | 560,0000 | ¢ 60,000 |
|  | STRUCTURES |  |  |  |  |
|  |  | 0 | ${ }^{\text {LS }}$ |  | s |
| Cons rivicton sueiotal |  |  |  |  | ${ }^{5} \quad 16.472 .508$ |
|  |  |  |  |  | ${ }^{\text {cosememe }}$ |
|  |  |  |  |  |  |
|  | RIGHT OF WAY AND UTLLTIES |  |  |  |  |
|  |  | 1 | ${ }_{\text {Ls }}$ | S24.770.000.00 |  |
| aw and uturi Esinate |  |  |  |  | s 30,020.000 |
| Total Prouect |  |  |  |  | s 99,787,0000 |


| Segment 1 Alignment Atternative No. 4 Cost Summary - FINAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| тем no. | description | ESTIMATED <br> QUANTIT | unt | UnIt PRice | тотaL |
| ROADWAY |  |  |  |  |  |
| 10001.000 | ClEARING ANO GRUBBING ROADWAY | 1 | เs | 8250,000.00 | 8 250,000 |
| 2001.000 | BuILONG DEMOUTITON | 89 | Ls | 81,000,0 | 890,000 |
| 204001.000 | мовILİtion | 1 | Ls | \$150,000.00 | ¢ 150.000 |
| 207001.001 | UNCLASSIFEE EXCAVATON | 105,000 | cr | \$1200 | ¢ 1,260,000 |
| 207020.000 | SUBGRADE <br> FABRIC FOR SEPARATION | ${ }_{\text {che }}^{18.63}$ | $\stackrel{\text { cr }}{\text { SY }}$ | S5200 | s ${ }_{\text {s }}$ |
| ${ }^{207034000}$ |  | ${ }_{\text {cher }}^{111.948}$ | ${ }_{\text {cr }}^{\text {cr }}$ | Siti.00 | [ ${ }^{\text {s }}$ |
| 401 TEMS | SUPERPAVE HMA | 73,95 | ton | \$105.00 | \$ 7,760,025 |
|  | MAJOR DRAINAGE PIPESS $36^{\prime \prime}$ ) |  |  |  |  |
|  |  | 1 | $\stackrel{\text { Ls }}{ }$ | s60,000.00 | 60,000 |
|  |  |  | $\stackrel{\text { ıs }}{ }$ | 8100,000.00 | 100,000 |
|  | MINOR DSAINAGE (PPESS < 36") |  |  |  |  |
| 604TEMS | MNOR D DRANAGE PPIES | 1 | $\stackrel{\text { Ls }}{ }$ | 870,000.00 | ¢ 70.000 |
| E05.fIEM | DRAINAGE INLETS | 10 | EA. | 81.500.00 | \% 15.000 |
| ${ }^{6060293001}$ |  | ${ }_{\text {4, }}^{\text {4.,200 }}$ | $\stackrel{\text { FT }}{\text { FT }}$ | Si200 | 552,00 <br> 110.40 |
| 607001 |  | 4.075 | ${ }_{\text {FT }}$ | \$12.00 | 48.90 |
|  | GUAADBAL L ENO TEEMMNAL | 12 | EA. | \$1,600.00 | ¢ 19,200 |
| 68802 | RIGHT OF WAY FENCE, FARM FELD TPE | 0 | ${ }_{\text {FT }}$ | 54.00 | ${ }^{5}$ |
| $610-\mathrm{TEM}$ | CONCRETE CURB AND GUTIER | 0 | LF | s75.00 | s |
| 633 -TEMS | DUMPED ROCK GUTIER | 1 | Ls | \$50,000.00 | 50.00 |
| 666-TEMS | MAINTENANCE OF TRAFFIC | 1 | ${ }^{\text {LS }}$ | \$1,50,000.00 | \$ 1.500.000 |
| 677-TEMS | WATER FOR DUST PALLATVE | 1.240 | MGAL | s10.00 | ¢ 12.400 |
| 683-1EMS | PROUECT, RIGHTOOFWAV, SUAVEY M MAKERS | 1 | $\stackrel{\text { Ls }}{ }$ | \$25.000.00 | ¢ 25.000 |
| 699.TEMS | Consstruction lavout stakes | 1 | $\stackrel{15}{ }$ | \$55,000.00 | ¢ 50,000 |
| 640-TEMS | FFELDOFFICE AND STOPAGE BUILING | 1 | $\stackrel{\text { Ls }}{ }$ | \$50.000.00 | S 50.006 |
| 662-TEMS | TEMPORAAY PROUECT WAIER POLLUTION CONTROL | 1 | $\stackrel{\text { LS }}{ }$ | \$150,000.00 | S 150,000 |
| 65--TEMS | SEEDING AND MUCCHING | 1 | Ls | s60.000.00 | \$ 60.000 |
| 655.TEMS | MAATING | 1 | Ls | \$20,000.00 | \$ 20,000 |
| 660-ITMS | Traf FIC Signal Per Location | 2 | Ls | \$135.00,00 | S 270,000 |
|  | SIGNING \& PAVEMENT MARKINGS |  |  |  |  |
| 65-TIEMS | RoADSIIE MOUNIED SIGN SUPPOATS | 1 | Ls | \$50.000.00 | ¢ 50.000 |
| 661.1 IEMS | TrAAFFIC SIGNS AND DELINEATORS | 1 | Ls | \$840,000.00 | 340.000 |
| 663 -TEMS | MISCELANEOUS PAVEMENT MAAKINGS | 1 | Ls | 860.000.00 | 60.00 |
|  | STRUCTURES |  |  |  |  |
|  |  | 0 | Ls |  | s |
| CONSTRUCTION SUBTOTAL <br> COO\% ERCUCTION ESTIMATE <br> CONSTRUCTE |  |  |  |  |  |
|  |  |  |  |  | (16.54.408 |
|  |  |  |  |  | come |
|  | RIGHT OF WAY AND UTILTIES |  |  |  |  |
|  | RIGHT OF WAY ACQUISITION UTILITY RELOCATION |  | ${ }_{\text {Ls }}$ | 820.675.000.00 | s 20.675.000.00 |
|  |  | 1 | Ls | S5,250,000.00 | S 5,250,000.00 |
| RWN AND UTILIT ESTMATE |  |  |  |  | S $25.95,000$ |
| Total Provect |  |  |  |  | s $45.790,200$ |


| Segment 1 Alignment Aternative No. 5 Cost Summary - -INAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| тем м | DESCRIPTION | ESTIMATED | UNT | UnIt PRIIE | Total |
| 201001000 | ROADWAY |  |  |  |  |
| 202001.000 | BULIDMG DEMOLITON | 9 | Is |  |  |
| 204001.000 | MOBILITION | 1 | Ls | \$150,000.00 | S 150,000 |
| 207001.001 | UNCLASSIFIED EXCAVATON | 103,000 | cr | \$12.00 | 1,236,00 |
|  | SUGEADE |  |  |  |  |
| ${ }^{2077023000}$ | SUBGRADE | $\xrightarrow{16,07} 9$ | $\stackrel{\text { cr }}{\text { sV }}$ | ¢S5200 <br> 51.50 | ${ }_{\text {c }}^{8}$ |
| 311006.001 | OPEN GPADED PREE DPANNG BASE COURSE | 10,738 | cr | S120.00 | ¢ 1,288,560 |
| 401 TEMS | SUPEPPAVE HMA | 63,785 | ton | S105.00 | \$ 6,697,425 |
|  | MAJOR DRAINaGE( PIPES 3 36") |  |  |  |  |
|  | PIPE END SECTIONS PIPES | $\frac{1}{1}$ | ${ }_{\text {LS }}^{\text {LS }}$ | $\underbrace{\text { s85,0000 }}_{\text {S60,000.00 }}$ |  |
|  | MINOR DPAANAGE (PIPES < $36{ }^{\text {c/ }}$ ) |  |  |  |  |
|  |  |  |  |  |  |
| B04TEMS | MINOR D PANANGE PPIES | 1 | LS | 5910,000.00 | 910.00 |
| G05. TEMS | DRAINAGE INLETS | 130 | EA. | 81.500.00 | $8 \quad 1950$ |
|  |  | 46.000 | ${ }_{\text {FT }}^{\text {FT }}$ | St1200 | ${ }^{\text {¢ }}$ |
| 607001 | TTPE 1 GUARDPALL-CLASS 1 | 4.075 | ${ }_{\text {FT }}$ | \$1200 | ¢ 48,900 |
|  | GUAABPALI END TERMNAL | 12 | EA. | s1.600.00 | 19,200 |
| 60802 | RIGGT OF WAY FENCE, FARM FIELD TYPE | 0 | ${ }_{\text {FT }}$ | \$4,00 |  |
| 60-ITEMS | CONCREEE CURB AND GUTIER | 46.00 | LF | \$75.00 | \$ 3.450,000 |
| 633.ITEMS | OUMPED ROCK GUTIER | 1 | Ls | \$50,000.00 | \$ 50,000 |
| 36.TEMS | MAINTENANCE OF TRAFFIC | 1 | LS | \$1,50,000.00 | 1,50,000 |
| 637-ITEM | WATER FOR DUSTPALLATVE | 1.240 | MGAL | s10.00 | S 12.40 |
| E838.IEMS | PRoJECT, RGGHT-OF-WAY, SUVVEY MARKERS | 1 | Ls | s25,000.00 | ¢ 25.00 |
| 639.IEMS | Construution lavout stakes | 1 | LS | \$55,000.00 | ¢ 50,00 |
| 640-TIEMS | FELLD OFFICE AND STORAGE BULING | 1 | LS | \$55,000.00 | S 50.000 |
| 642-ITENS | TEMPOAAAY PROUECCT WATER POLLUTION CONTROL | 1 | Ls | \$150,000.00 | 150,00 |
| 652-ITEMS | SEEDING ANO MUCHHNG | 1 | Ls | \$60,000.00 | \$ 60.000 |
| 655.1 IEMS | MATING | 1 | Ls | s22,000.00 | \$ 20.000 |
| 60-IEMS | Traf Fic sicnals Per Locaton | 2 | EA | \$135,000.00 | \$ 270,000 |
|  | SIGNING \& PAVEMENT MARKINGS |  |  |  |  |
| 657-IEMS | RoADSIE MOUNTED SIGN SUPPOATS | 1 | Ls | S50,000.00 | S 50,000 |
| 66-ITEMS | TRAFFIC SIINS ANO DELINEATORS | 1 | LS | \$340.000.00 | \$ 340,000 |
| 663-1/ ME | MISCELANEOUS PAVEMENT MARKNGS | 1 | ${ }^{\text {LS }}$ | s60,000.00 | S 60.000 |
|  | STRUCTURES |  |  |  |  |
|  |  | 0 | Ls |  |  |
|  |  |  |  |  |  |
| COSSTTUCTION SUBTOTAL <br> 20\% ERCOUCTION ESTIMATE <br> CONSTRRCTM |  |  |  |  | 19,582,415 |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  | RIGHT OF WAY ACQUISITION UTLITY RELOCATION | 1 | ${ }^{\text {LS }}$ | \$25.550.000.00 | \$ 25,050.000.00 |
|  |  |  | ${ }^{\text {LS }}$ | 85,250,000.00 | \$ 5.250,000.00 |
| RW AND UTIUTV ESTMATE |  |  |  |  | \$ 30,300,000 |
| TOTAL PROJECT |  |  |  |  | $s^{53,798,8}$ |


| Segment 1 Alignment Atternative No. 6 Cost Summary - FINAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| тем no. | description | ESTIMATED QUANTI | unt | UnIt PRice | Total |
| ROADWAY |  |  |  |  |  |
| 10001.000 | ClEARING ANO GRUBBING ${ }^{\text {ROADWAY }}$ | 1 | เs | 8250,000.00 | \% 250,000 |
| 2001.000 | Bullong demolion | 89 | Ls | 81,000,0 | 890,000 |
| 204001.000 | мовILİton | 1 | Ls | \$150,000.00 | ¢ 150,000 |
| 207001.001 | UNCLASSIFIED EXCAVATON | 105,000 | cr | \$1200 | ¢ 1,280,000 |
| 20702-000 | SUBGRADE <br> FABRIC FOR SEPARATION | $\xrightarrow{16,107}$ O6, | $\stackrel{\mathrm{cr}}{\mathrm{sy}}$ | S5200 |  |
| ${ }^{2070234000}$ |  | ${ }_{\text {c }}^{\text {96,644 }} 10.788$ | ${ }_{\text {cr }}^{\text {cr }}$ | Sile |  |
| 401 TEMS | superpave hma | ${ }^{63,785}$ | Ton | \$105.00 | ${ }^{5}$ 6,697,425 |
|  | MAJOR DRANAGE (PIPES $33^{6 \prime \prime}$ ) |  |  |  |  |
|  |  | 1 | ${ }^{\text {LS }}$ | 860,000.00 |  |
|  |  |  | $\stackrel{\text { Ls }}{ }$ | 885,000.00 | s 85,000 |
|  | MINOR DRAINAGE (PPESS 3 36") |  |  |  |  |
| 604TEMS | MINOR DRANAGE PPIES | 1 | $\stackrel{\text { Ls }}{ }$ | \$910.000.00 | S 910,000 |
| E05.NEMS | DRAINAGE INLETS | 130 | EA. | \$1.500.00 | ¢ 195.000 |
| ${ }^{6060293001}$ |  | $\xrightarrow{4.0 .000}$ | $\stackrel{\text { FT }}{\text { FT }}$ | Si200 | ¢52.000 |
| 667001 | TTPE 1 GUAADPAAL - CLASS 1 | 4.075 | ${ }_{\text {FT }}$ | \$12.00 | 48.900 |
|  | GUARODAL END TEEMINAL | 12 | EA. | \$1,600.00 | ¢ 19,200 |
| 60802 | RIGHT OF WAY FENCE, FARM FELLO TPE | 0 | ${ }_{\text {FT }}$ | 54.00 | s |
| 610-ITEM | CONCRETE CURB ANO GUUTER | 46.00 | LF | s75.00 | \$ 3.450,000 |
| 633 -TEMS | DUMPED ROCK GUITER | 1 | Ls | \$50,000.00 | \$ 50,000 |
| 636-ITEM | MAINTENANCE OF TRAFFIC | 1 | $\stackrel{\text { LS }}{ }$ | \$1.50,000.00 | S 1.500,000 |
| 677.ITEM | WATER FOR DUST PALLATVE | 1.240 | MGAL | S10.00 | ¢ 12.400 |
| 688.1EMS | PROUECT, RIGHTOOFWAV, SUAVEY M MAKERS | 1 | ${ }^{\text {Ls }}$ | \$25,000.00 | ¢ 25.000 |
| 639.fens | Consstructov Larour stakes | 1 | ${ }^{\text {Ls }}$ | \$50.000.00 | ¢ 50.000 |
| 640-TEMS | FFELDOFFICE AND STOPAGE BUILING | 1 | $\stackrel{\text { Ls }}{ }$ | \$50.000.00 | ¢ 50,000 |
| 642-TEMS | TEMPOAAAY PROUECT WATER POLLUTION CONTROL | 1 | $\stackrel{\text { LS }}{ }$ | \$150,000.00 | ¢ 150,000 |
| 65--TEMS | SEEDING AND MUCCHING | 1 | Ls | s60.000.00 | ¢ 60,000 |
| 655 -TEM | MAATING | 1 | Ls | \$20,000.00 | ¢ 20,000 |
| 660-ITMS | Traf FIC Signal Per Location | 2 | EA | \$135.00,00 | \$ 270,000 |
|  | SIGNING \& PAVEMENT MARKINGS |  |  |  |  |
| 657-ITMS | ROAOSIEE MOUNIED SIGN SUPPOATS | 1 | Ls | \$50.000.00 | ¢ 50,000 |
| 661.1 IEMS | TrAAFFIC SIGNS AND DELINEATORS | 1 | Ls | \$840,000.00 | 340,000 |
| 663 -TEMS | MISCELANEOUS PAVEMENT MAAKINGS | 1 | Ls | 860.000.00 | 60.000 |
|  | STRUCTURES |  |  |  |  |
|  |  | 1 | Ls |  | $\stackrel{ }{5}$ |
| CONSTRUCTION SUBTOTAL <br> COO\% ERCUCTION ESTIMATE <br> CONSTRUCTE |  |  |  |  |  |
|  |  |  |  |  | (19.56.415 |
|  | RIGHT OF WAY AND UTIITIES |  |  |  | ${ }_{\text {23,503,988 }}$ |
|  |  |  |  |  |  |
|  | RIGHTO OF WA ACOUISTION |  | ${ }_{\text {Ls }}$ |  | S 27,990,000.00 |
|  | UIUITY RELOCATON | 1 | Ls | \$85,55,000.00 | ${ }^{\text {s } 5.550 .00000000}$ |
| RW ANOUTIUTVESTMATE |  |  |  |  | S 32,940,000 |
| Total Provect |  |  |  |  | S 56,443,698 |


| Segement 2 and 7 Alignment Alternative No. 2 Cost Summary - FINAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| m no. | DESCRFPToN | ESTIMATED <br> QUANTIT | Unt | UnIT PRICE | тоtal |
|  | ROADWAY |  |  |  |  |
| 201001-000 | ClEARING ANO GRUBBING | 1 | Ls | s250,000.00 | \$ 250.000 |
| 2001000 | IILING DEMOLITON | 0 | Ls | S10,000.00 |  |
| 204001.000 | MOBILZATON | 1 | Ls | \$150,000,00 | 150,000 |
| 207001.001 | UNCLASSIFIED EXCAVATION | 59.00 | cr | \$1200 | \$ 708.000 |
| 207702.000 | SUBGAADE | 7.863 | cr | \$5200 | \$ 408.876 |
| ${ }^{2027034000}$ | FABEIC For SEPARATON | ${ }_{\substack{47,178 \\ 5.24}}$ | SY | Si.500 | ¢ ${ }_{\text {s }}$ |
| 401 TEMS | SUPERPAVE EMMA | 31,137 | Ton | \$105.00 | \$ 3,269,35 |
|  | MAJOR DRANAGE( PIPES 3 36") |  |  |  |  |
|  | PIPE ENO SECTIONS | 1 | ıs | s60,000.00 | \$ 60,000 |
|  |  | 1 | เs | \$100,000.00 | \$ 100,000 |
|  | MINOR D DAANAGE (PIPES S 36") |  |  |  |  |
| E04TEMS | MINOR DRANAGE PPES | 1 | Ls | s70,000.00 | ¢ 70.000 |
| E05-IEMS | drandage Ile | 10 | EA. | s.1500.00 | ${ }^{\text {s }} \quad 15.000$ |
|  |  | ${ }_{\substack{27.000 \\ 5.400}}$ | ${ }_{\text {FT }}^{\text {FT }}$ | ${ }_{\text {si2 }}^{\text {si200 }}$ | ${ }^{\text {s }}$ |
| 667001 | TTPE 1 GUARDPAL - Class 1 | 1.400 | FT | \$12.00 | 16.800 |
|  | GUAADPAL END TEPMMNAL | 8 | EA. | \$1,600.00 | \$ 12,800 |
| 60802 | RIGHT Of WAY FENCE, FARM Fillo TPP | 0 | ${ }_{\text {FT }}$ | \$4.00 |  |
| 610-ITEM | CONCRETE CURB AND GUTIER | 0 | LF | 875.00 | s |
| 633.IEWS |  |  |  |  |  |
|  |  |  |  |  |  |
| 636-IEMS | MAINTENANCE OF TRAFFIC | 1 | Ls | 8750,000.00 | \$ 750,000 |
| 677.1EMS | WATER FOR DUSTPALLATVE | 1.240 | MGAL | \$10.00 | ¢ 12.400 |
| 638.IEMS | PROUECT, RGGHTTOF-WAY, SUAVEY MAREERS | 1 | Ls | s25,000.00 | S 25.000 |
| 699.IEMS | Construction LaYout Stakes | 1 | LS | S50,000.00 | 50.000 |
| 640-TEMS | FFELDOFFICE AND STORAGE BULILING | 1 | Ls | \$50,000.00 | S 50,000 |
| 842-IEMS | TEMPORAAY PROUECT WATER POLLUTION CONRROL | 1 | Ls | 85,000.00 | ${ }^{\text {s }} \quad 75.000$ |
| 652-IEMS | SEEDING AND MUCHHMG | 1 | Ls | S60,000.00 | ¢ 60,000 |
| 655-TEMS | mating | 1 | Ls | S22,000.00 | ¢ 20,000 |
| 60-IEMS | Traffic signals Per Location | 1 | EA | \$135,000.00 | 135,00 |
|  | SIGNING \& PAVEMENT MARKINGS |  |  |  |  |
| 65-IEMS | ROADSIEE MOUNTED SICN SUPPOATS | 1 | $\stackrel{\text { Ls }}{ }$ | S50,000.00 | S 50,000 |
| $66^{\text {6-ITEMS }}$ | TrAAFIC SICNS AND DELINEATORS | 1 | LS | s170.000.00 | S 170,000 |
| 66-TEMS | MSCELLANEOUS PAVEMENT MARKINGS | 1 | $\stackrel{\text { Ls }}{ }$ | 860,000.00 | ¢ 60.000 |
|  | StRUCTURES |  |  |  |  |
|  |  | 1 | Ls |  | s |
|  |  |  |  |  |  |
| Constructoon subitotal |  |  |  |  | ${ }_{7,656.868}$ |
|  |  |  |  |  |  |
|  | RIGHT OF WAY AND UTLITIES |  |  |  |  |
|  | RIGHTI OF WAY ACOUUSTION |  | ${ }^{\text {LS }}$ | \$5.410,000.00 | \$5.410,000.00 |
|  | Uulur ellocaton | 1 | Ls | S5.250,000.00 | S 5.250,000.00 |
| RWN AND UTULTV ESTMATE |  |  |  |  | \$ 10,660.000 |
| Total Prouect |  |  |  |  | $s \quad 19.884,242$ |



| Segement 8 Atternative No. 1 Overpass Cost Summary - FiNAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| M No. | desciripton | ESTIMATED QUANTITY | unt | UnIT PRice | тotal |
|  | ROADWAY |  |  |  |  |
| 201001.000 | Cleating ano gubebing | 1 | เs | 8250,000.00 | 250.000 |
| 202001.000 | BUULONG DEMOLITION | 27 | Ls | \$10,00000 | \$ 270.000 |
| 204001.000 | Mobilizaton | 1 | Ls | S156,000.00 | 155000 |
| 220001001 | UnCLASSFIELEEECAVATION | 1,154,000 | or | 1200 | 13,848,000 |
| 207020.000 | SUBGRaDE | ${ }^{7.578}$ | cr | ${ }_{552} 5$ | 394,066 |
| $\frac{207034000}{311005001}$ | Ferabic for separaton | ${ }_{\text {L }}^{4.957}$ | s\% | $\frac{8}{\text { sin }}$ ST00 | ${ }^{\text {c }}$ |
| 401 TeMs | SUPERPAVE HMA | 30.08 | ToN | S105.00 | s 3,15, 840 |
|  | MAJOR DRANAGEEPPPESS 3 36") |  |  |  |  |
|  | PPPE ENO SECTIONS | 1 | ${ }_{\text {Ls }}$ | S60.000.00 | 60.000 |
|  |  |  | เs |  |  |
|  | MINOR DRAINAGEE PPPES < 36] |  |  |  |  |
| 604TEMS | MINOR DRANAGE PPES | 1 | Ls | 870.00.00 | \$ 70,000 |
| 605.EMS | drandage ILETS | 10 | EA. | \$1.500.00 | ${ }^{\text {s }} \quad 15.000$ |
|  | Frie oranlug base frevch | ${ }_{\substack{18.600 \\ 3.720}}$ | ${ }_{\text {FT }}^{\text {FT }}$ | $\xrightarrow{\text { S1200 }}$ |  |
| 607001 | TTPE 1 GUAABDALL Class 1 | 7800 | fт | S20 |  |
|  | GUAROPALI END TEFMNAL | 16 | EA. | s1,600.00 | ¢ 25.500 |
| 68802 | RIGHT OF WAY FENCE, FAAM FELLD TPE | 0 | ${ }_{\text {FT }}$ | S4,00 | s |
| 610-TEMS | CONCCRE EE CURE AND GUTITER | 0 | ${ }_{\text {LF }}$ | 857.00 |  |
| 633.EMS | OUMPED ROCK GUTIER | 1 | ${ }^{15}$ | \$50.00.00 | S 50.000 |
| 636-TEMS | MANTENANCE OF TRAFFIC | 1 | LS | 81.500.00.00 | 1.500.000 |
| C37.EEMS | WATER For dust pallatie | 1.240 | MGAL | s10,00 | 12400 |
| 689.EMMS | Prouject, Rligrop-war, Surver Mafkers | 1 | Ls | \$25.00,00 | 25.00 |
| 639.EMS | Constructoon lavout stakes | 1 | $\stackrel{1}{5}$ | 850.000.00 | 5.000 |
| 640-TEMS | FELLDOFFICE AND STOPAGE EULIDNG | 1 | Ls | \$50,00,00 | S 50,000 |
| 642-EEMS | TEMPORAAY PROUECT WATER POLLUTON Control | 1 | เs | 557.000.00 | 75,000 |
| 652-IEMS | SEEDNG ANO MUCHMIG | 1 | $\stackrel{\text { LS }}{ }$ | S60.0000 | 60.000 |
| 659.rems | mating | 1 | Ls | \$20.00,00 | ¢ 20.000 |
| 66-ITEMS | Traffic Signals Per Locaton | 3 | EA | S135.00000 | 405,000 |
|  | SIGNING \& PAVEMENT MARKINGS |  |  |  |  |
| 65-TEMS | Roodosid Mounte sian Sup Poris | 1 | Ls | \$56,00000 | 50,000 |
| 66-ITEMS | TPAFFIIC SIINS AND DELINEATOAS | 1 | LS | S170,000.00 | 170,000 |
| 66s.rems | MSCELLANEOUS PAVEMENT MARKNGS | 1 | Ls | 860.00000 | 60.00 |
|  | STRUCTURES |  |  |  |  |
|  |  | 1 | ${ }^{\text {Ls }}$ | Sti.3.7.77.00 |  |
|  |  |  |  |  |  |
|  |  |  |  |  | 28.37.724 |
|  |  |  |  |  |  |
| US 19 CONNECTOR |  |  |  |  |  |
|  | US 19 COONE CTOR-SEE US 19 CoNMECTOE ESTMATE FOR DETALIS | 1 | LS | 13,669,43 | 13,669,483 |
| RIGHT OF WAY AND UTLUTIES |  |  |  |  |  |
|  |  | 1 | ${ }_{\text {Ls }}^{15}$ | S10.25.500.00 | (10.25500000 |
|  |  |  |  |  |  |
| AW ANO UTIUTV ESTIMATE |  |  |  |  | 15,525.000 |
| Total Prouect |  |  |  |  | 5 S62711.053 |


| Segement 8 Alternative No. 1 At-Grade Cost Summary - FiNAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| тем мо. | descaripton | ESTIMATED | UnT | UnTt PRIE | Total |
| 201001.00 | Cleanimg ano grubeing roadway |  |  |  |  |
| 220001.00 | BUILIONG Demoltion | ${ }^{27}$ | Ls | S10.000.00 | 270.000 |
| 200001.00 | мobluaton | 1 | Ls | \$150,000.00 | 150,000 |
| 200001.01 | UNCLASSFIELEEXCAVATION | 2.235,000 | or | \$1200 | 26.820.000 |
| $\frac{200702000}{20730000}$ |  | ${ }_{\text {7.985 }}^{\text {4,9, }}$ | ${ }_{\text {cr }}^{\text {sY }}$ | ${ }_{5 \text { S5200 }}^{5150}$ | ${ }^{\text {s }}$ |
| 201006.001 |  |  | ${ }_{\text {cr }}^{\text {cr }}$ | Stiono |  |
| 401 TEMS | SUPERPPVVE HMA | 31,621 | Ton | S105.00 | S ${ }^{\text {3,320,205 }}$ |
|  | MAJOO DRANAGEE PPIESS $36^{6}$ ) |  |  |  |  |
|  | Plipe Eno sectoos | 1 | ${ }_{\text {Ls }}$ | S60.00.00 | ${ }^{\text {s }}$ - 60.000 |
|  |  |  | Ls | S100,00000 | s 100,000 |
|  | MINOR DAANAGE (PIPES < 36") |  |  |  |  |
| E04TEMS | MMOR DRANAGEE PPES | 1 | Ls | s70.000.00 | ¢ 70.000 |
| E05.fens | ORANMGE MEETS | 10 | EA. |  | 1500 |
|  |  | ${ }_{\substack{19.600 \\ 3,920}}$ | $\stackrel{\text { r }}{\text { FT }}$ | ¢ | - |
| 6070 | TVPE 1 GUARBPALI - CLASS 1 | 3,500 | ${ }_{\text {FT }}$ | \$1200 | \$ 42000 |
|  | GUARODALL END TERMMNAL | 8 | EA. | 81,600.00 | 12880 |
| 68802 | RGGHT OF W AY FENCE, FAPM FIEL T TPE | 0 | fr | 84.00 |  |
| 610-TEMS | CONCCEEE CURB AND GUTIER | 0 | LF | 875.00 | s |
|  |  |  |  |  |  |
| 683\%.1.MS | OUMPEED Pock Gulter | 1 | Ls | S50,000.00 | 50,000 |
| E66-TEMS | MANTENANCE OF TRAFFIC | 1 | Ls | \$1.500.000.00 | s 1.50.000 |
| 687.EEMS | WAIEE FOR DUST PALLATIVE | 1.240 | MGAL | s10.00 | - 12.400 |
| C68.-TEMS | PROUJECT, RGGHTOF-WAV, SUVVEY MARKERS | 1 | เs | s25,000.00 | ¢ 25,000 |
| 699.1EMS | Consstructoo LaYout Stakes | 1 | เs | S50,000.00 | 50.00 |
| 60-TEMS | FELLD OFFICE AND STOPAGE BULIONG | 1 | Ls | \$50.000.00 | 50.000 |
| G62-TEMS | TEMPOPAAY PROUECT WATER Polluton control | 1 | ${ }^{\text {LS }}$ | 857,000.00 | S 75.000 |
| 652-IEMS | SEEDNG ANO MUCHMING | 1 | ${ }^{\text {LS }}$ | S60.000.00 | ¢ 60.000 |
| E55.rems | mating | 1 | Ls | S20.00000 | S $\quad 20.000$ |
| 660-TEMS | Trafflc Signals Per Location | 4 | EA | ¢135.00.00 | \$ 540.000 |
|  | SIGNING \& PAVEMENT MARKINGS |  |  |  |  |
| 657-IEMS | ROAOSIEE MOUNTED SIGNSUPPORTS | 1 | ${ }^{15}$ | \$50,000.00 | S 50.000 |
| 66-ITEMS | TraAFIC SIGNS AND DELINEATOAS | 1 | Ls | 8170.00,00 | \$ 170.000 |
| 663 TEMS | MSCELLANEOUS PAVEMENT MAFKNGS | 1 | ${ }^{\text {LS }}$ | s60,000.00 | 60.00 |
|  | STRUCTURES |  |  |  |  |
|  | LITIE BEAVER CREEK BRIDGE ESSTMATEE AT S SOO1 PER SQ. FT.) WV 307 OVERPASS (ESTIMATED AT \$201 PER SQ. FT.) | 1 | ${ }_{\text {Ls }}^{\text {LS }}$ | Stionticheo |  |
| CONSTRUCTION SUBTOTAL <br> $20 \%$ E\&C CONSTRUCTION ESTIMATE |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  | cione |
|  | US 19 CONNECTOR |  |  |  |  |
|  | US 19 CoONE CTOR- SEE US 19 CONNECTOR ESTIMATE FOR DETALIS | 1 | ${ }^{\text {LS }}$ | ${ }_{13,169483}$ | 13,669,43 |
|  | RIGHT OF WAY AND UTLITIES |  |  |  |  |
|  | Right of way Acoulsion | 1 | ${ }^{\text {Ls }}$ | s99955000.00 | 9.985000000 |
|  | UTULTY RELOCATON |  | Ls | S5,250,00000 | \$ 5.250.000.00 |
| EN AND UTIUTVESTMMATE |  |  |  |  | 15.235 .00 |
| Total Prouect |  |  |  |  | $s$ s $78.361,511$ |


| Segement 8 Aternative No. 2 Cost Summary - FinAL |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| тем no. | DESCRAPTIoN | ESTIMATED <br> QUANTITY | unt | UNTT PRIGE | Total |
| 20.10000 | ROADWAY |  |  |  |  |
| 22000.000 |  |  |  |  |  |
| 202001.000 | BULIDMG demoltion | ${ }^{27}$ | Ls | 50.000 | 20.00 |
| 204001.00 | Mobilzaton | 1 | Ls | \$150.00,00 | 150.000 |
| 207000-01 | UNCLASSIFELE EXCAVATON | 1,566,000 | or | S1200 | S 18,792,00 |
| $\frac{20702000}{20030000}$ |  | $\underbrace{\substack{\text { cis }}}_{\substack{6.763 \\ 40585}}$ | ${ }_{\text {cr }}^{\text {cr }}$ | ${ }_{\substack{\text { S5200 }}}^{\text {S150 }}$ |  |
|  |  | 4.509 | ${ }_{\text {cr }}^{\text {cr }}$ | sti.00 | $\xrightarrow{\text { 540,080 }}$ |
| 4011 TeMs | SUPERPAVE HMA | 26.781 | ToN | \$105.00 | \$ 2.812 .005 |
|  | MASOR DRANAGEE PPIESS 3 36") |  |  |  |  |
|  | PPREEND SECTONS | 1 | $\stackrel{\text { Ls }}{15}$ | S60,0000 | ${ }^{\text {s }}$ ¢0.000 |
|  |  |  |  |  |  |
|  | MINOR DPAINAGEE (PIPES < 36") |  |  |  |  |
| 604TEMS | MINOR DPANAGE P PIES | 1 | Ls | 50,000.00 | ¢ 70.000 |
| E05.fens | ORANAGE MEFTS | 10 | EA. |  | - |
|  | Fefe dranlig Base itench | ${ }_{\substack{16,600 \\ 3,300}}^{\text {a }}$ | ${ }_{\text {FT }}^{\text {FT }}$ | $\underset{\substack{\text { si220 } \\ \text { S1200 }}}{ }$ | (199200 |
| 607001 | TPPE 1 GUAARPALI - CLASS 1 | 5.900 | FT | \$1200 | \$ 70,800 |
|  | GUAROBAL END TEEMNAL | 10 | EA. | 81,600.00 | 16.00 |
| 68802 | RIGHT OF W AY FENCE, FAAM FELID TPE | 0 | FT | 5400 | s |
| 610-TEMS | CONCREEE CUBE ANO GUTITER | 0 | ${ }^{\text {LF }}$ | 575.00 | s |
|  | OUMPED ROCK GUTIER | 1 | $\stackrel{\text { Ls }}{ }$ | S50.00000 | ¢ 50.00 |
| E36-IEMS | MANTENANCE OF TRAFFIC | 1 | ${ }^{\text {Ls }}$ | 81.50.0.00.00 | 1.50,000 |
| 637.few | WATER FOR DUST PALLATIVE | 1.240 | MGAL | s10.00 | ${ }_{12,400}$ |
| 689.IEMS | PROUECT, RGGHT.OF-WAY, SUVVVY MAAKERS | 1 | Ls | \$25,000.00 | \% 25.000 |
| 693.1EMS | Consstructoo Lavour Stakes | 1 | LS | \$50.000.00 | 50.00 |
| 600-TEMS | Fell office Ano storage bulong | 1 | Ls | \$50.000.00 | - 50.000 |
| 662-IEMS | TEMPOBAAY PROUECT WATER Polluton conntol | 1 | Ls | 575,000.00 | ¢ 75.000 |
| 652-IEMS | SEEDNG ANO MULCHING | 1 | $\stackrel{\text { Ls }}{ }$ | S60,000. | 60.00 |
| 655.rems | mativa | 1 | Ls | S20,000.00 | 20.000 |
| 660-1TEMS | TrAFFIC SIINALS PER LOCATION | 3 | EA | S135.00,00 | 405.000 |
|  | SİNING \& PAVEMENT MARKINGS |  |  |  |  |
| 657-1EMS | ROADSIE MOUNTEDSIGNSUPPORTS | 1 | $\stackrel{\text { Ls }}{ }$ | \$50,00000 | ¢ 50,00 |
| 66-TEMS | Traffic sicns Ano delinearons | 1 | $\stackrel{15}{ }$ | S170.000.00 | ¢ 170.000 |
| 663.rems | MSCCLLANEOUS PAVEMENT MARKINGS | 1 | ${ }^{\text {Ls }}$ | s60.000.00 | 60.00 |
|  | STRUCTURES |  |  |  |  |
|  |  | 1 | ${ }_{\text {LS }}^{15}$ |  | ${ }_{\text {s }}^{\text {s }} 1$ |
| CONSTRUCTION SUBTOTA 20\% E\&C CONSTRUCTION ESTIMAT |  |  |  |  | ${ }^{32,776,23}$ |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  | US 19 CONNECTOR |  |  |  |  |
|  | US 19 Coonvector. SEE US 19 COMNECTOR ESTMATE EOR DETALLS | 1 | Ls | 13,169483 | S 13,169,483 |
|  | RIGHT OF WAY AND UTLITIES |  |  |  |  |
|  |  | 1 | $\stackrel{15}{15}$ | Sosems.00.00 | ¢ 9,955.00000 |
| AW AND UTILIT ESTIMATE |  |  |  |  | ¢ 1523 |
| TOTAL PROJECT |  |  |  |  | $s$ s $67,735,963$ |



## Appendix D - Acquisition Tables

ACQUISITION TABLE

| PARCEL NUMBER | PARCEL TOTALS |  | SEGMENT 1 - US 19 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 4 |  | ALT 5 |  | ALT 6 |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
| 1 | 8,936 | 0.21 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 2 | 27,768 | 0.64 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 3 | 78,003 | 1.79 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 4 | 71,194 | 1.63 | 0 | 0 | 0.00 | 0 | 0.00 | 1,805 | 0.04 | 0 | 0.00 | 1,805 | 0.04 |
| 5 | 40,429 | 0.93 | 0 | 1,573 | 0.04 | 1,965 | 0.05 | 5,242 | 0.12 | 1,965 | 0.05 | 5,242 | 0.12 |
| 6 | 293,373 | 6.73 | 0 | 17,085 | 0.39 | 17,085 | 0.39 | 23,500 | 0.54 | 17,085 | 0.39 | 23,500 | 0.54 |
| 7 | 49,778 | 1.14 | 0 | 7,873 | 0.18 | 9,530 | 0.22 | 8,777 | 0.20 | 9,530 | 0.22 | 8,777 | 0.20 |
| 8 | 4,719 | 0.11 | 0 | 804 | 0.02 | 982 | 0.02 | 923 | 0.02 | 982 | 0.02 | 923 | 0.02 |
| 9 | 3,724 | 0.09 | 0 | 845 | 0.02 | 130 | 0.00 | 963 | 0.02 | 130 | 0.00 | 963 | 0.02 |
| 10 | 6,147 | 0.14 | 0 | 763 | 0.02 | 967 | 0.02 | 902 | 0.02 | 967 | 0.02 | 902 | 0.02 |
| 11 | 37,406 | 0.86 | 0 | 8,225 | 0.19 | 8,225 | 0.19 | 7,750 | 0.18 | 8,225 | 0.19 | 7,750 | 0.18 |
| 12 | 18,683 | 0.43 | 0 | 8,175 | 0.19 | 9,491 | 0.22 | 9,150 | 0.21 | 9,491 | 0.22 | 9,150 | 0.21 |
| 13 | 11,179 | 0.26 | 0 | 3,207 | 0.07 | 3,207 | 0.07 | 3,074 | 0.07 | 3,207 | 0.07 | 3,074 | 0.07 |
| 14 | 12,254 | 0.28 | 0 | 2,954 | 0.07 | 2,954 | 0.07 | 2,825 | 0.06 | 2,954 | 0.07 | 2,825 | 0.06 |
| 15 | 36,011 | 0.83 | 0 | 214 | 0.00 | 562 | 0.01 | 527 | 0.01 | 562 | 0.01 | 527 | 0.01 |
| 16 | 70,797 | 1.63 | 0 | 7,146 | 0.16 | 7,146 | 0.16 | 6,827 | 0.16 | 7,146 | 0.16 | 6,827 | 0.16 |
| 17 | 45,067 | 1.03 | 0 | 7,938 | 0.18 | 7,938 | 0.18 | 8,244 | 0.19 | 7,938 | 0.18 | 8,244 | 0.19 |
| 18 | 20,599 | 0.47 | 0 | 5,469 | 0.13 | 5,469 | 0.13 | 5,198 | 0.12 | 5,469 | 0.13 | 5,198 | 0.12 |
| 19 | 32,857 | 0.75 | 0 | 3,869 | 0.09 | 3,673 | 0.08 | 4,024 | 0.09 | 3,673 | 0.08 | 4,024 | 0.09 |
| 20 | 50,412 | 1.16 | 0 | 8,182 | 0.19 | 7,523 | 0.17 | 8,387 | 0.19 | 7,523 | 0.17 | 8,387 | 0.19 |
| 21 | 1,763,594 | 40.49 | 0 | 21,530 | 0.49 | 24,802 | 0.57 | 20,276 | 0.47 | 24,802 | 0.57 | 20,276 | 0.47 |
| 22 | 29,667 | 0.68 | 0 | 4,418 | 0.10 | 4,051 | 0.09 | 4,641 | 0.11 | 4,051 | 0.09 | 4,641 | 0.11 |
| 23 | 25,730 | 0.59 | 0 | 4,103 | 0.09 | 3,769 | 0.09 | 4,255 | 0.10 | 3,769 | 0.09 | 4,255 | 0.10 |
| 24 | 13,027 | 0.30 | 0 | 4,232 | 0.10 | 3,743 | 0.09 | 4,520 | 0.10 | 3,743 | 0.09 | 4,520 | 0.10 |
| 25 | 27,293 | 0.63 | 0 | 4,582 | 0.11 | 4,010 | 0.09 | 4,871 | 0.11 | 4,010 | 0.09 | 4,871 | 0.11 |
| 26 | 32,761 | 0.75 | 0 | 5,446 | 0.13 | 4,687 | 0.11 | 5,783 | 0.13 | 4,687 | 0.11 | 5,783 | 0.13 |
| 27 | 19,732 | 0.45 | 0 | 4,057 | 0.09 | 3,453 | 0.08 | 4,293 | 0.10 | 3,453 | 0.08 | 4,293 | 0.10 |
| 28 | 15,405 | 0.35 | 0 | 5,925 | 0.14 | 6,622 | 0.15 | 5,553 | 0.13 | 6,622 | 0.15 | 5,553 | 0.13 |
| 29 | 10,999 | 0.25 | 0 | 885 | 0.02 | 989 | 0.02 | 833 | 0.02 | 989 | 0.02 | 833 | 0.02 |
| 30 | 45,746 | 1.05 | 0 | 7,002 | 0.16 | 5,794 | 0.13 | 7,421 | 0.17 | 5,794 | 0.13 | 7,421 | 0.17 |
| 31 | 21,712 | 0.50 | 0 | 5,361 | 0.12 | 6,080 | 0.14 | 4,991 | 0.11 | 6,080 | 0.14 | 4,991 | 0.11 |
| 32 | 13,598 | 0.31 | 0 | 5,770 | 0.13 | 6,392 | 0.15 | 5,433 | 0.12 | 6,392 | 0.15 | 5,433 | 0.12 |
| 33 | 32,292 | 0.74 | 0 | 4,576 | 0.11 | 3,685 | 0.08 | 4,827 | 0.11 | 3,685 | 0.08 | 4,827 | 0.11 |
| 34 | 12,352 | 0.28 | 0 | 4,953 | 0.11 | 5,519 | 0.13 | 4,648 | 0.11 | 5,519 | 0.13 | 4,648 | 0.11 |
| 35 | 24,156 | 0.55 | 0 | 2,929 | 0.07 | 2,101 | 0.05 | 3,158 | 0.07 | 2,101 | 0.05 | 3,158 | 0.07 |
| 36 | 48,149 | 1.11 | 0 | 3,630 | 0.08 | 4,040 | 0.09 | 3,329 | 0.08 | 4,040 | 0.09 | 3,329 | 0.08 |
| 37 | 20,287 | 0.47 | 0 | 6,887 | 0.16 | 7,676 | 0.18 | 6,444 | 0.15 | 7,676 | 0.18 | 6,444 | 0.15 |
| 38 | 13,366 | 0.31 | 0 | 4,411 | 0.10 | 4,907 | 0.11 | 4,115 | 0.09 | 4,907 | 0.11 | 4,115 | 0.09 |
| 39 | 6,838 | 0.16 | 0 | 6,838 | 0.16 | 6,838 | 0.16 | 6,838 | 0.16 | 6,838 | 0.16 | 6,838 | 0.16 |
| 40 | 65,678 | 1.51 | 0 | 11,923 | 0.27 | 13,203 | 0.30 | 11,903 | 0.27 | 13,203 | 0.30 | 11,903 | 0.27 |
| 41 | 6,002 | 0.14 | 0 | 1,270 | 0.03 | 177 | 0.00 | 1,315 | 0.03 | 177 | 0.00 | 1,315 | 0.03 |
| 42 | 7,385 | 0.17 | 0 | 2,935 | 0.07 | 2,060 | 0.05 | 3,051 | 0.07 | 2,060 | 0.05 | 3,051 | 0.07 |
| 43 | 1,613 | 0.04 | 0 | 952 | 0.02 | 707 | 0.02 | 1,018 | 0.02 | 707 | 0.02 | 1,018 | 0.02 |
| 44 | 22,981 | 0.53 | 0 | 2,966 | 0.07 | 3,411 | 0.08 | 2,654 | 0.06 | 3,411 | 0.08 | 2,654 | 0.06 |
| 45 | 20,891 | 0.48 | 0 | 5,165 | 0.12 | 4,139 | 0.10 | 5,344 | 0.12 | 4,139 | 0.10 | 5,344 | 0.12 |
| 46 | 23,594 | 0.54 | 0 | 4,999 | 0.11 | 5,754 | 0.13 | 4,442 | 0.10 | 5,754 | 0.13 | 4,442 | 0.10 |
| 47 | 29,591 | 0.68 | 0 | 9,197 | 0.21 | 6,772 | 0.16 | 9,848 | 0.23 | 7,389 | 0.17 | 9,848 | 0.23 |
| 48 | 108,361 | 2.49 | 0 | 5,100 | 0.12 | 5,647 | 0.13 | 3,761 | 0.09 | 5,647 | 0.13 | 3,761 | 0.09 |
| 49 | 20,127 | 0.46 | 0 | 4,158 | 0.10 | 2,652 | 0.06 | 4,435 | 0.10 | 3,324 | 0.08 | 4,435 | 0.10 |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  | SEGMENT 1-US 19 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 4 |  | ALT 5 |  | ALT 6 |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| 51 | 19,640 | 0.45 | 0 | 8,167 | 0.19 | 8,899 | 0.20 | 6,327 | 0.15 | 8,899 | 0.20 | 6,327 | 0.15 |
| 52 | 72,204 | 1.66 | 0 | 9,978 | 0.23 | 4,768 | 0.11 | 10,666 | 0.24 | 7,901 | 0.18 | 10,666 | 0.24 |
| 53 | 18,333 | 0.42 | 0 | 2,121 | 0.05 | 2,498 | 0.06 | 1,273 | 0.03 | 2,498 | 0.06 | 1,273 | 0.03 |
| 54 | 7,523 | 0.17 | 0 | 3,375 | 0.08 | 1,484 | 0.03 | 4,155 | 0.10 | 1,974 | 0.05 | 4,155 | 0.10 |
| 55 | 25,440 | 0.58 | 0 | 5,095 | 0.12 | 2,493 | 0.06 | 5,550 | 0.13 | 2,493 | 0.06 | 5,550 | 0.13 |
| 56 | 6,009 | 0.14 | 0 | 2,296 | 0.05 | 1,011 | 0.02 | 2,501 | 0.06 | 1,325 | 0.03 | 2,501 | 0.06 |
| 57 | 24,733 | 0.57 | 0 | 3,953 | 0.09 | 1,782 | 0.04 | 4,303 | 0.10 | 2,291 | 0.05 | 4,303 | 0.10 |
| 58 | 41,925 | 0.96 | 0 | 21,194 | 0.49 | 24,508 | 0.56 | 17,437 | 0.40 | 24,508 | 0.56 | 17,437 | 0.40 |
| 59 | 9,768 | 0.22 | 0 | 4,149 | 0.10 | 1,839 | 0.04 | 4,523 | 0.10 | 2,391 | 0.05 | 4,523 | 0.10 |
| 60 | 28,242 | 0.65 | 0 | 12,007 | 0.28 | 5,335 | 0.12 | 13,076 | 0.30 | 6,947 | 0.16 | 13,076 | 0.30 |
| 61 | 8,971 | 0.21 | 0 | 3,721 | 0.09 | 1,266 | 0.03 | 4,054 | 0.09 | 1,856 | 0.04 | 4,054 | 0.09 |
| 62 | 3,134 | 0.07 | 0 | 1,299 | 0.03 | 544 | 0.01 | 1,415 | 0.03 | 751 | 0.02 | 1,415 | 0.03 |
| 63 | 5,421 | 0.12 | 0 | 2,169 | 0.05 | 844 | 0.02 | 2,368 | 0.05 | 1,242 | 0.03 | 2,368 | 0.05 |
| 64 | 27,560 | 0.63 | 0 | 14,768 | 0.34 | 16,769 | 0.38 | 11,863 | 0.27 | 16,769 | 0.38 | 11,863 | 0.27 |
| 65 | 12,242 | 0.28 | 0 | 5,098 | 0.12 | 1,833 | 0.04 | 5,552 | 0.13 | 2,590 | 0.06 | 5,552 | 0.13 |
| 66 | 18,293 | 0.42 | 0 | 7,643 | 0.18 | 3,333 | 0.08 | 8,326 | 0.19 | 4,416 | 0.10 | 4,005 | 0.09 |
| 67 | 19,525 | 0.45 | 0 | 8,145 | 0.19 | 3,423 | 0.08 | 8,874 | 0.20 | 4,704 | 0.11 | 8,874 | 0.20 |
| 68 | 9,114 | 0.21 | 0 | 3,787 | 0.09 | 2,190 | 0.05 | 4,125 | 0.09 | 2,190 | 0.05 | 4,125 | 0.09 |
| 69 | 19,051 | 0.44 | 0 | 7,792 | 0.18 | 3,341 | 0.08 | 8,492 | 0.19 | 4,492 | 0.10 | 8,492 | 0.19 |
| 70 | 11,425 | 0.26 | 0 | 4,814 | 0.11 | 1,979 | 0.05 | 5,237 | 0.12 | 2,800 | 0.06 | 5,237 | 0.12 |
| 71 | 57,111 | 1.31 | 0 | 6,265 | 0.14 | 7,426 | 0.17 | 4,123 | 0.09 | 7,426 | 0.17 | 4,123 | 0.09 |
| 72 | 18,676 | 0.43 | 0 | 7,532 | 0.17 | 3,137 | 0.07 | 8,217 | 0.19 | 4,322 | 0.10 | 8,217 | 0.19 |
| 73 | 70,905 | 1.63 | 0 | 9,968 | 0.23 | 12,011 | 0.28 | 7,997 | 0.18 | 12,011 | 0.28 | 7,997 | 0.18 |
| 74 | 16,833 | 0.39 | 0 | 2,320 | 0.05 | 0 | 0.00 | 1,306 | 0.03 | 405 | 0.01 | 1,306 | 0.03 |
| 75 | 74,857 | 1.72 | 0 | 10,320 | 0.24 | 12,904 | 0.30 | 8,274 | 0.19 | 12,904 | 0.30 | 8,274 | 0.19 |
| 76 | 42,285 | 0.97 | 0 | 31,744 | 0.73 | 14,998 | 0.34 | 27,282 | 0.63 | 14,998 | 0.34 | 27,282 | 0.63 |
| 77 | 17,729 | 0.41 | 0 | 728 | 0.02 | 1,146 | 0.03 | 652 | 0.01 | 1,146 | 0.03 | 652 | 0.01 |
| 78 | 28,528 | 0.65 | 0 | 2,795 | 0.06 | 5,356 | 0.12 | 3,772 | 0.09 | 5,356 | 0.12 | 3,772 | 0.09 |
| 79 | 62,261 | 1.43 | 0 | 9,818 | 0.23 | 14,189 | 0.33 | 9,848 | 0.23 | 14,189 | 0.33 | 9,848 | 0.23 |
| 80 | 27,540 | 0.63 | 0 | 5,486 | 0.13 | 6,677 | 0.15 | 4,621 | 0.11 | 6,677 | 0.15 | 4,621 | 0.11 |
| 81 | 82,344 | 1.89 | 0 | 5,401 | 0.12 | 6,509 | 0.15 | 4,548 | 0.10 | 6,509 | 0.15 | 4,548 | 0.10 |
| 82 | 36,454 | 0.84 | 0 | 24,550 | 0.56 | 11,195 | 0.26 | 20,696 | 0.48 | 11,195 | 0.26 | 20,696 | 0.48 |
| 83 | 33,431 | 0.77 | 0 | 6,134 | 0.14 | 7,383 | 0.17 | 5,159 | 0.12 | 7,383 | 0.17 | 5,159 | 0.12 |
| 84 | 3,218 | 0.07 | 0 | 3,001 | 0.07 | 3,218 | 0.07 | 2,104 | 0.05 | 3,218 | 0.07 | 2,104 | 0.05 |
| 85 | 31,639 | 0.73 | 0 | 10,029 | 0.23 | 8,334 | 0.19 | 7,214 | 0.17 | 10,393 | 0.24 | 7,214 | 0.17 |
| 86 | 23,802 | 0.55 | 0 | 3,087 | 0.07 | 0 | 0.00 | 1,434 | 0.03 | 0 | 0.00 | 1,434 | 0.03 |
| 87 | 30,720 | 0.71 | 0 | 10,250 | 0.24 | 4,442 | 0.10 | 10,573 | 0.24 | 4,442 | 0.10 | 10,573 | 0.24 |
| 88 | 11,064 | 0.25 | 0 | 4,805 | 0.11 | 4,257 | 0.10 | 4,195 | 0.10 | 6,512 | 0.15 | 4,195 | 0.10 |
| 89 | 32,338 | 0.74 | 0 | 4,479 | 0.10 | 3,925 | 0.09 | 3,839 | 0.09 | 5,899 | 0.14 | 3,839 | 0.09 |
| 90 | 18,524 | 0.43 | 0 | 6,460 | 0.15 | 2,784 | 0.06 | 6,623 | 0.15 | 2,784 | 0.06 | 6,623 | 0.15 |
| 91 | 3,960 | 0.09 | 0 | 1,261 | 0.03 | 504 | 0.01 | 1,276 | 0.03 | 504 | 0.01 | 1,276 | 0.03 |
| 92 | 39,090 | 0.90 | 0 | 5,455 | 0.13 | 4,828 | 0.11 | 4,675 | 0.11 | 7,250 | 0.17 | 4,675 | 0.11 |
| 93 | 16,953 | 0.39 | 0 | 5,335 | 0.12 | 1,547 | 0.04 | 5,510 | 0.13 | 1,547 | 0.04 | 5,510 | 0.13 |
| 94 | 35,821 | 0.82 | 0 | 5,161 | 0.12 | 6,922 | 0.16 | 4,424 | 0.10 | 6,922 | 0.16 | 4,424 | 0.10 |
| 95 | 134,122 | 3.08 | 0 | 4,818 | 0.11 | 177 | 0.00 | 5,039 | 0.12 | 177 | 0.00 | 5,039 | 0.12 |
| 96 | 18,737 | 0.43 | 0 | 4,434 | 0.10 | 6,009 | 0.14 | 3,792 | 0.09 | 6,009 | 0.14 | 3,792 | 0.09 |
| 97 | 23,276 | 0.53 | 0 | 5,682 | 0.13 | 7,716 | 0.18 | 4,257 | 0.10 | 7,716 | 0.18 | 4,257 | 0.10 |
| 98 | 22,211 | 0.51 | 0 | 7,965 | 0.18 | 10,680 | 0.25 | 5,432 | 0.12 | 10,680 | 0.25 | 5,432 | 0.12 |
| 99 | 56,899 | 1.31 | 0 | 24,423 | 0.56 | 8,152 | 0.19 | 21,863 | 0.50 | 8,152 | 0.19 | 44 | 0.00 |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  | SEGMENT 1-US 19 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 4 |  | ALT 5 |  | ALT 6 |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 100 | 55,870 | 1.28 | 0 | 8,434 | 0.19 | 10,617 | 0.24 | 4,762 | 0.11 | 10,617 | 0.24 | 0 | 0.00 |
| 101 | 66,865 | 1.54 | 0 | 12,371 | 0.28 | 12,374 | 0.28 | 4,315 | 0.10 | 12,374 | 0.28 | 0 | 0.00 |
| 102 | 20,145 | 0.46 | 0 | 4,855 | 0.11 | 1,183 | 0.03 | 3,741 | 0.09 | 1,183 | 0.03 | 3,741 | 0.09 |
| 103 | 46,567 | 1.07 | 0 | 7,036 | 0.16 | 3,828 | 0.09 | 5,940 | 0.14 | 3,828 | 0.09 | 0 | 0.00 |
| 104 | 40,279 | 0.92 | 0 | 5,462 | 0.13 | 4,480 | 0.10 | 446 | 0.01 | 4,480 | 0.10 | 446 | 0.01 |
| 105 | 39,490 | 0.91 | 0 | 4,882 | 0.11 | 5,700 | 0.13 | 2,444 | 0.06 | 5,700 | 0.13 | 0 | 0.00 |
| 106 | 16,441 | 0.38 | 0 | 5,461 | 0.13 | 15,531 | 0.36 | 31,078 | 0.71 | 19,271 | 0.44 | 33,240 | 0.76 |
| 107 | 37,932 | 0.87 | 0 | 8,694 | 0.20 | 48,717 | 1.12 | 32,363 | 0.74 | 51,515 | 1.18 | 40,808 | 0.94 |
| 108 | 87,111 | 2.00 | 0 | 10,765 | 0.25 | 26,317 | 0.60 | 51,631 | 1.19 | 28,766 | 0.66 | 52,160 | 1.20 |
| 109 | 23,375 | 0.54 | 0 | 5,655 | 0.13 | 34,391 | 0.79 | 19,544 | 0.45 | 36,619 | 0.84 | 22,264 | 0.51 |
| 110 | 1,781,896 | 40.91 | 0 | 14,520 | 0.33 | 17,970 | 0.41 | 3,731 | 0.09 | 17,970 | 0.41 | 3,731 | 0.09 |
| 111 | 307,027 | 7.05 | 0 | 36,019 | 0.83 | 14,943 | 0.34 | 30,199 | 0.69 | 14,943 | 0.34 | 30,199 | 0.69 |
| 112 | 420,317 | 9.65 | 0 | 19,046 | 0.44 | 52,219 | 1.20 | 11,256 | 0.26 | 51,401 | 1.18 | 40,946 | 0.94 |
| 113 | 313,100 | 7.19 | 0 | 49,948 | 1.15 | 15,658 | 0.36 | 47,361 | 1.09 | 15,658 | 0.36 | 47,361 | 1.09 |
| 114 | 161,915 | 3.72 | 0 | 17,983 | 0.41 | 31,867 | 0.73 | 11,383 | 0.26 | 35,719 | 0.82 | 22,216 | 0.51 |
| 115 | 122,175 | 2.80 | 0 | 16,293 | 0.37 | 15,926 | 0.37 | 10,306 | 0.24 | 15,926 | 0.37 | 10,306 | 0.24 |
| 116 | 25,037 | 0.57 | 0 | 16,255 | 0.37 | 18,979 | 0.44 | 14,145 | 0.32 | 18,979 | 0.44 | 14,145 | 0.32 |
| 117 | 7,638 | 0.18 | 0 | 2,695 | 0.06 | 1,678 | 0.04 | 1,856 | 0.04 | 1,678 | 0.04 | 1,856 | 0.04 |
| 118 | 6,385 | 0.15 | 0 | 2,560 | 0.06 | 1,653 | 0.04 | 2,031 | 0.05 | 1,653 | 0.04 | 2,031 | 0.05 |
| 119 | 39,761 | 0.91 | 0 | 19,981 | 0.46 | 21,257 | 0.49 | 10,006 | 0.23 | 21,257 | 0.49 | 10,006 | 0.23 |
| 120 | 18,225 | 0.42 | 0 | 4,599 | 0.11 | 2,945 | 0.07 | 4,223 | 0.10 | 2,945 | 0.07 | 4,223 | 0.10 |
| 121 | 10,554 | 0.24 | 0 | 2,487 | 0.06 | 1,607 | 0.04 | 2,615 | 0.06 | 1,607 | 0.04 | 2,615 | 0.06 |
| 122 | 8,868 | 0.20 | 0 | 2,217 | 0.05 | 1,508 | 0.03 | 2,655 | 0.06 | 1,508 | 0.03 | 2,655 | 0.06 |
| 123 | 8,214 | 0.19 | 0 | 2,158 | 0.05 | 1,554 | 0.04 | 2,850 | 0.07 | 1,554 | 0.04 | 2,850 | 0.07 |
| 124 | 9,532 | 0.22 | 0 | 2,197 | 0.05 | 1,615 | 0.04 | 3,031 | 0.07 | 1,615 | 0.04 | 3,031 | 0.07 |
| 125 | 9,329 | 0.21 | 0 | 1,943 | 0.04 | 1,404 | 0.03 | 2,768 | 0.06 | 1,404 | 0.03 | 2,768 | 0.06 |
| 126 | 7,927 | 0.18 | 0 | 2,325 | 0.05 | 1,681 | 0.04 | 3,319 | 0.08 | 1,681 | 0.04 | 3,319 | 0.08 |
| 127 | 84,442 | 1.94 | 0 | 14,586 | 0.33 | 18,689 | 0.43 | 7,730 | 0.18 | 18,689 | 0.43 | 7,730 | 0.18 |
| 128 | 8,814 | 0.20 | 0 | 4,099 | 0.09 | 2,841 | 0.07 | 5,806 | 0.13 | 2,841 | 0.07 | 5,806 | 0.13 |
| 129 | 5,435 | 0.12 | 0 | 899 | 0.02 | 1,164 | 0.03 | 477 | 0.01 | 1,164 | 0.03 | 477 | 0.01 |
| 130 | 19,862 | 0.46 | 0 | 3,414 | 0.08 | 1,161 | 0.03 | 6,593 | 0.15 | 1,161 | 0.03 | 6,593 | 0.15 |
| 131 | 19,963 | 0.46 | 0 | 10,617 | 0.24 | 9,356 | 0.21 | 3,787 | 0.09 | 9,356 | 0.21 | 3,787 | 0.09 |
| 132 | 36,337 | 0.83 | 0 | 10,663 | 0.24 | 13,766 | 0.32 | 5,888 | 0.14 | 13,766 | 0.32 | 5,888 | 0.14 |
| 133 | 60,442 | 1.39 | 0 | 20,963 | 0.48 | 13,583 | 0.31 | 27,890 | 0.64 | 13,583 | 0.31 | 27,890 | 0.64 |
| 134 | 168,470 | 3.87 | 0 | 25,787 | 0.59 | 35,428 | 0.81 | 6,162 | 0.14 | 35,428 | 0.81 | 6,162 | 0.14 |
| 135 | 67,630 | 1.55 | 0 | 26,417 | 0.61 | 12,915 | 0.30 | 38,855 | 0.89 | 12,915 | 0.30 | 40,511 | 0.93 |
| 136 | 639,697 | 14.69 | 0 | 39,839 | 0.91 | 53,650 | 1.23 | 12,096 | 0.28 | 53,650 | 1.23 | 12,096 | 0.28 |
| 137 | 47,314 | 1.09 | 0 | 11,737 | 0.27 | 16,263 | 0.37 | 4,229 | 0.10 | 16,263 | 0.37 | 4,229 | 0.10 |
| 138 | 36,358 | 0.83 | 0 | 16,011 | 0.37 | 6,152 | 0.14 | 18,417 | 0.42 | 6,152 | 0.14 | 18,417 | 0.42 |
| 139 | 144,713 | 3.32 | 0 | 14,878 | 0.34 | 5,689 | 0.13 | 17,058 | 0.39 | 5,689 | 0.13 | 17,058 | 0.39 |
| 140 | 17,839 | 0.41 | 0 | 7,187 | 0.16 | 10,040 | 0.23 | 1,963 | 0.05 | 10,040 | 0.23 | 1,963 | 0.05 |
| 141 | 19,633 | 0.45 | 0 | 5,396 | 0.12 | 1,993 | 0.05 | 6,078 | 0.14 | 1,993 | 0.05 | 6,078 | 0.14 |
| 142 | 42,788 | 0.98 | 0 | 10,845 | 0.25 | 3,966 | 0.09 | 12,416 | 0.29 | 3,966 | 0.09 | 12,416 | 0.29 |
| 143 | 25,316 | 0.58 | 0 | 15,169 | 0.35 | 17,860 | 0.41 | 5,972 | 0.14 | 17,860 | 0.41 | 5,972 | 0.14 |
| 144 | 12,375 | 0.28 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 145 | 46,935 | 1.08 | 0 | 1,345 | 0.03 | 4,128 | 0.09 | 0 | 0.00 | 4,128 | 0.09 | 0 | 0.00 |
| 146 | 152,391 | 3.50 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 147 | 417,166 | 9.58 | 0 | 22,369 | 0.51 | 4,980 | 0.11 | 16,634 | 0.38 | 4,980 | 0.11 | 16,634 | 0.38 |
| 148 | 14,899 | 0.34 | 0 | 2,588 | 0.06 | 3,350 | 0.08 | 803 | 0.02 | 3,350 | 0.08 | 803 | 0.02 |
| 149 | 44,434 | 1.02 | 0 | 5,980 | 0.14 | 8,244 | 0.19 | 1,418 | 0.03 | 8,244 | 0.19 | 1,418 | 0.03 |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  | SEGMENT 1 - US 19 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 4 |  | ALT 5 |  | ALT 6 |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 150 | 88,511 | 2.03 | 0 | 65,461 | 1.50 | 17,196 | 0.39 | 59,093 | 1.36 | 17,196 | 0.39 | 59,093 | 1.36 |
| 151 | 26,697 | 0.61 | 0 | 4,023 | 0.09 | 5,198 | 0.12 | 681 | 0.02 | 5,198 | 0.12 | 681 | 0.02 |
| 152 | 11,689 | 0.27 | 0 | 2,117 | 0.05 | 2,669 | 0.06 | 12 | 0.00 | 2,669 | 0.06 | 12 | 0.00 |
| 153 | 7,350 | 0.17 | 0 | 1,596 | 0.04 | 2,012 | 0.05 | 0 | 0.00 | 2,012 | 0.05 | 0 | 0.00 |
| 154 | 13,426 | 0.31 | 0 | 3,240 | 0.07 | 4,097 | 0.09 | 0 | 0.00 | 4,097 | 0.09 | 0 | 0.00 |
| 155 | 7,102 | 0.16 | 0 | 2,004 | 0.05 | 2,427 | 0.06 | 0 | 0.00 | 2,427 | 0.06 | 0 | 0.00 |
| 156 | 6,615 | 0.15 | 0 | 2,074 | 0.05 | 2,548 | 0.06 | 0 | 0.00 | 2,548 | 0.06 | 0 | 0.00 |
| 157 | 3,510 | 0.08 | 0 | 1,682 | 0.04 | 2,048 | 0.05 | 0 | 0.00 | 2,048 | 0.05 | 0 | 0.00 |
| 158 | 2,015 | 0.05 | 0 | 1,609 | 0.04 | 1,881 | 0.04 | 0 | 0.00 | 1,881 | 0.04 | 0 | 0.00 |
| 159 | 1,467 | 0.03 | 0 | 1,467 | 0.03 | 1,467 | 0.03 | 0 | 0.00 | 1,467 | 0.03 | 0 | 0.00 |
| 160 | 29,701 | 0.68 | 0 | 3,407 | 0.08 | 2,424 | 0.06 | 4,103 | 0.09 | 2,424 | 0.06 | 4,103 | 0.09 |
| 161 | 779 | 0.02 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 162 | 1,195 | 0.03 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 163 | 2,202 | 0.05 | 0 | 101 | 0.00 | 503 | 0.01 | 0 | 0.00 | 503 | 0.01 | 0 | 0.00 |
| 164 | 3,056 | 0.07 | 0 | 1,503 | 0.03 | 2,065 | 0.05 | 0 | 0.00 | 2,065 | 0.05 | 0 | 0.00 |
| 165 | 3,475 | 0.08 | 0 | 2,010 | 0.05 | 2,635 | 0.06 | 0 | 0.00 | 2,635 | 0.06 | 0 | 0.00 |
| 166 | 35,917 | 0.82 | 0 | 0 | 0.00 | 822 | 0.02 | 0 | 0.00 | 822 | 0.02 | 0 | 0.00 |
| 167 | 12,083 | 0.28 | 0 | 10,411 | 0.24 | 11,660 | 0.27 | 601 | 0.01 | 11,660 | 0.27 | 1,742 | 0.04 |
| 168 | 43,012 | 0.99 | 0 | 8,458 | 0.19 | 4,255 | 0.10 | 14,007 | 0.32 | 4,255 | 0.10 | 14,007 | 0.32 |
| 169 | 8,134 | 0.19 | 0 | 3,284 | 0.08 | 1,699 | 0.04 | 4,724 | 0.11 | 1,699 | 0.04 | 4,724 | 0.11 |
| 170 | 473,331 | 10.87 | 0 | 37,824 | 0.87 | 16,587 | 0.38 | 51,652 | 1.19 | 16,587 | 0.38 | 51,652 | 1.19 |
| 171 | 16,860 | 0.39 | 0 | 0 | 0.00 | 2,367 | 0.05 | 0 | 0.00 | 2,367 | 0.05 | 0 | 0.00 |
| 172 | 7,875 | 0.18 | 0 | 0 | 0.00 | 1,244 | 0.03 | 0 | 0.00 | 1,244 | 0.03 | 0 | 0.00 |
| 173 | 1,631 | 0.04 | 0 | 1,631 | 0.04 | 1,631 | 0.04 | 496 | 0.01 | 1,631 | 0.04 | 1,742 | 0.04 |
| 174 | 5,573 | 0.13 | 0 | 0 | 0.00 | 675 | 0.02 | 0 | 0.00 | 675 | 0.02 | 0 | 0.00 |
| 175 | 12,003 | 0.28 | 0 | 0 | 0.00 | 3,265 | 0.07 | 0 | 0.00 | 3,265 | 0.07 | 0 | 0.00 |
| 176 | 8,296 | 0.19 | 0 | 8,296 | 0.19 | 8,296 | 0.19 | 2,824 | 0.06 | 8,296 | 0.19 | 7,405 | 0.17 |
| 177 | 17,356 | 0.40 | 0 | 0 | 0.00 | 3,298 | 0.08 | 0 | 0.00 | 3,298 | 0.08 | 0 | 0.00 |
| 178 | 17,136 | 0.39 | 0 | 0 | 0.00 | 2,982 | 0.07 | 0 | 0.00 | 2,982 | 0.07 | 0 | 0.00 |
| 179 | 29,817 | 0.68 | 0 | 7,031 | 0.16 | 3,604 | 0.08 | 9,341 | 0.21 | 3,604 | 0.08 | 9,341 | 0.21 |
| 180 | 19,018 | 0.44 | 0 | 12,643 | 0.29 | 15,082 | 0.35 | 3,060 | 0.07 | 15,082 | 0.35 | 7,405 | 0.17 |
| 181 | 3,867 | 0.09 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 182 | 8,113 | 0.19 | 0 | 1,955 | 0.04 | 1,074 | 0.02 | 2,406 | 0.06 | 1,074 | 0.02 | 2,406 | 0.06 |
| 183 | 9,351 | 0.21 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 184 | 79,156 | 1.82 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 185 | 69,758 | 1.60 | 0 | 22,370 | 0.51 | 14,920 | 0.34 | 28,061 | 0.64 | 14,920 | 0.34 | 28,061 | 0.64 |
| 186 | 7,406 | 0.17 | 0 | 4,111 | 0.09 | 5,201 | 0.12 | 1,005 | 0.02 | 5,201 | 0.12 | 2,614 | 0.06 |
| 187 | 868,140 | 19.93 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 188 | 9,780 | 0.22 | 0 | 5,664 | 0.13 | 7,185 | 0.16 | 1,483 | 0.03 | 7,185 | 0.16 | 3,485 | 0.08 |
| 189 | 11,786 | 0.27 | 0 | 6,117 | 0.14 | 4,123 | 0.09 | 8,643 | 0.20 | 4,123 | 0.09 | 8,643 | 0.20 |
| 190 | 1,894 | 0.04 | 0 | 1,894 | 0.04 | 1,894 | 0.04 | 1,899 | 0.04 | 1,894 | 0.04 | 1,899 | 0.04 |
| 191 | 18,711 | 0.43 | 0 | 7,067 | 0.16 | 9,066 | 0.21 | 1,827 | 0.04 | 9,066 | 0.21 | 4,792 | 0.11 |
| 192 | 23,617 | 0.54 | 0 | 14,534 | 0.33 | 7,181 | 0.16 | 16,290 | 0.37 | 7,181 | 0.16 | 16,290 | 0.37 |
| 193 | 24,924 | 0.57 | 0 | 5,792 | 0.13 | 7,134 | 0.16 | 2,198 | 0.05 | 7,134 | 0.16 | 3,920 | 0.09 |
| 194 | 14,221 | 0.33 | 0 | 6,453 | 0.15 | 8,089 | 0.19 | 2,719 | 0.06 | 8,089 | 0.19 | 4,356 | 0.10 |
| 195 | 41,569 | 0.95 | 0 | 9,912 | 0.23 | 11,570 | 0.27 | 4,638 | 0.11 | 11,570 | 0.27 | 6,970 | 0.16 |
| 196 | 17,464 | 0.40 | 0 | 7,245 | 0.17 | 3,669 | 0.08 | 8,263 | 0.19 | 3,669 | 0.08 | 8,263 | 0.19 |
| 197 | 18,745 | 0.43 | 0 | 5,608 | 0.13 | 2,747 | 0.06 | 6,346 | 0.15 | 2,747 | 0.06 | 6,346 | 0.15 |
| 198 | 11,278 | 0.26 | 0 | 6,597 | 0.15 | 3,148 | 0.07 | 7,157 | 0.16 | 3,148 | 0.07 | 7,157 | 0.16 |
| 199 | 1,388,497 | 31.88 | 0 | 80,215 | 1.84 | 62,431 | 1.43 | 15,466 | 0.36 | 62,431 | 1.43 | 15,466 | 0.36 |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  | SEGMENT 1 - US 19 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 4 |  | ALT 5 |  | ALT 6 |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 200 | 28,437 | 0.65 | 0 | 2,892 | 0.07 | 4,220 | 0.10 | 459 | 0.01 | 4,220 | 0.10 | 1,307 | 0.03 |
| 201 | 9,699 | 0.22 | 0 | 6,691 | 0.15 | 7,642 | 0.18 | 2,644 | 0.06 | 7,642 | 0.18 | 4,792 | 0.11 |
| 202 | 54,568 | 1.25 | 0 | 10,818 | 0.25 | 5,071 | 0.12 | 11,986 | 0.28 | 5,071 | 0.12 | 11,986 | 0.28 |
| 203 | 4,767 | 0.11 | 0 | 4,767 | 0.11 | 4,767 | 0.11 | 3,546 | 0.08 | 4,767 | 0.11 | 4,356 | 0.10 |
| 204 | 60,433 | 1.39 | 0 | 8,228 | 0.19 | 2,953 | 0.07 | 7,785 | 0.18 | 2,953 | 0.07 | 7,785 | 0.18 |
| 205 | 280,552 | 6.44 | 0 | 34,488 | 0.79 | 18,601 | 0.43 | 44,570 | 1.02 | 18,601 | 0.43 | 44,570 | 1.02 |
| 206 | 32,378 | 0.74 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 207 | 84,383 | 1.94 | 0 | 4,900 | 0.11 | 2,428 | 0.06 | 7,515 | 0.17 | 2,428 | 0.06 | 7,515 | 0.17 |
| 208 | 7,779 | 0.18 | 0 | 4,575 | 0.11 | 2,728 | 0.06 | 6,644 | 0.15 | 2,728 | 0.06 | 6,644 | 0.15 |
| 209 | 3,406 | 0.08 | 0 | 3,092 | 0.07 | 1,717 | 0.04 | 3,406 | 0.08 | 1,717 | 0.04 | 3,406 | 0.08 |
| 210 | 108,010 | 2.48 | 0 | 4,503 | 0.10 | 2,571 | 0.06 | 6,755 | 0.16 | 2,571 | 0.06 | 6,755 | 0.16 |
| 211 | 45,397 | 1.04 | 0 | 7,024 | 0.16 | 4,163 | 0.10 | 9,104 | 0.21 | 4,163 | 0.10 | 9,104 | 0.21 |
| 212 | 5,110 | 0.12 | 0 | 843 | 0.02 | 556 | 0.01 | 1,045 | 0.02 | 556 | 0.01 | 1,045 | 0.02 |
| 213 | 47,220 | 1.08 | 0 | 11,087 | 0.25 | 13,594 | 0.31 | 7,429 | 0.17 | 13,594 | 0.31 | 7,429 | 0.17 |
| 214 | 132,360 | 3.04 | 0 | 4,868 | 0.11 | 2,794 | 0.06 | 5,710 | 0.13 | 2,794 | 0.06 | 5,710 | 0.13 |
| 215 | 210,443 | 4.83 | 0 | 19,907 | 0.46 | 18,717 | 0.43 | 20,697 | 0.48 | 18,717 | 0.43 | 20,697 | 0.48 |
| 216 | 86,331 | 1.98 | 0 | 0 | 0.00 | 0 | 0.00 | 164 | 0.00 | 0 | 0.00 | 164 | 0.00 |
| 217 | 13,064 | 0.30 | 0 | 10,651 | 0.24 | 10,534 | 0.24 | 9,315 | 0.21 | 10,534 | 0.24 | 9,315 | 0.21 |
| 218 | 9,101 | 0.21 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 219 | 88,320 | 2.03 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 220 | 17,176 | 0.39 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 221 | 94,288 | 2.16 | 0 | 4,074 | 0.09 | 4,930 | 0.11 | 1,804 | 0.04 | 4,930 | 0.11 | 1,804 | 0.04 |
| 222 | 94,461 | 2.17 | 0 | 15,723 | 0.36 | 10,769 | 0.25 | 23,396 | 0.54 | 10,769 | 0.25 | 23,396 | 0.54 |
| 223 | 967 | 0.02 | 0 | 86 | 0.00 | 105 | 0.00 | 25 | 0.00 | 105 | 0.00 | 25 | 0.00 |
| 224 | 17,254 | 0.40 | 0 | 4,383 | 0.10 | 5,420 | 0.12 | 2,009 | 0.05 | 5,420 | 0.12 | 2,009 | 0.05 |
| 225 | 36,383 | 0.84 | 0 | 2,781 | 0.06 | 6,537 | 0.15 | 1,140 | 0.03 | 6,537 | 0.15 | 1,140 | 0.03 |
| 226 | 39,444 | 0.91 | 0 | 16,645 | 0.38 | 23,261 | 0.53 | 7,525 | 0.17 | 23,261 | 0.53 | 7,525 | 0.17 |
| 227 | 16,194 | 0.37 | 0 | 2,841 | 0.07 | 1,813 | 0.04 | 3,922 | 0.09 | 1,813 | 0.04 | 3,922 | 0.09 |
| 228 | 7,392 | 0.17 | 0 | 7,392 | 0.17 | 4,802 | 0.11 | 7,392 | 0.17 | 4,802 | 0.11 | 7,392 | 0.17 |
| 229 | 144,054 | 3.31 | 0 | 9,172 | 0.21 | 6,217 | 0.14 | 23,550 | 0.54 | 6,217 | 0.14 | 23,550 | 0.54 |
| 230 | 20,678 | 0.47 | 0 | 6,520 | 0.15 | 8,839 | 0.20 | 3,443 | 0.08 | 8,839 | 0.20 | 3,443 | 0.08 |
| 231 | 17,541 | 0.40 | 0 | 5,874 | 0.13 | 10,707 | 0.25 | 3,258 | 0.07 | 10,707 | 0.25 | 3,258 | 0.07 |
| 232 | 43,306 | 0.99 | 0 | 4,231 | 0.10 | 2,813 | 0.06 | 5,902 | 0.14 | 2,813 | 0.06 | 5,902 | 0.14 |
| 233 | 38,649 | 0.89 | 0 | 5,593 | 0.13 | 3,873 | 0.09 | 7,630 | 0.18 | 3,873 | 0.09 | 7,630 | 0.18 |
| 234 | 20,861 | 0.48 | 0 | 7,563 | 0.17 | 13,770 | 0.32 | 4,464 | 0.10 | 13,770 | 0.32 | 4,464 | 0.10 |
| 235 | 53,808 | 1.24 | 0 | 5,182 | 0.12 | 3,551 | 0.08 | 6,964 | 0.16 | 3,551 | 0.08 | 6,964 | 0.16 |
| 236 | 60,944 | 1.40 | 0 | 5,109 | 0.12 | 3,313 | 0.08 | 6,500 | 0.15 | 3,313 | 0.08 | 6,500 | 0.15 |
| 237 | 19,067 | 0.44 | 0 | 6,464 | 0.15 | 10,264 | 0.24 | 3,941 | 0.09 | 10,264 | 0.24 | 3,941 | 0.09 |
| 238 | 78,740 | 1.81 | 0 | 7,890 | 0.18 | 4,804 | 0.11 | 10,093 | 0.23 | 4,804 | 0.11 | 10,093 | 0.23 |
| 239 | 34,922 | 0.80 | 0 | 5,953 | 0.14 | 8,815 | 0.20 | 3,832 | 0.09 | 8,815 | 0.20 | 3,832 | 0.09 |
| 240 | 34,794 | 0.80 | 0 | 3,072 | 0.07 | 1,364 | 0.03 | 4,231 | 0.10 | 1,364 | 0.03 | 4,231 | 0.10 |
| 241 | 142,727 | 3.28 | 0 | 8,366 | 0.19 | 12,289 | 0.28 | 5,222 | 0.12 | 12,289 | 0.28 | 5,222 | 0.12 |
| 242 | 38,423 | 0.88 | 0 | 4,542 | 0.10 | 876 | 0.02 | 7,387 | 0.17 | 876 | 0.02 | 7,387 | 0.17 |
| 243 | 10,506 | 0.24 | 0 | 6,409 | 0.15 | 4,002 | 0.09 | 8,041 | 0.18 | 4,002 | 0.09 | 8,041 | 0.18 |
| 244 | 7,283 | 0.17 | 0 | 5,473 | 0.13 | 3,372 | 0.08 | 6,578 | 0.15 | 3,372 | 0.08 | 6,578 | 0.15 |
| 245 | 176,371 | 4.05 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 246 | 10,281 | 0.24 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 247 | 21,907 | 0.50 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 248 | 24,125 | 0.55 | 0 | 513 | 0.01 | 0 | 0.00 | 1,649 | 0.04 | 0 | 0.00 | 1,649 | 0.04 |
| 249 | 27,113 | 0.62 | 0 | 7,300 | 0.17 | 10,802 | 0.25 | 4,710 | 0.11 | 10,802 | 0.25 | 4,710 | 0.11 |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  | SEGMENT 1-US 19 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 4 |  | ALT 5 |  | ALT 6 |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 250 | 68,919 | 1.58 | 0 | 6,580 | 0.15 | 9,612 | 0.22 | 4,036 | 0.09 | 9,612 | 0.22 | 4,036 | 0.09 |
| 251 | 31,418 | 0.72 | 0 | 7,368 | 0.17 | 10,250 | 0.24 | 4,443 | 0.10 | 10,250 | 0.24 | 4,443 | 0.10 |
| 252 | 33,393 | 0.77 | 0 | 5,646 | 0.13 | 2,870 | 0.07 | 7,912 | 0.18 | 2,870 | 0.07 | 7,912 | 0.18 |
| 253 | 18,536 | 0.43 | 0 | 3,346 | 0.08 | 4,860 | 0.11 | 1,881 | 0.04 | 4,860 | 0.11 | 1,881 | 0.04 |
| 254 | 214,572 | 4.93 | 0 | 20,375 | 0.47 | 27,681 | 0.64 | 9,973 | 0.23 | 27,681 | 0.64 | 9,973 | 0.23 |
| 255 | 38,360 | 0.88 | 0 | 3,077 | 0.07 | 1,718 | 0.04 | 3,390 | 0.08 | 1,718 | 0.04 | 3,390 | 0.08 |
| 256 | 20,406 | 0.47 | 0 | 5,517 | 0.13 | 3,267 | 0.08 | 6,781 | 0.16 | 3,267 | 0.08 | 6,781 | 0.16 |
| 257 | 49,331 | 1.13 | 0 | 10,230 | 0.23 | 5,103 | 0.12 | 12,054 | 0.28 | 5,103 | 0.12 | 12,054 | 0.28 |
| 258 | 38,846 | 0.89 | 0 | 7,445 | 0.17 | 4,248 | 0.10 | 9,902 | 0.23 | 4,248 | 0.10 | 9,902 | 0.23 |
| 259 | 54,979 | 1.26 | 0 | 3,807 | 0.09 | 4,810 | 0.11 | 1,765 | 0.04 | 4,810 | 0.11 | 1,765 | 0.04 |
| 260 | 14,549 | 0.33 | 0 | 1,749 | 0.04 | 1,192 | 0.03 | 3,098 | 0.07 | 1,192 | 0.03 | 3,098 | 0.07 |
| 261 | 14,331 | 0.33 | 0 | 1,635 | 0.04 | 1,193 | 0.03 | 2,938 | 0.07 | 1,193 | 0.03 | 2,938 | 0.07 |
| 262 | 15,700 | 0.36 | 0 | 2,971 | 0.07 | 2,417 | 0.06 | 4,910 | 0.11 | 2,417 | 0.06 | 4,910 | 0.11 |
| 263 | 29,593 | 0.68 | 0 | 7,245 | 0.17 | 8,689 | 0.20 | 3,735 | 0.09 | 8,689 | 0.20 | 3,735 | 0.09 |
| 264 | 9,425 | 0.22 | 0 | 827 | 0.02 | 706 | 0.02 | 1,396 | 0.03 | 706 | 0.02 | 1,396 | 0.03 |
| 265 | 6,120 | 0.14 | 0 | 582 | 0.01 | 483 | 0.01 | 971 | 0.02 | 483 | 0.01 | 971 | 0.02 |
| 266 | 58,012 | 1.33 | 0 | 6,038 | 0.14 | 6,586 | 0.15 | 3,044 | 0.07 | 6,586 | 0.15 | 3,044 | 0.07 |
| 267 | 116,164 | 2.67 | 0 | 9,329 | 0.21 | 9,075 | 0.21 | 14,797 | 0.34 | 9,075 | 0.21 | 14,797 | 0.34 |
| 268 | 114,213 | 2.62 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 269 | 8,375 | 0.19 | 0 | 5,200 | 0.12 | 5,098 | 0.12 | 3,923 | 0.09 | 5,098 | 0.12 | 3,923 | 0.09 |
| 270 | 7,421 | 0.17 | 0 | 2,177 | 0.05 | 1,985 | 0.05 | 1,575 | 0.04 | 1,985 | 0.05 | 1,575 | 0.04 |
| 271 | 8,131 | 0.19 | 0 | 2,835 | 0.07 | 2,540 | 0.06 | 2,136 | 0.05 | 2,540 | 0.06 | 2,136 | 0.05 |
| 272 | 29,833 | 0.68 | 0 | 4,226 | 0.10 | 3,545 | 0.08 | 4,105 | 0.09 | 3,545 | 0.08 | 4,105 | 0.09 |
| 273 | 15,407 | 0.35 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 274 | 22,773 | 0.52 | 0 | 13,687 | 0.31 | 12,419 | 0.29 | 10,944 | 0.25 | 12,419 | 0.29 | 10,944 | 0.25 |
| 275 | 14,639 | 0.34 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 276 | 172,211 | 3.95 | 0 | 27,771 | 0.64 | 30,220 | 0.69 | 29,522 | 0.68 | 30,220 | 0.69 | 29,522 | 0.68 |
| 277 | 8,789 | 0.20 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 278 | 13,703 | 0.31 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 279 | 13,346 | 0.31 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 280 | 99,970 | 2.29 | 0 | 8,509 | 0.20 | 8,200 | 0.19 | 6,815 | 0.16 | 8,200 | 0.19 | 8,276 | 0.19 |
| 281 | 24,746 | 0.57 | 0 | 11,032 | 0.25 | 10,882 | 0.25 | 10,287 | 0.24 | 10,882 | 0.25 | 10,287 | 0.24 |
| 282 | 17,863 | 0.41 | 0 | 851 | 0.02 | 1,951 | 0.04 | 726 | 0.02 | 1,951 | 0.04 | 726 | 0.02 |
| 283 | 126,063 | 2.89 | 0 | 11,771 | 0.27 | 11,114 | 0.26 | 13,364 | 0.31 | 16,117 | 0.37 | 16,553 | 0.38 |
| 284 | 14,999 | 0.34 | 0 | 11,390 | 0.26 | 11,702 | 0.27 | 8,239 | 0.19 | 11,702 | 0.27 | 8,239 | 0.19 |
| 285 | 29,397 | 0.67 | 0 | 0 | 0.00 | 24 | 0.00 | 0 | 0.00 | 24 | 0.00 | 0 | 0.00 |
| 286 | 8,640 | 0.20 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 287 | 15,540 | 0.36 | 0 | 3,883 | 0.09 | 5,619 | 0.13 | 4,304 | 0.10 | 5,619 | 0.13 | 4,304 | 0.10 |
| 288 | 10,196 | 0.23 | 0 | 10,196 | 0.23 | 10,196 | 0.23 | 8,901 | 0.20 | 10,019 | 0.23 | 10,019 | 0.23 |
| 289 | 19,076 | 0.44 | 0 | 2,937 | 0.07 | 4,270 | 0.10 | 3,709 | 0.09 | 4,270 | 0.10 | 3,709 | 0.09 |
| 290 | 29,132 | 0.67 | 0 | 8,820 | 0.20 | 9,068 | 0.21 | 8,249 | 0.19 | 9,068 | 0.21 | 8,249 | 0.19 |
| 291 | 9,127 | 0.21 | 0 | 6,462 | 0.15 | 7,518 | 0.17 | 7,314 | 0.17 | 7,841 | 0.18 | 9,148 | 0.21 |
| 292 | 754 | 0.02 | 0 | 476 | 0.01 | 567 | 0.01 | 502 | 0.01 | 567 | 0.01 | 871 | 0.02 |
| 293 | 5,089 | 0.12 | 0 | 2,341 | 0.05 | 2,791 | 0.06 | 2,407 | 0.06 | 2,791 | 0.06 | 3,049 | 0.07 |
| 294 | 20,209 | 0.46 | 0 | 8,976 | 0.21 | 9,017 | 0.21 | 8,227 | 0.19 | 9,017 | 0.21 | 8,227 | 0.19 |
| 295 | 12,826 | 0.29 | 0 | 4,921 | 0.11 | 5,707 | 0.13 | 5,031 | 0.12 | 5,707 | 0.13 | 5,227 | 0.12 |
| 296 | 17,269 | 0.40 | 0 | 4,600 | 0.11 | 5,546 | 0.13 | 4,797 | 0.11 | 5,546 | 0.13 | 4,797 | 0.11 |
| 297 | 20,882 | 0.48 | 0 | 7,729 | 0.18 | 7,381 | 0.17 | 6,798 | 0.16 | 7,381 | 0.17 | 6,798 | 0.16 |
| 298 | 12,943 | 0.30 | 0 | 2,942 | 0.07 | 3,575 | 0.08 | 3,122 | 0.07 | 3,575 | 0.08 | 3,122 | 0.07 |
| 299 | 17,870 | 0.41 | 0 | 3,252 | 0.07 | 3,869 | 0.09 | 3,442 | 0.08 | 3,869 | 0.09 | 3,442 | 0.08 |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  | SEGMENT 1 - US 19 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 4 |  | ALT 5 |  | ALT 6 |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 300 | 9,751 | 0.22 | 0 | 3,923 | 0.09 | 3,069 | 0.07 | 2,848 | 0.07 | 3,069 | 0.07 | 2,848 | 0.07 |
| 301 | 8,431 | 0.19 | 0 | 3,093 | 0.07 | 2,455 | 0.06 | 2,273 | 0.05 | 2,455 | 0.06 | 2,273 | 0.05 |
| 302 | 16,084 | 0.37 | 0 | 5,416 | 0.12 | 6,468 | 0.15 | 5,672 | 0.13 | 6,468 | 0.15 | 5,672 | 0.13 |
| 303 | 12,348 | 0.28 | 0 | 7,655 | 0.18 | 8,689 | 0.20 | 7,428 | 0.17 | 8,689 | 0.20 | 7,428 | 0.17 |
| 304 | 45,215 | 1.04 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 305 | 8,298 | 0.19 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 306 | 45,892 | 1.05 | 0 | 6,485 | 0.15 | 6,583 | 0.15 | 5,749 | 0.13 | 6,583 | 0.15 | 5,749 | 0.13 |
| 307 | 4,776 | 0.11 | 0 | 4,776 | 0.11 | 4,776 | 0.11 | 4,776 | 0.11 | 4,776 | 0.11 | 4,776 | 0.11 |
| 308 | 13,145 | 0.30 | 0 | 2,957 | 0.07 | 3,465 | 0.08 | 3,077 | 0.07 | 3,465 | 0.08 | 3,077 | 0.07 |
| 309 | 24,975 | 0.57 | 0 | 5,424 | 0.12 | 6,298 | 0.14 | 5,676 | 0.13 | 6,298 | 0.14 | 5,676 | 0.13 |
| 310 | 11,420 | 0.26 | 0 | 3,277 | 0.08 | 3,778 | 0.09 | 3,263 | 0.07 | 3,778 | 0.09 | 3,263 | 0.07 |
| 311 | 36,620 | 0.84 | 0 | 11,087 | 0.25 | 10,133 | 0.23 | 11,804 | 0.27 | 10,133 | 0.23 | 11,804 | 0.27 |
| 312 | 47,924 | 1.10 | 0 | 1,087 | 0.02 | 1,316 | 0.03 | 1,072 | 0.02 | 1,316 | 0.03 | 1,072 | 0.02 |
| 313 | 30,377 | 0.70 | 0 | 7,297 | 0.17 | 6,802 | 0.16 | 6,794 | 0.16 | 6,802 | 0.16 | 6,794 | 0.16 |
| 314 | 73,136 | 1.68 | 0 | 6,793 | 0.16 | 6,975 | 0.16 | 6,246 | 0.14 | 6,975 | 0.16 | 6,246 | 0.14 |
| 315 | NOT US | ED |  |  |  | T USED |  |  |  |  | NOT |  |  |
| 316 | 8,821 | 0.20 | 0 | 2,848 | 0.07 | 2,290 | 0.05 | 1,526 | 0.04 | 2,290 | 0.05 | 1,526 | 0.04 |
| 317 | 9,443 | 0.22 | 0 | 3,094 | 0.07 | 1,241 | 0.03 | 1,259 | 0.03 | 1,241 | 0.03 | 1,259 | 0.03 |
| 318 | 37,950 | 0.87 | 0 | 410 | 0.01 | 143 | 0.00 | 644 | 0.01 | 143 | 0.00 | 644 | 0.01 |
| 319 | 9,983 | 0.23 | 0 | 0 | 0.00 | 0 | 0.00 | 70 | 0.00 | 0 | 0.00 | 70 | 0.00 |
| 320 | 9,321 | 0.21 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 321 | 7,790 | 0.18 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 322 | 8,950 | 0.21 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 323 | 41,078 | 0.94 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 324 | 8,223 | 0.19 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 325 | 9,295 | 0.21 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 326 | 8,449 | 0.19 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 327 | 245,822 | 5.64 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 328 | 101,519 | 2.33 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 329 | 40,912 | 0.94 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 330 | 49,239 | 1.13 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 331 | 55,777 | 1.28 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 332 | 15,189 | 0.35 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 333 | 44,193 | 1.01 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 334 | NOT US | ED |  |  |  | T USED |  |  |  |  | NOT |  |  |
| 335 | NOT US | ED |  |  |  | T USED |  |  |  |  | NOT |  |  |
| 336 | 210,073 | 4.82 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 337 | 35,504 | 0.82 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 338 | 4,039 | 0.09 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 339 | 812,061 | 18.64 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 340 | 12,089 | 0.28 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 341 | 95,837 | 2.20 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 342 | 32,733 | 0.75 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 343 | 197,842 | 4.54 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 344 | 928,794 | 21.32 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 345 | 28,992 | 0.67 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 346 | 1,228,222 | 28.20 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 347 | 78,814 | 1.81 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 348 | 28,910 | 0.66 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 349 | 485,404 | 11.14 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  | SEGMENT 1 - US 19 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 4 |  | ALT 5 |  | ALT 6 |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 350 | 1,330,124 | 30.54 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 351 | 223,558 | 5.13 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 352 | 2,002,822 | 45.98 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 353 | 5,411 | 0.12 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 354 | 167,690 | 3.85 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 355 | 81,889 | 1.88 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 356 | 87,017 | 2.00 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 357 | 11,875 | 0.27 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 358 | 52,359 | 1.20 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 359 | 16,732 | 0.38 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 360 | 23,772 | 0.55 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 361 | 19,930 | 0.46 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 362 | 82,339 | 1.89 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 363 | 6,283 | 0.14 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 364 | 70,180 | 1.61 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 365 | 15,996 | 0.37 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 366 | 15,438 | 0.35 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 367 | 264,367 | 6.07 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 368 | 21,225 | 0.49 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 369 | 299,554 | 6.88 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 370 | 415,715 | 9.54 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 371 | 1,951,583 | 44.80 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 372 | 1,992,770 | 45.75 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 373 | 1,273,757 | 29.24 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 374 | 27,955,462 | 641.77 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 375 | 458,047 | 10.52 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 376 | 1,496,029 | 34.34 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 377 | 4,248,452 | 97.53 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 378 | 15,324 | 0.35 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 379 | 305,933 | 7.02 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 380 | 14,033 | 0.32 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 381 | 5,100 | 0.12 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 382 | 9,569 | 0.22 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 383 | 67,051 | 1.54 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 384 | 3,389,986 | 77.82 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 385 | 3,761 | 0.09 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 386 | 824,479 | 18.93 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 387 | 606,113 | 13.91 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 388 | 45,092,966 | 1035.19 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 389 | 39,249 | 0.90 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 390 | 53,532 | 1.23 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 391 | 283,626 | 6.51 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 392 | 29,669 | 0.68 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 393 | 30,208 | 0.69 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 394 | 28,474 | 0.65 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 395 | 66,857 | 1.53 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 396 | 12,034 | 0.28 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 397 | 37,097 | 0.85 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 398 | 42,713 | 0.98 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 399 | 35,890 | 0.82 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  | SEGMENT 1 - US 19 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 4 |  | ALT 5 |  | ALT 6 |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 400 | 150,346 | 3.45 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 401 | 196,731 | 4.52 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 402 | 79,361,921 | 1821.90 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 403 | 158,911 | 3.65 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 404 | 107,001 | 2.46 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 405 | 173,028 | 3.97 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 406 | 29,439 | 0.68 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 407 | 38,530 | 0.88 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 408 | 17,360,460 | 398.54 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 409 | 5,354,881 | 122.93 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 410 | 512,016 | 11.75 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 411 | 983,920 | 22.59 | 0 | 804 | 0.02 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 412 | 14,783 | 0.34 | 0 | 1,175 | 0.03 | 0 | 0.00 | 2,652 | 0.06 | 0 | 0.00 | 2,652 | 0.06 |
| 413 | 16,644 | 0.38 | 0 | 1,864 | 0.04 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 414 | 16,290 | 0.37 | 0 | 1,018 | 0.02 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 415 | 13,718 | 0.31 | 0 | 124 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 416 | 16,214 | 0.37 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 417 | 41,667 | 0.96 | 0 | 0 | 0.00 | 1,633 | 0.04 | 0 | 0.00 | 1,633 | 0.04 | 0 | 0.00 |
| 418 | 197,190 | 4.53 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 419 | 12,298 | 0.28 | 0 | 0 | 0.00 | 0 | 0.00 | 3,871 | 0.09 | 0 | 0.00 | 3,871 | 0.09 |
| 420 | 41,370 | 0.95 | 0 | 0 | 0.00 | 0 | 0.00 | 1,063 | 0.02 | 2,614 | 0.06 | 4,792 | 0.11 |
| 421 | 11,642 | 0.27 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 422 | 7,845 | 0.18 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 423 | 54,079 | 1.24 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 424 | 27,960 | 0.64 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 425 | 1,311,175 | 30.10 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  |  SEGMENTS 2 and 7 - WV 307/AIRPORT ROAD   <br> ALT 1 ALT 2   |  |  |  |  | SEGMENT 8 - US 19 CONNECTOR |  |  |  |  |  | US 19 CONNECTOR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA |  |  |  |  |  | ALT 1-OVERPASS |  | ALT 1-AT GRADE |  | ALT 2 |  |  |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 254 | 214,572 | 4.93 | 0 | 0 | 0.00 | 0 | 0.00 | 25,274 | 0.58 | 25,274 | 0.58 | 0 | 0.00 | 0 | 0.00 |
| 255 | 38,360 | 0.88 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 256 | 20,406 | 0.47 | 0 | 0 | 0.00 | 0 | 0.00 | 5,379 | 0.12 | 5,379 | 0.12 | 0 | 0.00 | 0 | 0.00 |
| 257 | 49,331 | 1.13 | 0 | 0 | 0.00 | 0 | 0.00 | 10,831 | 0.25 | 10,831 | 0.25 | 0 | 0.00 | 0 | 0.00 |
| 258 | 38,846 | 0.89 | 0 | 0 | 0.00 | 0 | 0.00 | 9,105 | 0.21 | 9,105 | 0.21 | 0 | 0.00 | 0 | 0.00 |
| 259 | 54,979 | 1.26 | 0 | 0 | 0.00 | 0 | 0.00 | 5,019 | 0.12 | 5,019 | 0.12 | 0 | 0.00 | 0 | 0.00 |
| 260 | 14,549 | 0.33 | 0 | 0 | 0.00 | 0 | 0.00 | 2,652 | 0.06 | 2,652 | 0.06 | 0 | 0.00 | 0 | 0.00 |
| 261 | 14,331 | 0.33 | 0 | 0 | 0.00 | 0 | 0.00 | 2,457 | 0.06 | 2,457 | 0.06 | 0 | 0.00 | 0 | 0.00 |
| 262 | 15,700 | 0.36 | 0 | 0 | 0.00 | 0 | 0.00 | 4,043 | 0.09 | 4,043 | 0.09 | 0 | 0.00 | 0 | 0.00 |
| 263 | 29,593 | 0.68 | 0 | 0 | 0.00 | 0 | 0.00 | 11,623 | 0.27 | 11,623 | 0.27 | 0 | 0.00 | 0 | 0.00 |
| 264 | 9,425 | 0.22 | 0 | 0 | 0.00 | 0 | 0.00 | 1,090 | 0.03 | 1,090 | 0.03 | 0 | 0.00 | 0 | 0.00 |
| 265 | 6,120 | 0.14 | 0 | 0 | 0.00 | 0 | 0.00 | 656 | 0.02 | 656 | 0.02 | 0 | 0.00 | 0 | 0.00 |
| 266 | 58,012 | 1.33 | 0 | 0 | 0.00 | 0 | 0.00 | 12,239 | 0.28 | 12,239 | 0.28 | 0 | 0.00 | 0 | 0.00 |
| 267 | 116,164 | 2.67 | 0 | 0 | 0.00 | 0 | 0.00 | 5,495 | 0.13 | 5,495 | 0.13 | 0 | 0.00 | 0 | 0.00 |
| 268 | 114,213 | 2.62 | 0 | 0 | 0.00 | 0 | 0.00 | 4,023 | 0.09 | 4,023 | 0.09 | 0 | 0.00 | 0 | 0.00 |
| 269 | 8,375 | 0.19 | 0 | 0 | 0.00 | 0 | 0.00 | 8,375 | 0.19 | 8,375 | 0.19 | 0 | 0.00 | 0 | 0.00 |
| 270 | 7,421 | 0.17 | 0 | 0 | 0.00 | 0 | 0.00 | 7,421 | 0.17 | 7,421 | 0.17 | 0 | 0.00 | 0 | 0.00 |
| 271 | 8,131 | 0.19 | 0 | 0 | 0.00 | 0 | 0.00 | 8,131 | 0.19 | 8,131 | 0.19 | 3,085 | 0.07 | 0 | 0.00 |
| 272 | 29,833 | 0.68 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 6,005 | 0.14 | 0 | 0.00 |
| 273 | 15,407 | 0.35 | 0 | 0 | 0.00 | 0 | 0.00 | 605 | 0.01 | 605 | 0.01 | 0 | 0.00 | 1,569 | 0.04 |
| 274 | 22,773 | 0.52 | 0 | 0 | 0.00 | 0 | 0.00 | 10,985 | 0.25 | 10,985 | 0.25 | 14,775 | 0.34 | 0 | 0.00 |
| 275 | 14,639 | 0.34 | 0 | 0 | 0.00 | 0 | 0.00 | 9,217 | 0.21 | 9,217 | 0.21 | 0 | 0.00 | 0 | 0.00 |
| 276 | 172,211 | 3.95 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 19,990 | 0.46 | 0 | 0.00 |
| 277 | 8,789 | 0.20 | 0 | 0 | 0.00 | 0 | 0.00 | 8,789 | 0.20 | 8,789 | 0.20 | 0 | 0.00 | 0 | 0.00 |
| 278 | 13,703 | 0.31 | 0 | 0 | 0.00 | 0 | 0.00 | 8,651 | 0.20 | 8,651 | 0.20 | 2,414 | 0.06 | 0 | 0.00 |
| 279 | 13,346 | 0.31 | 0 | 0 | 0.00 | 0 | 0.00 | 9,599 | 0.22 | 9,599 | 0.22 | 1,462 | 0.03 | 0 | 0.00 |
| 280 | 99,970 | 2.29 | 0 | 0 | 0.00 | 0 | 0.00 | 42,417 | 0.97 | 42,417 | 0.97 | 33,464 | 0.77 | 25,585 | 0.59 |
| 281 | 24,746 | 0.57 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 282 | 17,863 | 0.41 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 283 | 126,063 | 2.89 | 0 | 0 | 0.00 | 0 | 0.00 | 61,492 | 1.41 | 61,492 | 1.41 | 112,702 | 2.59 | 28,502 | 0.65 |
| 284 | 14,999 | 0.34 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 285 | 29,397 | 0.67 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 286 | 8,640 | 0.20 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 287 | 15,540 | 0.36 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 4,694 | 0.11 |
| 288 | 10,196 | 0.23 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 10,189 | 0.23 |
| 289 | 19,076 | 0.44 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 3,630 | 0.08 |
| 290 | 29,132 | 0.67 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 20,067 | 0.46 |
| 291 | 9,127 | 0.21 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 9,114 | 0.21 |
| 292 | 754 | 0.02 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 754 | 0.02 |
| 293 | 5,089 | 0.12 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 3,538 | 0.08 |
| 294 | 20,209 | 0.46 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 12,089 | 0.28 |
| 295 | 12,826 | 0.29 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 5,676 | 0.13 |
| 296 | 17,269 | 0.40 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 5,192 | 0.12 |
| 297 | 20,882 | 0.48 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 8,768 | 0.20 |
| 298 | 12,943 | 0.30 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 3,597 | 0.08 |
| 299 | 17,870 | 0.41 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 3,883 | 0.09 |

ACQUISITION TABLE


ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  | SEGMENTS 2 and 7 - WV 307/AIRPORT ROAD |  |  |  |  | SEGMENT 8-US 19 CONNECTOR |  |  |  |  |  | US 19 CONNECTOR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA | ALT 1 | ALT 2 |  | ALT 3 |  | ALT 1 - OVERPASS |  | ALT 1 - AT GRADE |  | ALT 2 |  |  |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 350 | 1,330,124 | 30.54 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 351 | 223,558 | 5.13 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 352 | 2,002,822 | 45.98 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 353 | 5,411 | 0.12 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 354 | 167,690 | 3.85 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 355 | 81,889 | 1.88 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 356 | 87,017 | 2.00 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 357 | 11,875 | 0.27 | 0 | 3,498 | 0.08 | 4,220 | 0.10 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 358 | 52,359 | 1.20 | 0 | 4,107 | 0.09 | 6,239 | 0.14 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 359 | 16,732 | 0.38 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 360 | 23,772 | 0.55 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 361 | 19,930 | 0.46 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 362 | 82,339 | 1.89 | 0 | 0 | 0.00 | 7,052 | 0.16 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 363 | 6,283 | 0.14 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 364 | 70,180 | 1.61 | 0 | 7,820 | 0.18 | 10,115 | 0.23 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 365 | 15,996 | 0.37 | 0 | 785 | 0.02 | 1,115 | 0.03 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 366 | 15,438 | 0.35 | 0 | 693 | 0.02 | 996 | 0.02 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 367 | 264,367 | 6.07 | 0 | 1,454 | 0.03 | 2,292 | 0.05 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 368 | 21,225 | 0.49 | 0 | 13,215 | 0.30 | 15,619 | 0.36 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 369 | 299,554 | 6.88 | 0 | 7,262 | 0.17 | 5,701 | 0.13 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 370 | 415,715 | 9.54 | 0 | 11,724 | 0.27 | 9,657 | 0.22 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 371 | 1,951,583 | 44.80 | 0 | 103,396 | 2.37 | 97,511 | 2.24 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 372 | 1,992,770 | 45.75 | 0 | 80,943 | 1.86 | 78,548 | 1.80 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 373 | 1,273,757 | 29.24 | 0 | 44,141 | 1.01 | 41,066 | 0.94 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 374 | 27,955,462 | 641.77 | 0 | 53,103 | 1.22 | 21,391 | 0.49 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 375 | 458,047 | 10.52 | 0 | 45,447 | 1.04 | 45,447 | 1.04 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 376 | 1,496,029 | 34.34 | 0 | 177,909 | 4.08 | 220,775 | 5.07 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 377 | 4,248,452 | 97.53 | 0 | 44,330 | 1.02 | 184,915 | 4.25 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 378 | 15,324 | 0.35 | 0 | 10,443 | 0.24 | 9,646 | 0.22 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 379 | 305,933 | 7.02 | 0 | 54,594 | 1.25 | 54,349 | 1.25 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 380 | 14,033 | 0.32 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 475 | 0.01 |
| 381 | 5,100 | 0.12 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 382 | 9,569 | 0.22 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 1,034 | 0.02 |
| 383 | 67,051 | 1.54 | 0 | 0 | 0.00 | 0 | 0.00 | 39,650 | 0.91 | 38,903 | 0.89 | 22,707 | 0.52 | 0 | 0.00 |
| 384 | 3,389,986 | 77.82 | 0 | 122,330 | 2.81 | 135,392 | 3.11 | 281,402 | 6.46 | 263,388 | 6.05 | 326,804 | 7.50 | 0 | 0.00 |
| 385 | 3,761 | 0.09 | 0 | 0 | 0.00 | 0 | 0.00 | 3,761 | 0.09 | 3,531 | 0.08 | 3,592 | 0.08 | 0 | 0.00 |
| 386 | 824,479 | 18.93 | 0 | 0 | 0.00 | 0 | 0.00 | 297,616 | 6.83 | 309,015 | 7.09 | 278,840 | 6.40 | 0 | 0.00 |
| 387 | 606,113 | 13.91 | 0 | 0 | 0.00 | 0 | 0.00 | 82,090 | 1.88 | 149,101 | 3.42 | 129,077 | 2.96 | 0 | 0.00 |
| 388 | 45,092,966 | 1035.19 | 0 | 0 | 0.00 | 0 | 0.00 | 21,464 | 0.49 | 27,933 | 0.64 | 167,104 | 3.84 | 0 | 0.00 |
| 389 | 39,249 | 0.90 | 0 | 0 | 0.00 | 0 | 0.00 | 26,015 | 0.60 | 38,829 | 0.89 | 37,106 | 0.85 | 0 | 0.00 |
| 390 | 53,532 | 1.23 | 0 | 0 | 0.00 | 0 | 0.00 | 9,236 | 0.21 | 43,868 | 1.01 | 44,085 | 1.01 | 0 | 0.00 |
| 391 | 283,626 | 6.51 | 0 | 0 | 0.00 | 0 | 0.00 | 2,960 | 0.07 | 37,577 | 0.86 | 14,464 | 0.33 | 0 | 0.00 |
| 392 | 29,669 | 0.68 | 0 | 0 | 0.00 | 0 | 0.00 | 22,621 | 0.52 | 29,669 | 0.68 | 26,891 | 0.62 | 0 | 0.00 |
| 393 | 30,208 | 0.69 | 0 | 0 | 0.00 | 0 | 0.00 | 23,970 | 0.55 | 30,208 | 0.69 | 30,208 | 0.69 | 0 | 0.00 |
| 394 | 28,474 | 0.65 | 0 | 0 | 0.00 | 0 | 0.00 | 14,653 | 0.34 | 28,474 | 0.65 | 28,474 | 0.65 | 0 | 0.00 |
| 395 | 66,857 | 1.53 | 0 | 0 | 0.00 | 0 | 0.00 | 14,742 | 0.34 | 19,022 | 0.44 | 9,132 | 0.21 | 0 | 0.00 |
| 396 | 12,034 | 0.28 | 0 | 0 | 0.00 | 0 | 0.00 | 12,034 | 0.28 | 9,351 | 0.21 | 2,675 | 0.06 | 0 | 0.00 |
| 397 | 37,097 | 0.85 | 0 | 0 | 0.00 | 0 | 0.00 | 17,425 | 0.40 | 6,622 | 0.15 | 575 | 0.01 | 0 | 0.00 |
| 398 | 42,713 | 0.98 | 0 | 0 | 0.00 | 0 | 0.00 | 36,636 | 0.84 | 42,713 | 0.98 | 39,197 | 0.90 | 0 | 0.00 |
| 399 | 35,890 | 0.82 | 0 | 0 | 0.00 | 0 | 0.00 | 15,095 | 0.35 | 15,176 | 0.35 | 9,487 | 0.22 | 0 | 0.00 |

ACQUISITION TABLE

| PARCEL | PARCEL TOTALS |  |  SEGMENTS 2 and 7-WV 307/AIRPORT ROAD  <br> ALT 1 ALT 2 ALT 3 |  |  |  |  | SEGMENT 8 - US 19 CONNECTOR |  |  |  |  |  | US 19 CONNECTOR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA | AREA |  |  |  |  |  | ALT 1-OVERPASS |  | ALT 1 - AT GRADE |  | ALT 2 |  |  |  |
|  | SF | AC | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC | SF | AC |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 400 | 150,346 | 3.45 | 0 | 0 | 0.00 | 0 | 0.00 | 57,693 | 1.32 | 97,491 | 2.24 | 85,957 | 1.97 | 0 | 0.00 |
| 401 | 196,731 | 4.52 | 0 | 0 | 0.00 | 0 | 0.00 | 78,670 | 1.81 | 102,739 | 2.36 | 90,542 | 2.08 | 0 | 0.00 |
| 402 | 79,361,921 | 1821.90 | 0 | 0 | 0.00 | 0 | 0.00 | 432,767 | 9.93 | 507,635 | 11.65 | 459,628 | 10.55 | 0 | 0.00 |
| 403 | 158,911 | 3.65 | 0 | 0 | 0.00 | 0 | 0.00 | 60,255 | 1.38 | 69,254 | 1.59 | 61,795 | 1.42 | 0 | 0.00 |
| 404 | 107,001 | 2.46 | 0 | 0 | 0.00 | 0 | 0.00 | 34,818 | 0.80 | 39,447 | 0.91 | 34,346 | 0.79 | 0 | 0.00 |
| 405 | 173,028 | 3.97 | 0 | 0 | 0.00 | 0 | 0.00 | 28,801 | 0.66 | 37,640 | 0.86 | 26,115 | 0.60 | 0 | 0.00 |
| 406 | 29,439 | 0.68 | 0 | 0 | 0.00 | 0 | 0.00 | 19,399 | 0.45 | 23,369 | 0.54 | 44,352 | 1.02 | 0 | 0.00 |
| 407 | 38,530 | 0.88 | 0 | 0 | 0.00 | 0 | 0.00 | 5,641 | 0.13 | 11,573 | 0.27 | 5,201 | 0.12 | 0 | 0.00 |
| 408 | 17,360,460 | 398.54 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 409 | 5,354,881 | 122.93 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 410 | 512,016 | 11.75 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 411 | 983,920 | 22.59 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 412 | 14,783 | 0.34 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 413 | 16,644 | 0.38 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 414 | 16,290 | 0.37 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 415 | 13,718 | 0.31 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 416 | 16,214 | 0.37 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 417 | 41,667 | 0.96 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 418 | 197,190 | 4.53 | 0 | 889 | 0.02 | 433 | 0.01 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 419 | 12,298 | 0.28 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 420 | 41,370 | 0.95 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 |
| 421 | 11,642 | 0.27 | 0 | 0 | 0.00 | 0 | 0.00 | 1,504 | 0.03 | 1,504 | 0.03 | 0 | 0.00 | 0 | 0.00 |
| 422 | 7,845 | 0.18 | 0 | 0 | 0.00 | 0 | 0.00 | 1,366 | 0.03 | 1,366 | 0.03 | 0 | 0.00 | 6,478 | 0.15 |
| 423 | 54,079 | 1.24 | 0 | 0 | 0.00 | 0 | 0.00 | 200 | 0.00 | 200 | 0.00 |  | 0.00 | 0 | 0.00 |
| 424 | 27,960 | 0.64 | 0 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 9,309 | 0.21 | 0 | 0.00 |
| 425 | 1,311,175 | 30.10 | 0 | 0 | 0.00 | 0 | 0.00 | 27,215 | 0.62 | 27,215 | 0.62 | 27,215 | 0.62 | 0 | 0.00 |
| 426 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1,632 | 0.04 |
| 427 |  |  |  |  |  |  |  |  |  |  |  |  |  | 157 | 0.00 |
| 428 |  |  |  |  |  |  |  |  |  |  |  |  |  | 786 | 0.02 |
| 429 |  |  |  |  |  |  |  |  |  |  |  |  |  | 5,940 | 0.14 |
| 430 |  |  |  |  |  |  |  |  |  |  |  |  |  | 10,277 | 0.24 |
| 431 |  |  |  |  |  |  |  |  |  |  |  |  |  | 374 | 0.01 |
| 432 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2,782 | 0.06 |
| 433 |  |  |  |  |  |  |  |  |  |  |  |  |  | 14,116 | 0.32 |
| 434 |  |  |  |  |  |  |  |  |  |  |  |  |  | 5,779 | 0.13 |
| 435 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7,939 | 0.18 |
| 436 |  |  |  |  |  |  |  |  |  |  |  |  |  | 7,041 | 0.16 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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## Appendix E

## Office Review Comments with Actions Taken

## DATE OF REVIEW: July 15, 2014

TO:
Mr. Timothy R. Priddy, WVDOH Project Manager
PROJECT NUMBER: State Project X241-ZWA/Y-1.00 Federal Project HPP-2007(050)D

DESCRIPTION: Beckley Z-Way Design Study
Office Review Meeting

PARTICIPANTS: Tim Priddy, WVDOH-DDR
Elwood Penn, WVDOH-RPL
Don Meadows, WVDOH-DT
Randy Epperly, WVDOH-DDE
Yuvonne Smith, FHWA
arry Clegg, CDM Smith
Brad Johnson, CDM Smith Joe Crittenden, CDM Smith
 review meeting.

## Comments:

1. Comment: Hard copies of typed comments concerning the traffic report were provided at the start of the review.

Action: No Response needed.
2. Comment: Appears to be inconsistencies in the traffic growth rates in the traffic report for different intersections. Verify the growth rates and add a section to the report explaining the growth rates and forecast parameters used for the project. Consider updating the AM Peak K-factor and D-factor if it is determined the AM Peak is overestimating forecast volumes

Action: The overestimation has no impact on the intersection analysis and resulting conclusions
3. Comment: In the traffic report add analysis for the segment 8 at-grade alternative.

Action: The suggested alternative has been added.
4. Comment: A fourth leg has been recently added to the WV 3/US 19 intersection at the Dollar General store. Please reflect this in the traffic report.

Action: This fourth leg is private entrance. The signal operation is governed by the WV-3 traffic
5. Comment: Add the location of existing and proposed traffic signals into the traffic report and design study report.
 Extension, at the at-grade intersection with WV 307 and the Bypass Extension and the I-64 Interchange ramp intersections would likely meet signal warrants.
6. Comment: Provide traffic analysis software files to the WVDOH.

## Action: These files will be provided.

7. Comment: Add a left turn lane from US 19 onto Greystone Drive at the US 19 Connector on both the study plans and traffic report.

Action: A left turn lane from Segment 8/US 19 Connector onto Greystone Drive is shown on the plan sheet for the Segment 8 Alternate 1 Overpass alternative. The Segment 8 Alternate 1 At-grade

 condition may cause additional operational issues during inclement weather. Additionally, the vertical alignment exceeds $16 \%$ and does not meet any design criteria contained within DD-601.
8. Comment: If possible, eliminate all retaining walls.
 detailed environmental assessments, subsurface investigation, and other salient information is obtained for the final design phase of the project.
9. Comment: In the design report the consultant is to recommend which sections of the project should be constructed in which sequence.

Action: Comment rescinded by WVDOH.
10. Comment: Add critical cross sections in areas with maximum cut and fill.

Action: Additional cross sections were added at selected critical locations to supplement the 500 foot interval cross sections.
11. Comment: Within the design report mention constructability problems within areas with adjusted vertical alignments.
 are selected to proceed into the design phase, special attention to the temporary traffic control design is required in the areas of vertical alignment adjustments.
12. Comment: Add an overview sheet for the US 19 Connector to Segment 8.

## Action: Overview sheets were added for all US 19 Connectors to Segment 8.

13. Comment: Add a cross section for Segment 8 under the I-64 Bridge.

Action: An Alternate 1 Overpass section showing Segment 8 under the I-64 Bridge is shown on sheet 223, Alternate 1 At-grade is shown on sheet 241 , and Alternate 2 is shown on sheet 259 . The sections are shown in the upper right corner of the appropriate plan sheet.
14. Comment: Add a typical section for Segment 8 under the I-64 Bridge.
 sections are shown in the upper right corner of the appropriate plan sheet.
15. Comment: Revise the Segment 8 profiles to a natural scale.

Action: The Segment 8 profiles were revised to a natural scale as requested.
16. Comment: Show design exceptions in the report for each segment.

## Action: Design exceptions are shown in Appendix B of the Design Report.

17. Comment: Verify maximum grade used in the design criteria and terrain type.

Action: The maximum grade for urban arterials in mountainous terrain is listed as $9 \%$ in Table $7-4$ of the 2011 "A Policy on Geometric Design of Highways and Streets".
18. Comment: Incorporate review comments with actions taken into the design report.

Action: The review comments with the actions taken will be incorporated into the design report.
19. Comment: Verify statement in the drainage report about drainage area being in error.

Action: The statement was revised to read; "The Little Beaver drainage area was verified using Maptech Terrain Professional.
20. Comment: In the design report, estimate the length of stream impacts for each segment's alternative.

Action: The estimated length of stream impacts is located on the appropriate evaluation matrix.
21. Comment: In the design report cost estimates for Segment 8, add a line item for the US 19 Connector and add a note on the US 19 Connector estimate that the number was carried to appropriate alternatives.

Action: A line was added into the detailed estimates showing the anticipated cost of the US 19 Connector.

Prepared by: CDM Smith

## ALIGNMENT ALTERNATIVE STUDY REPORT

STATE PROJECT X341-ZWA/Y-6.22 02
FEDERAL PROJECT STP-0019(429)D
BEAVER - SOUTH EISENHOWER DRIVE
RALEIGH COUNTY

PREPARED BY:


Engineers \& Consultants

PREPARED FOR:


APRIL 2018

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VICINITY MAP

## SECTION 1 - PROJECT SUMMARY

The purpose of this Alignment Alternative Report is to provide an alternative alignment option for the segment of the Beckley Z-Way from Beaver to the I-64 Exit I24 Interchange. The original alignment alternatives considered for this segment of the Z-Way was developed in the Beckley Z-Way Final Design Report Study by CDM Smith in November 2014. In the original 2014 Beckley Z-Way Design Report the Beaver - South Eisenhower Drive segment was called Segment 8. In the original report three various alignments studied.
> Alternate No 1 Overpass - An alignment with a bridge over WV307 (Airport Road)
$>$ Alternate No. 1 At Grade - An alignment with at-grade intersection over WV307 (Airport Road)
$>$ Alternate No. 2 (Overpass) -Alignment with a begin project moved about 1000 to the north.

In addition, the original study also had a separate alignment alternative connecting the existing US19 to the new Z-Way near the south end of the project.

The Gates alternative alignment is somewhat similar to the original Alternate No. 2 with a starting point further to the south and an overpass over Airport Road (WV307). However, the Gates alignment does have some significant differences from the earlier CDM Smith Study Alignments (see Figure 1 for a comparison of the Alignments). A few of the differences are listed below:
$>$ A more curved alignment between the Skyline Drive and Cherry Hills subdivision to minimize community impacts.
> The connector road between the Z-way and US19 is moved to the north and is included as part of the Gates alignment
> Improvements to Airport Road (WV307) adding a center turn lane to accommodate right turn and left turn lanes onto the Z-Way connector ramps from Airport Road.
> The original study did not have a connection to Orchard Hill Road or Skyline Drive. Connector roads to both Orchard Hill Road (CR9) and Skyline Drive (CR9/8) providing access to the local residences along the route have been added.

Shifted alignment on the mainline on the north end of the project near the interchange to minimize earthwork and avoid an existing Cell Tower.

The Gates alignment begins at the northern termini of the Z-Way project, Shady Spring - Beaver, near the intersection of US19 (Ritter Drive) \& County Route 19/36 (Old Crow Road). This segment of the Z-Way will diverge to the northwest away from US19 and continues on to the northwest crossing over WV307 (Airport Road) approximately 1100 feet north of the US19 \& WV307 intersection at Beaver. From WV307 the alignment continues to the northwest through mountainous terrain where it crosses County Route 9 (Orchard Hill Road) and then onto the northern termini location at the l-64 Exit 124 Beckley-Eisenhower Drive Interchange. This segment will be a new facility which connects US 19 directly to I-64. The construction of this segment will help alleviate congestion in the Beaver area, especially at US19 \& WV307 intersection, by providing a more direct route and more convenient access to the commercial areas along Eisenhower Drive and Robert C. Byrd Drive.


Figure 1: Comparison of Study Alignments

## SECTION 2-ROADWAY IMPROVEMENTS

## Mainline

The Beaver to South Eisenhower Drive project is part of the Beckley Z-Way project. The project begins at the north termini of the Shady Spring - Beaver project at Sta 292+95 and runs to the I-64 Exit 124 Interchange at Sta 393+88. This project is a 1.91 mile three-lane highway with a center turn lane that will provide better access to the nearby communities of Beaver, Daniels and Shady Spring to Interstate 64 and the commercial and retail areas of Beckley along Eisenhower and Robert C. Byrd Drive. In addition, the project will help alleviate local traffic congestion in the Beaver area and provide a safer facility for the travelling public. All design has been done to meet the AASHTO Policy on Geometric Design of Highways and Streets 2011, 6th edition. All of the specific design criteria for the project can be found in Appendix B.

## Side Roads and Connector Roads

The Beaver - S Eisenhower Drive projects includes connections to six local roads.
> Old Crow Road (CR 119/36) at Sta 299+00 Rt (340 ft)
> Ritter Drive (US Route 19/ WV 3) at Sta 305+75 Lt (460 ft)
> Airport Road Ramp (WV307) at Sta 315+00 Lt (485 ft)
> Airport Road Improvements at Sta 319+20 (980 ft)
$>$ Pine Haven Road at Sta 315+00 Rt ( 270 ft )
> Orchard Hill Road (CR 9) at Sta 343+25 Lt (505 ft)
$>$ Skyline Drive (CR 9/8) at Sta 343+25 Lt (300 ft)
The total length of all side road improvements is 3,340 feet ( 0.63 miles). Airport road will also be widened to accommodate a center turn lane primarily to add right and left turn lanes from Airport Road to the Connector Ramp to the Z-Way.

## Mainline \& Side Roads Temporary Traffic Control

Most of the Temporary Traffic Control issues will be fairly routine. Below is a summary of some of the proposed traffic control at each side road on the project.
> Begin Project connection to US19 Sta 293+00 to Sta 296+50 - Traffic will be maintained on the existing road throughout construction of the mainline. The tie-in connection at the beginning of the project back to US19 have to be one of the segments of the project to complete. Phased construction will be utilized to complete the tie-in in this area.
> Old Crow Road (CR119/36) - Sta 299+00 Rt, Similar to the tie-in to US19, traffic will be maintained on the existing roads during construction of the Z-Way and the final connection to the Z-Way will need to be done near the end of the project.
> Old US19 Connection - Sta 305+75 Lt, Similar to the tie-in to US19 and Old Crow Road, traffic will be maintained on the existing roads during construction of the Z-Way and the final connection to the US19 will need to be done near the end of the project. However, it would be possible to construct the Z-Way from the Begin Project Sta 292+95 to about Sta 306+00 and shift local traffic to this 1300 feet section of the Z-Way prior to construction the remainder of the Z-Way but it would not be preferable.
> Airport Road Ramps and Pine Haven Ramps - Sta 315+00 Rt \& Lt. Since the Z-Way embankment covers over Pine Haven Road, either a temporary road on the right side of the fill slope will need to be constructed for the Pine Haven community access or the Ramps will need to be complete entirely before the roadway fill can be constructed from Sta 615+00 to Sta 319+00.
> Airport Road Improvements - Since most of the Airport Road improvements are an overlay and widening scenario, traffic control should be fairly routine. However the proposed Box Culvert at Sta 79+75 for Little Beaver Creek does present the largest traffic control challenge on the project. It is the intent to extend the box culvert approximately 4 feet upstream of what is necessary to accommodate temporary traffic so that two-lane traffic can be maintained on Airport Road at all times while the box culvert is built in phases. In general, traffic will be maintained on the existing road while the upstream side of the box is built. Two-way traffic will then be moved onto the new box culvert while the downstream portion of the box is constructed.
> Airport Road Overpass Bridge - Since the bridge is to be built on new embankment fills and set
back from Airport Road, there should be minimal traffic disruption during construction. However the road will have to be closed temporarily when the beams are set
> Orchard Hill Road/ Skyline Drive - Traffic Control should be fairly straight forward in this area since Orchard Hill Road will be closed during construction.

## Interchange Improvements

The Interchange Design Criteria Listings have been established based on West Virginia Department of Transportation Division of Highways Design Directives and AASHTO's A Policy of Geometric Design of Highways and Streets, 2011 Sixth Edition (AASHTO Green Book) and direction from the West Virginia Department of Transportation Division of Highways (DOH). The US Route 19 Corridor utilized a design speed of 45 MPH and maximum superelevation of $4 \%$ as directed by DOH. South of the interchange with I64 , the typical section will be 2-11' travel lanes, 1-14' center turn lane and $11^{\prime}$ auxiliary turn lanes as required. Within the I-64 Interchange, there will be 1 or 2-12' travel lanes and $12^{\prime}$ auxiliary turn lanes as required. Auxiliary lanes have been introduced with tapers in accordance with DD-622, and lane shift tapers are developed with a speed-to-1 foot taper rate. A painted $12^{\prime}$ median will be provided and median barrier and impact attenuators will be used to protect the existing overpass bridge piers, as well as to tie into the existing condition north of the interchange. The proposed horizontal and vertical geometry will extend north beyond the interchange to provide access to the existing US Route 19 and closely mimic the existing horizontal and vertical geometry through the interchange. South of the interchange, US Route 19 will require additional right-of-way for the new alignment. The proposed minimum vertical clearance is $20^{\prime}-8^{\prime \prime}$, under the I-64 EB structure. It is anticipated that additional topographical survey will be required from STA $378+00$ to $395+00$ to accurately tie down final plans.

The jughandle design speed varies from 40 MPH to 15 MPH as it approaches a stop condition. Maximum superelevation in the jughandle, which is part of the US Route 19 Corridor, is also 4\%. The jughandle lane width will vary from 1-16' lane to 2-15' lanes. A small retaining wall or concrete barrier may be required under the bridge, the proposed horizontal and vertical geometry ties in with the US Route 19 and the I-64 EB Entrance Ramp. The jughandle meets the US Route 19, EB ramp intersection at a $96^{\circ} 11^{\prime} 39^{\prime \prime}$ angle. The proposed minimum vertical clearance under the I-64 EB Structure is $18^{\prime}-8^{\prime \prime}$. A rock cut will be required
along the right side of the jughandle. The jughandle will require additional right-of-way. It is anticipated that additional topographical survey will be required from STA 920+00 to $923+00$ to accurately tie down final plans and develop wall or barrier elevations, if required.

I-64 EB entrance ramp design speed varies from 20 MPH to 50 MPH as the ramp approaches the Interstate. The ramp will have 2-15' lanes and will be tapered to match existing conditions before the tie in. Existing horizontal geometry could not be used as the curve leading up to l-64 EB could not meet 50 MPH design speed criteria. The horizontal geometry departs US Route 19 with a $95^{\circ} 34^{\prime} 48^{\prime \prime}$ angle. No additional right-of-way is required for this ramp. The ramp will require $362^{\prime}$ of guard rail to connect a cut slope terminal with the existing guard rail. It is anticipated that additional topographical survey will be required from STA $711+00$ to $713+00$ to accurately tie down final plans.

I-64 EB exit ramp design speed is 25 MPH as an exit ramp in accordance with AASHTO Green Book, page 10-89, Loop Ramps. As the ramp approaches a stop condition, a 20 MPH design speed is utilized. The ramp horizontal geometry is parallel to the I-64 EB entrance ramp as it approaches US Route 19. The vertical geometry approaching US Route 19 is a graphic grade controlled by the I-64 EB entrance ramp as it approaches a stop condition. The horizontal geometry approaches US Route 19 with a $96^{\circ} 10^{\prime} 12^{\prime \prime}$ angle. No additional right-of-way is required for this ramp. It is anticipated that additional topographical survey will be required from STA 849+00 to 850+50 to accurately tie down final plans.

The I-64 WB exit ramp design speed is 45 MPH , and the I-64 WB exit ramp spur has a 15 MPH design speed as it is approaching a stop condition. The I-64 WB exit ramp is 1-16' lane and the I-64 WB exit ramp spur is 1-16' lane that develops off of the I-64 WB exit ramp as it approaches US Route 19 for southbound access.

The I-64 WB exit ramp approaches US Route 19 northbound and maintains its own lane going northbound No additional right-of-way is required for this ramp. The ramp will require $400^{\prime}$ of guard rail from the existing guard rail to the end of the fill condition, and an additional 575' of guard rail to connect a cut slope terminal to the existing guard rail. It is anticipated that additional topographical survey will be required from STA $404+00$ to $406+00$ and $424+00$ to $426+00$ to accurately tie down final plans.

The I-64 WB entrance ramp design speed varies from 15 MPH at the at-grade ramp terminal tie to 50 MPH
as the ramp approaches the interstate. The baseline of the I-64 WB entrance ramp departs US Route 19 at a $105^{\circ} 00^{\prime} 00^{\prime \prime}$ angle and the first curve on the alignment is within the at-grade ramp terminal intersection warping and does not meet superelevation. As traffic approaches the interstate the design speed increases to 50 MPH with the second curve meeting superelevation. No additional right-of-way is required for this ramp. It is anticipated that additional topographical survey will be required from STA 688+00 to 690+00 to accurately tie down final plans.

Intersections at US Route 19 and I-64 westbound ramps and US Route 19 and I-64 eastbound ramps and jughandle will be both signalized. They have been analyzed and provide AASHTO Case D Sight Distance, allowing all vehicles at stop bars to see all other vehicles at stop bars

## Interchange Temporary Traffic Control

## Jughandle, Eastbound Ramps and US 19 Reconstruction

Phase 1: With traffic maintained on existing roadways, construct US 19 ( $371+00$ to $375+00$ ), Jughandle and construct a temporary roadway immediately adjacent to and south of the proposed WB Ramps/US 19 intersection connecting US 19 to existing ramps in the vicinity of Station $703+50$. Construct a second temporary roadway from the jughandle (924+50) to US 19 (377+50).

Phase 2: Shift EB Ramp Traffic to the jughandle utilizing two-way traffic on the jughandle and temporary roadway widening constructed in Phase 1. Reconstruct new US 19/EB Ramp intersection as room allows. Construct EB Entrance Ramp from 705+00 to 708+00 and US 19 from 375+00 to 377+00.

Phase 3: Construct final tie-ins as necessary along US 19 and along the Eastbound Ramps.

## WB Exit Ramps

Phase 1: With traffic on the existing roadway, construct temporary widening/ temporary roadway from $405+00$ (left side) to create a temporary connection with US 19 in the vicinity of Station 389+00.

Phase 2: Shift WB Exit Ramp traffic to the temporary roadway constructed in Phase 1. Reconstruct right side of the WB Exit Ramp to the proposed condition.

Phase 3: Shift traffic to the newly constructed portion of the WB Exit Ramp. Construct the left side of the WB Exit Ramp and the WB Exit Ramp Spur to proposed condition.

## WB Entrance Ramp

Phase 1: With traffic shifted to the right side of the existing WB Entrance Ramp, construct the proposed US 19/WB Entrance Ramp intersection and reconstruct the existing ramp from 683+50 left to 689+50 left.

Phase 2- With traffic on the newly constructed left portion of the ramp, reconstruct the right side of the ramp to the proposed condition.

## Short Term Interchange Traffic Routing

Traffic routing contingency plan: Detour traffic from US Route 19 to I-64 WB onto I-64 EB for one exit to Airport Road where it will rejoin I-64 EB. I-64 EB traffic to US Route 19 will continue past the closed ramp one exit to Airport Road where it will exit and rejoin I-64 WB to exit for US Route 19. Working concurrently with construction of US Route 19, detour traffic from US Route 19 to I-64 EB south along the new US Route 19 and follow Airport Road to the interchange with I-64. Traffic from I-64 WB will exit one interchange prior at Airport Road and follow Airport Road to its new intersection with US Route 19

## Roadway Impacts

The Gates Alternative Alignment as well as the Original Study Alignment have several impacts. The Environmental Impacts will be detailed in the upcoming Environmental Assessment being prepared by Skelly and Loy under separate contract with the WVDOH. However, a brief summary of some of the known impacts are as follows:

Stream Impacts - Approximately 1000' of Little Beaver Creek will be impacted at two locations (Sta 304+00 to Sta $308+00$ and Sta $317+50$ to $318+50$.

Wetland Impacts - Identified in previous Shady - Beaver Z-Way project

- Wetland WL11 (0.635 Ac)
- Wetland WL12 $(0.061 \mathrm{Ac})$
- Wetland WL13 (0.031 Ac)
- Other wetlands are likely to be identified in the Beaver - S Eisenhower Drive Environmental Assessment when completed

Residential \& Commercial Structure Impacts - A total of 22 structures are to be demolished on the project. Of these 22 , three are commercial properties and 10 are residences. The Commercial and residential structures to be demolished are listed:

1. Sta $299+50$ Rt Residence
2. Sta 300+00 LT Commercial Business (First Properties Solutions)
3. Sta307+00 Lt Residence
4. Sta $317+50$ Lt Commercial business (Subway)
5. Sta 320+00 CL Two Apartment Complexes
6. Sta 327+00 CL Residence
7. Sta 331+25 Rt Residence
8. Sta $342+25$ Lt Residence
9. Sta 343+00 Lt Residence
10. Sta 344+25 Lt Residence
11. Sta 344+50 Lt Residence
12. Sta 348+00 CL Residenc
13. Sta 354+00 Rt Residence

In addition to the three commercial properties listed above, an additional four commercial are likely to be impacted but not require a structure demolition. They are

- Woodland Amenities (on Airport Road) Sta $80+00$ to $82+00 \mathrm{Rt}$
- Pine Haven/Whispering Pines (on Airport Road) Sta $82+00$ to $84+00$ Rt
- Strip Mall (on Airport Road) Sta 76+00 to Sta 80+00 Lt
- 84 Lumber (on Airport Road) Sta $81+00$ Lt

Overhead Electric and Phone - Along US19, Airport Road and Orchard Hill Road, there are the typical overhead lines adjacent to the road which will require relocation. In addition, AEP has a 138 kV transmission line which crosses the mainline at Sta 299+00 and runs along the right side of the road until Sta $320+00$. It is the believed that the Z-Way construction will not require the AEP Transmission line to be relocated.

Water - Both Beckley Water and Raleigh County Public Service District have major water mains throughout the project.

- Beckley Water has a $14^{\prime \prime}$ line along US19 at the beginning of the project
- Beckley Water has a $24^{\prime \prime}$ waterline which crosses under Airport Road at about Sta 316+40
- Raleigh County has a 14 " waterline which crosses the mainline at Sta $337+85$.
- All of these water mains will require relocation along with several other smaller water lines in the project area.

Sewer - Shady Spring Public Service District has several gravity sewer lines which will require relocation

- Sewer lines at the beginning of the project along US19 at Sta 292+95 to Sta 297+00
- Sewer main following Little Beaver Creek from Sta 303+00 to Sta 307+00
- Sewer lines along Airport Road from Sta 79+50 to Sta 86+75
- The existing sewer lines crossing overtop of the existing twin culverts along Airport Road will be particularly difficult to relocate since the existing culverts are to be replaced with a new box culvert of a deeper structure depth.

Gas - Mountaineer Gas has several facilities adjacent to US19 and Airport Road that will require relocation. In addition, a gas main crossing at Sta 338+00 near Orchard Hill Road will also require relocation.

## SECTION 3 - STRUCTURES

## Box Culvert beneath Relocated US19 at Station 306+77

A new precast box culvert will be required to carry a relocated portion of Little Beaver Creek beneath Relocated US Route 19 at Station 306+77.5. The box will be constructed on a $2.3 \%$ slope. To limit the hydraulic impact to the surrounding area the culvert section will be $20^{\prime} \times 12^{\prime}$. Cast-in-place wingwalls will be located at each end of the box. The culvert will be approximately $216^{\prime}$ in length and be located under approximately $30^{\prime}$ of fill

## Box Culvert beneath Airport Road at Station 79+76

An existing twin corrugated metal culvert type structure is carrying Little Beaver Creek beneath Airport Road at Station 79+76. Extension of this culvert is required as Airport Road is being widened in this area to accommodate a right hand turn lane onto the Relocated US Route 19. However, extending this type of culvert structure is impractical as it would require a $40^{\prime}$ long concrete span at each end of the structure. Therefore, the culvert structure will be replaced with an $18^{\prime} \times 10^{\prime}$ precast box culvert. Due to the large ADT along Airport Road at this location, the box culvert will be constructed in phases to maintain two lanes of traffic at all times. The box culvert will be approximately $84^{\prime}$ long and constructed on a grade of $3.96 \%$. Fill over the top of the box will range in depth from 0 to $3^{\prime}$. Cast-in-place wingwalls oriented at a 45 degree angle to the box will be constructed at each end to accommodate the 2:1 fill slopes.

## Bridge at Airport Road at Station 82+75

A new overpass bridge will be required to carry Relocated US Route 19 over Airport Road at Station 82+75 The bridge will be a 95 ' single span structure on integral abutments located behind MSE walls. The bridge will be oriented on a 23 degree skew to the Relocated US Route 19 to parallel Airport Road beneath. The MSE walls will be located outside the horizontal clear zone of Airport Road. Based on the proposed profile of the structure, the low chord will be located well above the minimum vertical clearance requirement of $16^{\prime}$ for Airport Road. It is anticipated that the superstructure will consist of $36^{\prime \prime}$ steel rolled beams spaced at approximately $9^{\prime}-0^{\prime \prime}$ supporting a Class $H$ Concrete Deck. The structure will carry two $12^{\prime}$ traffic lanes, a center turn lane, and $6^{\prime}$ shoulders on each side for a clear width of $48^{\prime}-0^{\prime \prime}$. Type $F$ Barriers will be located
on each side resulting in an out-to-out width of $50^{\prime}-6^{\prime \prime}$. Maximum height of the MSE walls will be approximately $30^{\prime}$ with the maximum length of MSE wall being approximately $70^{\prime}$. Three of the MSE walls will be located along 2:1 fill slopes. However, the northwest corner of the bridge will be located along a 1:1 reinforced earth fill slope to limit the impact of the bridge fill slope on the adjacent 84 Lumber property and parking lot

## SECTION 4-HYDRAULICS

## Summary

Little Beaver Creek will be impacted in two locations for this project. A new $20^{\prime} \times 12^{\prime}$ precast box culvert will be required to carry a relocated portion of Little Beaver Creek beneath Relocated US Route 19 at Station 306+77. Also, an existing twin corrugated metal culvert type structure carrying Little Beaver Creek beneath Airport Road at Station $79+76$ will be replaced with an $18^{\prime} \times 10^{\prime}$ precast box culvert.

The alternate studied for this project produces no rise in backwater when compared to the existing condition model for Little Beaver Creek in the preliminary hydraulic model. With these preliminary results, it is anticipated that backwater conditions will be within FEMA and WVDOH guidelines for backwater at stream crossings. A more detailed model will be developed when the project is finalized.

## Available Data

No original plans for the existing twin culverts at Airport Road were located. Hydrologic data for this site was not available. No existing hydraulic model was available. There is a Flood Insurance Study (FIS) available for Little Beaver Creek which includes the limits of this project. Design Discharges were determined using the hydrologic runoff estimation methods presented in the 2007 WVDOH Drainage Manual and verified with the FIS in the vicinity of this project. The Flood Insurance Rate Map (FIRM) for Little Beaver Creek indicates the project is located within the FEMA 100-year floodplain in Flood Hazard Zone AE. The Base Flood Elevation (BFE) for Relocated US Route 19 at Station 306+77 is approximately 2174 ft . The BFE for Airport Road at Station 79+76 is approximately 2204 ft . Information from available data is included in Appendix E - Hydraulic Analysis.

## Hydrology

Drainage areas were calculated using the USGS Topography Map. The drainage area of Little Beaver Creek for Relocated US Route 19 at Station 306+77 is 14.37 square miles and for Airport Road at Station 79+76 it is 14.49 square miles. Design Discharges for this project were determined using the hydrologic runoff estimation methods found in the 2007 WVDOH Drainage Manual. The TR-55 method was utilized to determine Design Discharges and verified with the Flood Insurance Study.

Water surface elevations for Normal Pool were field surveyed at the existing culvert on Airport Road at Station 79+76. The normal pool elevation and OHW was determined to be approximately 2167 and 2168.5, respectively. Drainage design calculations are included in Appendix E - Hydraulic Analysis.

## Hydraulic Modeling

The preliminary hydraulic model was created in HEC-RAS using stream cross section data obtained from the project mapping. The model extends a distance of approximately 650 feet upstream of the proposed US 19 culvert and 250 feet downstream of the Airport Road culvert. These distances should be sufficient to allow for fully expanded stream flow both upstream and downstream of the existing and proposed culverts.

The average slope of the stream in the vicinity of the bridge was also obtained from the project mapping and was then used to calculate the upstream and downstream normal depths within HEC-RAS.

All of the culverts for this project were modeled utilizing the Bridge/Culvert Data Editor. The preliminary modeling approach for each of the culverts was the energy method with supercritical flow regime. Analysis was performed to compare new conditions to existing conditions. For each condition, water surface elevations were determined for the 25-year, 50-year, and 100-year storms. Since the difference in discharges between the two culvert locations was insignificant, the greater flows were modeled throughout the reach. The existing and proposed culverts each pass the three respective storms in the preliminary model. The water surface elevation of 100-year storm was corroborated with the FIS Flood Profiles and the FEMA BFE and the proposed condition was shown to produce no rise in backwater when compared to the existing model. The preliminary backwater summary table is included below and the HEC-RAS files are available for further review.

## BACKWATER SUMMARY TABLE

For $Q_{100}=2812 c f s$

| RIVER SECTION | WATER SURFACE ELEVATION (EXISTING) | WATER SURFACE ELEVATION (PROPOSED) | NOTES |
| :---: | :---: | :---: | :---: |
| 3800 | 2218.88 | 2218.88 |  |
| 3600 | 2213.29 | 2213.29 |  |
| 3200 | 2204.91 | 2204.91 |  |
| 3000 | 2201.83 | NA | Stream relocation |
| 2800 | 2198.96 | 2206.71 | Stream relocation |
| 2600 | NA | PROPOSED US19 CULVERT | Stream relocation |
| 2400 | 2193.57 | 2193.37 | Stream relocation |
| 2200 | 2188.54 | 2188.54 |  |
| 2000 | 2185.09 | 2185.09 |  |
| 1800 | 2179.58 | 2179.58 |  |
| 1600 | 2176.95 | 2176.95 |  |
| 1400 | 2174.53 | 2174.53 |  |
| 1270 | EXISTING AIRPORT RD CULVERT | PROPOSED AIRPORT RD CULVERT |  |
| 1200 | 2165.77 | 2168.01 | Localized drop at existing culvert outlet. |
| 1000 | 2165.10 | 2165.10 |  |

## HEC-RAS Plan Files

The HEC-RAS model was developed using two project files. The existing conditions for Little Beaver Creek for both the Airport Road and US 19 sites, along with the proposed culvert at Airport Road are modeled in the project file named B2EHECAHM.prj. The Little Beaver Creek stream relocation and the proposed culvert at US 19 are modeled in the project file named PROPOSEDB2EHECAHM.prj. Comparison of water surface elevations at common river stations between the models verified that the projects do not influence each other during the proposed conditions. A final hydraulic model including the proposed culverts at Airport Road and Relocated US 19 on the same reach will be further developed in the next stages of the project design.

| Plan | Plan File | Geometry File |
| :---: | :---: | :---: |
| Prelim Little Beaver Creek: B2EHECAHM.prj |  |  |
| Existing Little Beaver <br> Creek | B2EHECAHM.p02 | B2EHECAHM.g02 |
| Airport RdProposed <br> 18x10 Box Culvert | B2EHECAHM.p03 | B2EHECAHM.g03 |
| Prelim Proposed US19 Box with relocation: PROPOSEDB2EHECAHM.prj |  |  |
| Proposed US 19 with <br> Relocation | PROPOSEDB2EHECAHM.p02 | PROPOSEDB2EHECAHM.g03 |

## SECTION 5 - GEOTECHNICAL OVERVIEW

## Summary

This geotechnical overview is for approximately two miles of new roadway connecting US Route 19 in Beaver with Interstate 64 at the South Eisenhower Drive Interchange in Raleigh County, West Virginia. The observations and comments provided in this overview are based on a recent site visit performed by NGE's geotechnical engineer as well as research of available information.

The project will extend from Station $293+00$ to about $380+00$. The initial section of new roadway extending from about Station 295+00 to Station 322+00 will consist principally of fill embankment up to a maximum thickness of about 55 feet. Beyond Station $322+00$ to the end of the project, most of the roadway will be in cut with a maximum cut slope height of about 180 feet. The existing ground surface elevation along the planned roadway alignment ranges from about 2,180 to 2,540 feet.

Our engineer performed a visit on March 29, 2018 to examine the terrain, existing roadway conditions, geologic features, and to look for evidence of old or existing landslides and groundwater springs. Cut and fill slopes of existing roadways in the area appeared to be stable. No landslides or groundwater springs were observed. There were indications of some active rock fall in a few of the exposed cut slopes and rock outcrops. The low-lying areas adjacent to an existing creek between Stations 304+50 to about 310+00 appeared to be wet and swampy. It is likely that the soils in this area consist of soft, wet alluvial soils. Some undercutting of soft soils and use of select rock fill will likely be necessary in this area to provide adequate stability for the planned fill embankment. The culvert planned to carry the creek under the new roadway may also require undercutting and placement of select rock fill to control settlement.

Numerous existing roadway cut slopes and rock outcrops were examined in the project area to assess the rock strata types likely to be encountered in the project cuts. Following is a summary of the rock types observed and the approximate corresponding elevation range

| Approximate Elevation Range | Observed Rock Strata Description |
| :---: | :--- |
| 2,170 to 2,300 feet | Primarily soft to medium hard shale with some thin <br> interbedded sandstone layers. Sandstone layers visible in this <br> zone appeared to be thinly bedded to blocky and susceptible <br> to rock fall. |
| 2,300 to 2,360 feet | Massive bedded hard sandstone of good quality. |
| 2,360 to 2,500 feet | Primarily soft to medium hard shale with some thin <br> interbedded sandstone layers. |
|  |  |

Based on observations of existing roadway cut slopes in the area, we expect the soil overburden will likely be about 10 ft . or less in thickness in the planned cut slope sections except in areas where old strip spoil fill is suspected at the western end of the project. We anticipate that $2 \mathrm{H}: 1 \mathrm{~V}$ cut slopes in the soil overburden will have adequate stability. Hard sandstone bedrock encountered in the approximate elevation range for 2,300 to 2,360 feet would likely classify was WVDOH Type 1 rock and could be sloped at $1 / 4 \mathrm{H}: 1 \mathrm{~V}$. Most of the remaining rock strata observed at the site would fall in the range of Type 3 and Type 4 bedrock. For preliminary design purposes, we recommend the following cut slope configuration considerations:
> The cut slopes should be designed in accordance with guidelines provided in the West Virginia Division of Highways, Design Directive 403 and considering the various soil and bedrock strata present at the site. The cut slope design should consists of a series of benches and slopes, with the slope ratio and height between benches depending on the type of material to be excavated
> For preliminary design, we recommend assuming an overall vertical interval between rock benches of 40 feet and rock bench widths of 20 ft . with a $15: 1(\mathrm{H}: \mathrm{V})$ slope toward the roadway. We recommend an overall rock cut slope of $1 \mathrm{H}: 1 \mathrm{~V}$ except for the interval where massive hard sandstone was observed (approximate elevation range for 2,300 to $2,360 \mathrm{ft}$.) The upper 10 ft . of cuts should be assumed to be soil material sloped at a $2 \mathrm{H}: 1 \mathrm{~V}$ ratio to Station $358+00$. Beyond Station $358+00$ to the end of the project, it is expected that the cuts will encounter some strip mine spoil fill which should be graded no steeper than $2 \mathrm{H}: 1 \mathrm{~V}$. We recommend an assumed soil overburden thickness in this strip-mined area of 50 feet

## Stratigraphy and Structure

Geologic data was obtained from various sources including the West Virginia Geologic and Economic Survey (WVGES) in Morgantown, WV, the Geologic Map of West Virginia (WVGES, 1968, revised 1986) and online resources provided by the WVGES. Near-surface strata in the project vicinity belong to the lower New River Formation and upper Pocahontas Formation of the Pennsylvanian System. The New River formation is composed primarily of sandstone, with lesser amounts of shale, siltstone and several minable coal seams, including the Sewell, Beckley, Fire Creek, and Pocahontas No. 8 and No. 9 Coals. The Flattop Mountain Sandstone marks the boundary between the New River and underlying Pocahontas Formation, which is also comprised primarily of sandstone and includes the Pocahontas No. 1 through 7 coals.

Geologic mapping indicates there are no major structural features located along the project alignment Structural contours of the base of the Beckley coal indicate strata in the area are dipping gently to the northwest

## Mining Information

Mining research was conducted using the WVGES internet database. According to readily available information, the Beckley seam has been surface and deep mined in the project area. The mined areas occur along the western end of the project alignment between approximate Station 350+00 and 380+00. The deep mine workings are old room-and-pillar operations carried out in the 1940's. The elevation of the Beckley seam varies between approximately 2,360 and 2,480 feet in this area.

Based on the mining data collected from this study, it appears that some strip mine spoil will be encountered between Station $358+00$ to the end of the project. It appears that the planned roadway cuts will come within close proximity but will miss the deep mine workings from approximate Station $350+00$ to 360+00

## SECTION 6-ENVIRONMENTAL OVERVIEW

The WVDOH has Skelly \& Loy, Inc currently under contract to prepare an environmental assessment (EA) for the project. The EA will fully explain the purpose and need for the project, examine a range of alternatives, identify potential impacts, and document agency and public participation. The EA is expected to be completed in mid to late 2018. A narrative of the Environmental Impacts is not included in this report since it will be addressed in the Environmental Assessment prepared by Skelly \& Loy

## SECTION 7 - TRAFFIC ANALYSIS

HDR Engineering, Inc has prepared a separate Draft Traffic Study evaluating the current and future traffic conditions along the Z-Way. The Traffic Study also assesses the impacts to Interstate I-64 and the interchange modifications to I-64 Exit 124. In addition, an extensive Traffic analysis was performed using the VISSIM Traffic Simulation Model.

## Appendix A - Evaluation Matrix

| Beaver - S Eisenhower Drive Alignment Alternative Evaluation/Cost Matrix |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Impact Category | CDM Smith Alternative No. 1 - Overpass | CDM Smith Alternative No. 1-At Grade | CDM Smith Alternative No. 2 | CDM Smith US 19 Connector | Gates Alternate Alignment |
| Engineering |  |  |  |  |  |
| Prelim. Length | 9,800 | 9,800 | 8,300 | 2,100 | Mailine 10,093', Side Roads 3,340 |
|  | 1.86 | 1.86 | 1.57 | 0.40 | 2.54 |
| Roadway Conifuration | 2(12' Lanes) $14^{\text {' Continuous Lef Tum Lane 6' Paved Shoulders }}$ | 2(12' Lanes) $14^{\text {C }}$ Continuous Left Tum lane 6' Paved Shouliers | 2 (12' Lanes) $14{ }^{4}$ ' Continuous Left Turr Lane 6 ' Paved Shoulders | 2 (12' Lanes) $14^{\prime}$ Continuous Left Turn Lane 2' Gutter with Curb | 2(11' Lanes) $14^{\prime}$ Continuous Left Tum lane 6 ' Paved Shoulders |
| Horizontal Geometry (Min Radius) | 6000' | 6000' | 1855' | ${ }^{371}$ | 711 |
| Financial / Costs |  |  |  |  |  |
| Estimated Risth of Way Accuisition Costs | \$10,275,000 | \$9,985,000 | 59,985,000 | \$2,760,000 | ? |
| Stimated Uliliy Relocation Cost | 55,250,000 | 55,25,000 | \$5,25,000 | 55,250,000 | ? |
| Estimated Construction Cost | 534,016,570 | 549,957,028 | 59,3,31,480 | \$5,15, , 83 | 539,873,589 |
| Stimated Total Propiect Cost | S62,711,053 (Includes US 19 Connecrior) | 578,361,511 (licludes Us 19 Connetor) | S67, 735,963, (necludes U5 19 Connector) | S13,169,483 | , |
| Traffic Operations |  |  |  |  |  |
| Number of Local Roadway Severed | None | None | None | None | 6 |
| Safety Constraints / Impacts | New Alignment that connects to the $1-64 /$ Eisenhower interchange. Provides an overpass at WV 307/Airport Road. | New Alignment that connects to the 1-64/Eisenhower Interchange. Provides an at grade intersection with WV 307/Airport Road. | New Alignment that connects to the 1-64/Eisenhower interchange. Provides an overpass at WV 307/Airport Road. Due not meet current geometric design criteria. | New Aligrment that conneets to the $1.69 /$ /isenthower Interchange. Provides an overpass at WV 307/Airport Rood. Due to the close proximity of US 19, a comnector road to US 19 is not feasable. | New Alignment that connects to the I-64/Eisenhower Interchange. Provides an at grade intersection with WV 307/Airport Road. |
| Human Environment |  |  |  |  |  |
| Historic Resource Impacts | None | to be detremined | to be determined | to bedetermined | to be detremined |
| Cemetery impats | None | to be detremined | to be determined | to bedetermined | to be dettrmmeo |
| Industrial Failities Impacts le.g. Chemical Plant) | None | None | None | None | None |
| Commercial facitities Impacts ( e.8.8. Businesses) | ${ }^{13}$ | ${ }^{13}$ | ${ }^{13}$ | ${ }^{13}$ | 6 |
| Residential Displacement (fh houses) | 14 | 14 | 14 | 18 | 10 |
| Potential Land Development | None | to be dettrmineo | to be determineo | to bedetremined | to be dettrmineo |
| Physical Impatts |  |  |  |  |  |
| Potential Hazard Weste Sitefs) | None | Impacts to Exising and distoric Serice Stations | Impacts to Exising and listoric Serice Stations | Impacts to exising and historic Service Stations | TO be detremmeo |
| Maior (Public) UVilit Conficts / Impats | None | Meior Utility Relocations Required | Maior Utitity Relocations Required | Major Utility Relocations Required | Maior Uritity Elocations Required |
| Maior (Private) Utility Conflicts / Impacts | None | to be detremined | to be determineo | to bedetremined | to be determineo |
| Potential Stream impacts | 72 LF | ${ }^{55}$ LF | ${ }_{55}$ LF | None | 1000 LF |

## Appendix B - Design Criteria Summary

| US 19 Rural Arterials Two-Lane Arterial | do design criteria | ReCommended | SOURCE(S), COMMENTS, JUSTIFCACAION |
| :---: | :---: | :---: | :---: |
| Lane Widths | 11'-12' Lanes | 11'-12' Lanes | DD-601, Pg 10 of 24, Table 7-3 <br> (ADT > 2000) Lanes to transition from $12^{\prime}$ to $11^{\prime}$ south of ramps |
| Shoulder Widths | 6'-8' Shoulders | $6^{\prime} 88$ ' Shoulders | DD-601, Pg 10 of 24, Table 7-3 <br> (ADT > 2000) Shoulder to transition from $8^{\prime}$ to $6^{\prime}$ south of ramps |
| Travel Lanes | 2 Lanes | 2 Lanes (plus Auxillary Lanes) | Trafic Study |
| Cross Slopes (Minimum) | 2.0\% | 2.0\% | DD-601, Pg 12 of 24 |
| Cross Slope (Maximum) | 4.0\% | 4.0\% | Provided by DOH using urban criteria DD-610, Pg 6 of 8 |
| $\begin{array}{\|l\|l} \hline \text { Bridge Widths (Two-Lane } \\ 3 & \text { Facilities) } \\ \hline 3 \end{array}$ | N/A | N/A | N/A |
| Minimum Radius | $711{ }^{\text {' }}$ | 711 ' | DD-601, Pg 10 of 24; 2011 AASHTO Green Book, Pg 3-32, Table 3-7 |
| Vertical Grades (Minimum) | 0.5\% | 0.5\% | 2011 AASHTO Green Book, Pg 3-119 |
| vertical Clearance (Minimum) | $16.5{ }^{\prime}$ | 16.5' | DD-601, Pg 11 of 24 Including an additional $0.5^{\prime}$ for future overlays |
| Design Speed | 45 MPH | 45 MPH | Design Speed provided by DOH |
| Stopping Sight Distances (Minimum) | 360' | 360' | DD-601, Pg 10 of 24; 2011 AASHTO Green Book, Pg 7-3, Table 7-1 |
| Vertical Curves K-Value Crest | 61 | 61 | 2011 AASHTO Green Book, Pg 3-155, Table 3-34 |
| Vertical Curves K-Value Sag | 79 | 79 | 2011 AASHTO Green Book, Pg 3-161, Table 3-36 |
| $\begin{aligned} & \text { Vertical Grades } \\ & \text { (Maximum) } \end{aligned}$ | 7\% | 7\% | DD-601, Pg 10 of 24; 2011 AASHTO Green Book, Pg 7-4, Table 7-2 |
| \% Clear Sidewalk Width | $\mathrm{N} / \mathrm{A}$ (Paved Shoulder) | N/A (Paved Shoulder) | DD-813 Pg 8 or9 |
| 运 Clear-Zone Widths | 12'-14' | 12'-14' | DD-601, Pg 11 of 24; AASHTO Roadside Design Guide, Pg 3-3 |


| $\begin{gathered} \text { Jughandle } \\ \text { Interchange Ramp } \end{gathered}$ | DD DESIGN CRITERIA | recommended | SOURCE(S), COMMENTS, Justification |
| :---: | :---: | :---: | :---: |
| Lane Wioths | 15'-16' Lanes | 15'16' Lanes** | DD-602, Pg 1 of 1 <br> *Due to radius < 200', lane widths to be evaluated with turning templates |
| Shoulder Widths | Rt: $8^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a 5 ' paved section LT: $4^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a 3' paved shoulder | Rt: $8^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a $5^{\prime}$ paved section LT: 4'-0' ${ }^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a $3^{\prime}$ paved shoulder | DD-602, Pg 1 of 1 |
| Travel Lanes | $1-2$ | 1.2 | DD-602 Pg 1 of 1; Traffic study |
| Cross Slopes (Minimum) | 2.0\% | 2.0\% | Do-601, Pg 9 of 24 |
| Cross Slope (Maximum) | 4.0\% | 4.0\% | Provided by DOH using urban criteria DD-610, Pg. 6 of 8 |
| $\begin{array}{\|l} 3 \\ \frac{3}{2} \\ \text { Bridge Widths (Two-Lane } \\ \text { Facilities) } \end{array}$ | N/A | N/A | N/A |
| 僦Minimum Radius | 533 -42' | 533'-150' | DD-601, Pg 10 of 24; 2011 AASHTO Green Book, Pg 3-32, Table 3-7 |
| $\begin{array}{\|l} \begin{array}{l} \text { Vertical Grades } \\ \text { (Minimum } \end{array} \end{array}$ | 0.5\% | 0.5\% | DD-610, Pg 5 of 8 |
| Vertical Clearance (Minimum) | 16.5' | 16.5' | DD-601, Pg 8 of 24 <br> Including an additional 0.5 ' for future overlays |
| Design Speed | 40 MPH to Stop Condition ( 15 MPH ) | 40 MPH to Stop Condition ( 15 MPH ) | 2011 AASHTO Green Book, Pg 10-89 Table 10-1 |
| Stopping Sight Distances (Minimum) | 305'-80' | 305-80' | DD-601, Pg 10 of 24, 2011 AASHTO Green Book, Pg 7-3, Table 3-7, AASHTO Green Book Pg 3 155, Table 3-34 |
| Vertical Curves K-Value Crest | 44-3 | 44-3 | 2011 AASHTO Green Book, Pg 3-155, Table 3-34 |
| Vertical Curves <br> K-Value Sag | 64-10 | 64-10 | 2011 AASHTO Green Book, Pg 3-161, Table 3-36 |
| Vertical Grades <br> (Maximum) | 5\%-8\% | 5\% | DD-610, Pg 3 of 8, Table 7-4 |
| \% Clear Sidewalk Width | N/A | N/A | DD-610, Pg 8 of 8; DD-8813 Pg 8 of 9 |
| a clear-zone Widths | 122-14' | 12'-14' | DD-601, Pg 5 of 24; AASHTO Roadside Design Guide, $\operatorname{Pg}$ 3-3 |



| 1-64 WB Exit Ramp Interchange Ramp | DD DESIGN CRITERIA | RECOMMENDED | SOURCE(S), COMMENTS, JUSTIFICATION |
| :---: | :---: | :---: | :---: |
| Lane Widths | $16^{\prime}$ | $16^{\text {' }}$ | DD-602, Pg 1 of 1 |
| Shoulder Widths | Rt: $8^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a 5 ' paved section LT: $4^{\prime}-0$ " to face of guardrail or intersection of slope without guardrail; with a $3^{\prime}$ paved shoulder | Rt: $8^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a 5 ' paved section LT: 4 $\mathrm{O}^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a $3^{\prime}$ paved shoulder | DD-602, Pg 1 of 1 |
| Travel Lanes | 1 | 1 | DD-602, Pg 1 of 1; Traffic Study (Match Existing) |
| Cross Slopes (Minimum) | 2.0\% | 2.0\% | DD-601, Pg 9 of 24 |
| Cross Slope (Maximum) | 8.0\% | 8.0\% | DD-601, Pg 9 of 24 |
| Bridge Widths (Two-Lane Facilities) | N/A | N/A | N/A |
| Minimum Radius | $\begin{aligned} & 587^{\prime} \\ & \left(388^{*}\right) \end{aligned}$ | $\begin{aligned} & 1390^{\prime} \\ & \left(300^{*}\right) \end{aligned}$ | DD-601, Pg 10 of 24; 2011 AASHTO Green Book, Pg 3-32, Table 3-7 |
|  | 0.5\% | 0.5\% | DD-610, Pg 5 of 8 |
| Vertical Clearance (Minimum) | 16.5' | 16.5' | DD-601, Pg 8 of 24 <br> Including an additional $0.5^{\prime}$ for future overlays |
| Design Speed | $\begin{gathered} 45 \mathrm{MPH} \\ \left(15 \mathrm{MPH}^{*}\right) \end{gathered}$ | $\begin{gathered} 45 \mathrm{MPH}^{\left(15 \mathrm{MPH}^{*}\right.} \end{gathered}$ | 2011 AASHTO Green Book, Pg 10-89 Table 10-1; DD-624; Ramp Deceleration length table (mainline design speed $=75 \mathrm{MPH}$ ) |
| Stopping Sight Distances (Minimum) (Minimum) | $\begin{gathered} 360^{\prime} \\ \left(80^{* *}\right) \end{gathered}$ | $\begin{array}{r} 360^{\circ} \\ \left(80^{* *}\right) \\ \hline \end{array}$ | DD-610, Pg 2 of 8, Table 3-1 |
| Vertical Curves K-Value Crest | $\begin{aligned} & 61 \\ & \left(3^{*}\right) \end{aligned}$ | ${ }^{61}$ | 2011 AASHTO Green Book, Pg 3-155, Table 3-34 |
| Vertical Curves <br> K-Value Sag | $\begin{gathered} 79 \\ \left(10^{*}\right) \\ \hline \end{gathered}$ | $\begin{gathered} 79 \\ \left(10^{*}\right) \\ \hline \end{gathered}$ | 2011 AASHTO Green Book, Pg 3-161, Table 3-36 |
| Vertical Grades (Maximum) <br> (Maximum) | 5\%-8\% | $\begin{gathered} 7 \% \\ \left(7 \%{ }^{*}\right) \\ \hline \end{gathered}$ | 2011 AASHTO Green Book Pg 10-92 |
| \% Clear Sidewalk Width | N/A | N/A | Interstate Ramp |
| \% Clear-Zone Widths | 12'-14' | 12'-14' | DD-601, Pg 5 of 24; AASHTO Roadside Design Guide, Pg 3-3, Table 3-1 |


|  | $1-64$ EB Entrance Ramp Interchange Ramp | do design critrria | recommended | SOURCE(S), COMMENTS, JUSTIFICATION |
| :---: | :---: | :---: | :---: | :---: |
|  | Lane Widths | $15^{\prime}$ | $15^{\prime}$ | DD-602, Pg 1 of 1 |
|  | Shoulder Widths | Rt: $8^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a $5^{\prime}$ paved section LT: $4^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a $3^{\prime}$ paved shoulder | Rt: $8^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a $5^{\prime}$ paved section LT: $4^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a $3^{\prime}$ paved shoulder | DD-602, Pg 1 of 1 |
|  | Trav | 2 | 2 | DD-602, Pg 1 of 1; Traffic Study (Match Existing) |
|  | Cross Slopes (Minimum) | 2.0\% | 2.0\% | DD-601, Pg of 24 |
|  | Cross Slope (Maximum) | 8.0\% | 8.0\% | DD-601, Pg of 24 |
| $\left\lvert\, \begin{aligned} & \frac{3}{3} \\ & \left.\begin{array}{l} 3 \\ 0 \\ 0 \end{array} \right\rvert\, \end{aligned}\right.$ | Bridge Widths (Two-Lane Facilities) | N/A | N/A | N/A |
|  | Minimum Radius | 758-76' | $758{ }^{\prime}$ | DD-601, Pg 10 of 24; 2011 AASHTO Green Book, Pg 3-32, Table 3-7 |
|  | Vertical Grades (Minimum) | 0.5\% | 0.5\% | DD-610, Pg 5 of 8 |
|  | Vertical Clearance (Minimum) | $16.5{ }^{\prime}$ | $16.5{ }^{\prime}$ | DD-601, Pg 8 of 24 Including an additional $0.5^{\prime}$ for future overlays |
|  | Design Speed | $50 \mathrm{MPH}-20 \mathrm{MPH}$ | $50 \mathrm{MPH}-20 \mathrm{MPH}$ | Posted Advisory Speed $=25$ MPH; 2011 AASHTO Green Book Pg 10-89 (20 MPH at grade terminal) |
|  | stopping Sight Distances (Minimum) | ${ }^{425}$-115' | $4^{45}$-115' | DD-610, Pg 2 of 8, Table 3-1 |
|  | Vertical Curves K-Value Crest | 84.7 | 84 | 2011 AASHTO Green Book, Pg 3-155, Table 3-34 (Approaching interstate) |
|  | $\begin{aligned} & \text { Vertical Curves } \\ & \text { K-Value Sag } \\ & \hline \end{aligned}$ | -17 | 17 | 2011 AASHTO Green Book, Pg 3-161, Table 3-36 (At grade ramp terminal) |
|  | Vertical Grades | 5\%-8\% | 5\% | 2011 AASHTO Green Book, Pg 10-92 |
|  | clear Sidewalk Width | N/A | N/A | Interstate Ramp |
|  | e Widths | 12'-14' | ${ }^{12^{2}-14{ }^{\prime}}$ | DD-601, Pg 5 of 24 ; AASHTO Roadside Design Guide, Pg 3-3, Table 3-1 |


| 1-64 EB Exit Ramp Interchange Ramp | DD DESIGN CRITERIA | RECOMMENDED | SOURCE(S), COMMENTS, JUSTIFICATION |
| :---: | :---: | :---: | :---: |
| Lane Widths | $15^{\prime}-16^{\prime}$ | 15'-16' | DD-602, Pg 1 of 1; Tapers to 2-15' lanes |
| shoulder Widths | Rt: $8^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a 5 ' paved section LT: $4^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a ${ }^{\text {' }}$ paved shoulder | Rt: $8^{\prime}-0$ " to face of guardrail or intersection of slope without guardrail; with a 5 ' paved section LT: $4^{\prime}-0^{\prime \prime}$ to face of guardrail or intersection of slope without guardrail; with a 3' paved shoulder | DD-602, Pg 1 of 1 |
| Travel Lanes | 1 | 1 | DD-602, Pg 1 of 1; Traffic Study (Match Existing) |
| Cross Slopes (Minimum) | 2.0\% | 2.0\% | DD-601, Pg 9 of 24 |
| Cross Slope (Maximum) | 8.0\% | 8.0\% | D-601, Pg 9 of 24 |
| $\begin{array}{\|l}  \\ \\ =3 \\ 3 \end{array}$ | N/A | N/A | N/A |
| \% Minimum Radius | 134' | 200' | DD-601, Pg 10 of 24; 2011 AASHTO Green Book, Pg 3-32, Table 3-7 |
| vertical Grades (Minimum) | 0.5\% | 0.5\% | DD-610, Pg 5 of 8 |
| vertical Clearance (Minimum) | $16.5{ }^{\prime}$ | 16.51 | DD-601, Pg 8 of 24 <br> Including an additional $0.5^{\prime}$ for future overlays |
| Design Speed | 25 MPH | 25 MPH to Stop Condition (20 MPH) | Mainline Posted Speed $=70 \mathrm{MPH} ; 2011$ AASHTO Green Book Pg 10-89 (Loop Ramps) |
| Stopping Sight Distances (Minimum) | 155'-115' | 155'-115' | DD-610, Pg 2 of 8, Table 3-1 |
| Vertical Curves K-Value Crest | 12-7 | 12-7 | 2011 AASHTO Green Book, Pg 3-155, Table 3-34 |
| $\begin{array}{\|l} \begin{array}{l} \text { vertical Curves } \\ \text { k-value Sag } \end{array} \\ \hline \end{array}$ | 26-17 | 26-17 | 2011 AASHTO Green Book, Pg 3-161, Table 3-36 |
| Vertical Grades (Maximum) | 5\%-8\% | 5\% | 2011 AASHTO Green Book, Pg 10-92 |
| \% Clear Sidewalk Width | N/A | N/A | Interstate Ramp |
|  | 12'-14' | 12'-14' | DD-601, Pg 5 of 24; AASHTO Roadside Design Guide, Pg 3-3, Table 3-1 |

## Appendix C - Construction Cost Estimate

|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TEEM NUMEER | \|ancom | Descripton | UnT | quantry | unt price | amount |
| 201000-000 |  |  | 15 | 1 | (4000,00000 | 5400.000 |
| 202001.000 |  | BUIIONG DEMOLTION NUMBER, | 15 | 22 | S5,000.00 | 5110,000 |
| 20600.000 |  | Nosaliatos | 15 | 1 | 5100000000 |  |
| 200000.000 |  | мostlation | ${ }^{5}$ |  | 51,000,000.00 | 51,000,000 |
|  |  |  | $\stackrel{\text { cr }}{\text { cr }}$ | (198343 |  |  |
|  |  | Aabric for sparation | s\% |  |  | 16 |
| ${ }^{3070002.000}$ |  |  | c | ${ }^{14821}$ |  | ${ }_{5}^{51,111.575}$ |
| - 3 3077010000 |  |  | ¢ | ${ }^{108}$ | ${ }_{\text {che }}^{57500}$ | $\frac{58500}{521.450}$ |
|  |  |  |  |  |  |  |
|  |  |  | $\frac{68}{5 \gamma}$ | $\frac{450}{4550}$ | ${ }_{\substack{58.00}}^{54.00}$ | $\frac{5}{518.000}$ |
| 600002.001 |  | Cass b concrite | $\cdots$ | 12 | 51.00000 | 512000 |
| 604.TEMS |  | Dran ${ }^{\text {a }}$ E P PPES | 15 | 1 | S1125,00000 | S1,125000 |
| 605.revs |  | Orandage Incts | 15 | 1 | 52000000.00 | 5200,000 |
| 60609301] |  |  | ${ }^{\text {c }}$ | ${ }^{12375}$ | $\frac{51000}{5000}$ |  |
|  |  |  |  |  |  |  |
| 667001501 |  |  | ${ }_{\text {EA }}$ | $\frac{5150}{9}$ | ${ }_{5}^{515000}$ | $\frac{57,7,50}{59,00}$ |
| 6.10033 .033 <br> 6.1003 .004 |  |  |  | ${ }^{658}$ | $\frac{54500}{\substack{542.00}}$ | $\frac{597610}{514,12}$ |
| 622003.001 |  | CANTL EVER MA M BOX SUPPORT | ${ }_{\text {EA }}$ | 20 | S330.00 | 56,000 |
| ${ }_{6} 633003.001$ |  | OUMP ED ROCK GUTER | c | 500 | S60,00 | S30,000 |
| 636.1TMS |  | MANTEAACE OF F TRAFFIC | 15 | 1 | \$188,000.00 | 5180,000 |
| 6370001.001 |  | WATER For oust pallative | MG | ${ }^{300}$ | S50,00 | S15,000 |
| 638002.001 |  | RGGHT OF WAY MARKER | EA | 102 | S100000 | 510200 |
|  |  | Sufver MARKER | ${ }^{\text {EA }}$ | ${ }^{100}$ | ${ }_{5}^{530000}$ | $\frac{530000}{500}$ |
|  |  | OUTLET MABRER | ${ }^{\text {EA }}$ |  |  |  |
| 639001-001 |  | Constructov AYOUT STAKE | ${ }^{15}$ | 1 | \$100,00,00 | 5100,000 |
|  |  |  | No | $\frac{15}{1}$ | ${ }_{\text {Sta }}^{5200000}$ |  |
| 642 TEMS |  | TEMPOAAAY PROIECT WATER POLUTON CONTTOL | 15 | 1 | S590,000.00 | S390000 |
| 652.TEVS |  | SEEONG ANO MUCHMNG | ${ }^{15}$ | 1 | S85,000,00 | 585,000 |
| 699000.001 |  | ONIOBTRANNG | HR | 2000 | 50.80 | 51,600 |
|  |  | ASPHAIT PAVEMENT |  |  |  |  |
| 401001-040 |  | SUPEPPAVE ASEE C CSE, SG, TV 19 | TN | 9673 | 5100.00 | 59623,300 |
| 401001.050 |  | SUP PRPAVE EASE CRSE S SG, TV 375 | TN | 23349 | 5100.00 | 52983,900 |
| 402001.040 |  | SUPRPRAVE SKI PVT, SG, TV 95 | TN | ${ }^{4786}$ | 510000 | 5478,600 |
| 401003 -011 |  |  | TN | ${ }^{9}$ | S10000 | S9,50 |
| 63602-001 |  | AGGREGATE FOR MANTAN NG TRAFFCC, STOOV OR GRAVEL | TN | 2000 | 535.00 | 570,000 |
|  |  | RENFORCE COCONCRETE BOX CUIVERTS |  |  |  |  |
|  |  |  | $\frac{\mathrm{Cr}}{18}$ | ${ }^{\frac{1}{1250}}$ | $\frac{580000}{51.50}$ | $\frac{59000}{\frac{580}{533750}}$ |
| 6033929001 |  |  | ${ }_{5}$ | ${ }^{168}$ |  | ${ }_{516800}$ |
| 660470. ${ }^{6048}$ |  |  | $\frac{4}{4}$ | ${ }^{\frac{216}{84}}$ | ${ }_{\text {S }}^{5200000000}$ | ${ }^{\frac{5}{5184000}}$ |
| 639001.001 |  | onstructo ( AVOUT STARE | 15 |  | 510,00000 |  |

## CONSTRUCTION COST ESTIMAT <br> ONSTRUCTION COST ESTIMATE Federal Project: STP-0019(429)D <br> Federal Project: STP-0019(4299) State Project: X341-ZWAN-6.2202 BEAVER-SOUTH EISENHOWER DR.

| TIEM NMmber |  | osccipmon | unt | quavitr | Untrpace | amount |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SICNIG, SIINAL \& PAVEMENT M MAKINGS |  |  |  |  |
| 657-TEMS |  | ROAOS SE E NOUNTEOS SGV SUP Poort | 15 | 1 | 580,000.00 | 580,000 |
| 660.TTENS |  | Trafele Sligals per locaton | If | 2 | S15000000 | 5390000 |
| 661-TENS |  | Trafic sins ano delu | 15 | 1 | S85000000 | 585000 |
| 663.-TENS |  | MICClIANEOUS PAVEMENT MABRINGS | 15 | 1 | 5210,000.00 | 5210,000 |
|  |  | Water reocaton |  |  |  |  |
| 6 639001-001 |  | CONSTRUCTON A AVOUTSAAEE | 15 | 1 | S1000000 | 510,000 |
| 670004 - |  | 24 INCHOUCTIE RON PPE | IF | ${ }^{740}$ | 5200.00 | 5148,000 |
| 670007. |  | 6INCH Plastic Ppe | 15 | 1.300 | S5500 | 577.500 |
| 677007 . |  | 141 NCHP Pastic P PE | 1 If | 250 | 5180.00 | 5455000 |
| 675021 - |  | 3 Cl | ${ }_{\text {IF }}$ | 250 | 5250.00 | 562,500 |
| 675021 - |  | ${ }^{\text {A8 }}$ NCHC CASING PDE | If | 155 | 5220.00 | 565,100 |
|  |  | SANTIARY SEw ER REIOCATON |  |  |  |  |
| 639001.001 |  | CONSTRUCTON ATVOT STAEE | 15 | 1 | 510,000.00 | S10,000 |
| $675007 \cdot 022$ |  | 8 NCH PASTT C SEW ER P PE | ${ }^{15}$ | 1500 | 540,00 | 560,000 |
| 6 65014.001 |  |  | ${ }^{\text {EA }}$ | 10 | \$4500.00 | 545,000 |
| 675015.001 |  | OROP MANHOLE COMPIEEE, INCUOOING CASTNG | EA | 2 | \$5,50,00 | 511,000 |
| 675017.001 |  | ABANOONIGG MANHOIE | ${ }_{\text {EA }}$ | 3 | 5700.00 | 52,100 |
|  |  | REINFORCED SOIL SLOPE |  |  |  |  |
|  |  | (REEORANMG EASE TRENCH | $\frac{4}{4}$ | $\frac{250}{30}$ | ${ }_{\substack{510.00 \\ 520.00}}$ | ¢ |
|  |  |  |  |  | S10,00000 |  |
|  |  |  | $\frac{\text { sv }}{5 \gamma}$ | $\frac{8000}{4800}$ | ${ }_{\substack { \text { Sina00 } \\ \begin{subarray}{c}{13.00{ \text { Sina00 } \\ \begin{subarray} { c } { 1 3 . 0 0 } }\end{subarray}}$ |  |
|  |  | (ther ${ }_{\text {STRUCTURE }}$ |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  | W 307 OVE EPPASS [ESTM MATED AT S300 Per Se] | 15 | 1 | 51,500,000000 | S1,500,000 |
|  |  | INTERCAANGE |  |  |  |  |
| ${ }^{2027001.001}$ |  | UNCCASSA EED ExCavation | c | ${ }^{331601}$ |  |  |
| 207023000 |  | SABRC | ${ }_{\text {ch }}$ | ${ }^{\frac{31503}{3073}}$ | ¢ | $\frac{5856000}{561 / 06}$ |
| ${ }^{3110066001}$ |  | OPAN GRADE FRRE DRA N NG BASE COUSSE | c | 3414 | S125.00 | 5446,750 |
| 501001.010 |  |  | 57 | 30703 | 5110.00 | 533,372330 |
|  |  |  | $\frac{15}{15}$ | $\frac{1}{1}$ | $\frac{510000000}{530.0000}$ | $\frac{5120000}{53000}$ |
| 607001-001 |  | Troet GUAPbrall Class | 18 | 1479 | 51500 | ${ }^{522,185}$ |
| 610006.005 |  | MEDAN, TPPEV | 18 | ${ }^{652}$ | 55500 | 5335860 |
| 636 teNs |  | NANTENANC: Of Traflic | 15 | 1 | 5225,00,00 | 322,000 |
| 6427 TEMS |  | TEMPOAARY PROIECT WATER Polluton Control | 15 | 1 | 575,00000 | 575000 |
| 652.TEVS |  | SEEDNG ANO MUCHMNG | 15 | 1 | 555,00000 | 525000 |
|  |  |  | $\stackrel{\text { Ef }}{\text { EA }}$ | 2 | ${ }_{\text {Slisa,00.00 }}$ | $\frac{5300000}{}$ |
|  |  |  |  |  |  |  |

ENGINERPINGECONTIGENCY 13

grand total

## Appendix D - Acquisition Tables

| Parcel no. | $\begin{gathered} \text { PLAN } \\ \text { SHEET No. } \end{gathered}$ | titie holder | RECORDED |  | AREA - SQ. FT. (UNLESS OTHERWISE NOTED) |  |  |  |  |  |  |  |  |  | remarks | R/W DEED RECORD |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | deed book | page no. | tract no. | C/A | non-c/A | EASEMENT |  | Remaling |  |  | total taken | parcel total |  | DEED <br> BOOK | page no. |
|  |  |  |  |  |  |  |  | TYPE | AREA | Left | RIGHT | total |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 |  | Willie G. Foster, et al | 461 | 128 |  |  | 4,300 |  |  | 0 | 11,625 | 11,625 | 4,300 | 15,925 | Parcel total from deed |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 |  | MCNB Banks, Inc. | 5019 | 1408 |  |  | $\begin{gathered} \hline 0.13 \mathrm{Ac} . \\ 5.693 \\ \hline \end{gathered}$ |  |  | 3.66 Ac . | 0 | 3.66 Ac . | $\begin{gathered} \hline 0.13 \mathrm{Ac} . \\ 5.693 \\ \hline \end{gathered}$ | 3.7894 Ac . | PARCEL TOTAL FROM DeEd |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3-1 |  | Robert G Stoddard and Susan Stoddard | 5050 | 5019 |  |  | $\begin{gathered} 0.051 \mathrm{Ac} . \\ 2,244 \\ \hline \end{gathered}$ |  |  | 0 | $\begin{array}{\|c} \hline 0.198 \mathrm{AC} . \\ 8,625 \end{array}$ | $\begin{gathered} \hline 0.198 \mathrm{Ac} . \\ 8,625 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 0.051 \mathrm{Ac} . \\ 2,244 \\ \hline \end{gathered}$ | $\begin{array}{\|c\|} \hline 0.250 \mathrm{Ac} . \\ 10.873 \\ \hline \end{array}$ | PARCEL TOTAL FROM DeEd |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3-2 |  | Robert Stoddard and Susan Stoddard | 5058 | 4729 |  |  | $\begin{array}{\|c} \hline 0.074 \mathrm{Ac} . \\ 3.236 \\ \hline \end{array}$ |  |  | 0 | $\begin{gathered} 0.411 \mathrm{AC} . \\ 17.903 \\ \hline \end{gathered}$ | $\begin{array}{c\|} \hline 0.411 \mathrm{Ac} . \\ 17.903 \\ \hline \end{array}$ | $\begin{gathered} \hline 0.074 \mathrm{Ac} . \\ 3,236 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 0.485 \mathrm{Ac} . \\ 21,097 \\ \hline \end{gathered}$ | PARCEL TOTAL FROM Deed |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  | Jose Rizo and Luisa Rizo | 5048 | 6899 |  |  | $\begin{array}{\|c} \hline 0.033 \mathrm{Ac} . \\ 1,422 \\ \hline \end{array}$ |  |  | 0 | $\begin{array}{\|c} \hline 0.234 \mathrm{Ac} . \\ 10.193 \\ \hline \end{array}$ | $\begin{gathered} \hline 0.234 \mathrm{Ac} . \\ 10.193 \\ \hline \end{gathered}$ | $\begin{array}{\|c} \hline 0.033 \mathrm{Ac} . \\ 1,422 \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline 0.267 \mathrm{Ac} . \\ 11.630 \\ \hline \end{array}$ | PARCEL TOTAL FROM deed |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  | J\&B Investments, LIC | 5054 | 1226 |  |  | 1.05 Ac . |  |  | 0 | $\begin{array}{\|c} \hline 0.114 \mathrm{AC.} \\ \hline 9949 \\ \hline \end{array}$ | 3.39 Ac . | 1.05Ac. | 4.44 Ac . | PARCEL TOTAL FROM Deed |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  | Stanley Kendrick and Shirley Kendrick | 5031 | 633 |  |  | $\begin{array}{\|c\|} \hline 0.114 \mathrm{Ac} . \\ 4949 \\ \hline \end{array}$ |  |  | 0 | 5.322 Ac. | 5.322 Ac . | $\begin{gathered} \hline 0.114 \mathrm{Ac} . \\ 4949 \\ \hline \end{gathered}$ | 5.436 Ac. | PARCEL TOTAL FROM DEED |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  | Judy A. Cole | 480 | 82 |  |  | $\begin{gathered} \hline 0.15 \mathrm{Ac} . \\ 6.568 \\ \hline \end{gathered}$ |  |  | 0 | 0 | 0 | $\begin{gathered} \hline 0.15 \mathrm{Ac} . \\ 6.568 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 0.15 \mathrm{Ac} . \\ 6.568 \\ \hline \end{gathered}$ | total take |  |  |
|  |  |  | WB5065 | 6454 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 |  | Joan Kountz | 727 | 849 | 1 |  | $\begin{gathered} \hline 0.088 \mathrm{Ac} . \\ 3,820 \\ \hline \end{gathered}$ |  |  | 0 | $\begin{array}{\|c\|} \hline 0.162 \mathrm{Ac} . \\ 7,070 \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline 0.162 \mathrm{Ac.} \\ 7.070 \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline 0.088 \mathrm{Ac} . \\ 3,820 \\ \hline \end{array}$ | $\begin{gathered} \hline 0.25 \mathrm{Ac} . \\ 10.890 \\ \hline \end{gathered}$ | PARCEL TOTAL FROM DeEd |  |  |
|  |  |  |  |  | 2 |  |  | TSRE | $\begin{gathered} 0.073 \mathrm{AC.} \\ \hline 3.175 \\ \hline \end{gathered}$ |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 |  | Brenda Tyree | 706 | 474 |  |  | $\begin{array}{\|c} \hline 0.080 \mathrm{Ac} . \\ 3,479 \\ \hline \end{array}$ |  |  | 0 | $\begin{array}{\|c\|} \hline 0.42 \mathrm{Ac} . \\ 18,295 \\ \hline \end{array}$ | $\begin{array}{\|c} \hline 0.42 \mathrm{Ac} . \\ 18,295 \\ \hline \end{array}$ | $\begin{gathered} \hline 0.080 \mathrm{Ac} . \\ \hline 3,479 \\ \hline \end{gathered}$ | 0.50 Ac . | PARCEL TOTAL UNABLE TO DETERMINE |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 |  | Beaver Coal Company, Limited | 5037 | 5289 | 1 |  | 10.80 Ac . |  |  | 1.80 Ac . | 952.42 Ac. | 954.22 Ac . | 13.778 Ac. | 968 Ac. | Parcel total from deed |  |  |
|  |  |  |  |  | 2 |  |  | PCCE | 2.88 Ac . |  |  |  |  |  |  |  |  |
|  |  |  |  |  | 3 |  |  | PCCE | $\begin{gathered} 0.098 \mathrm{Ac} . \\ \hline 4.271 \\ \hline \end{gathered}$ |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



| parcelno. | $\begin{array}{\|c} \text { PLAN } \\ \text { SHEET NO. } \end{array}$ | titie holotr | RECORDED |  | AREA - SQ. FT. (UNLESS OTHERWISE NOTED) |  |  |  |  |  |  |  |  |  | remarks | R/W deed record |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Detd book | page no. | tract no. | C/A | NoN-C/A | EASEMENT |  | remaining |  |  | total taken | parceltotal |  | $\begin{aligned} & \text { DEED } \\ & \text { Book } \end{aligned}$ | page no. |
|  |  |  |  |  |  |  |  | TYPE | AREA | Left | RIGHT | total |  |  |  |  |  |
| 20 |  | Thomas C. Booth | 5008 | 7013 | 1 |  | 0.07 AC . <br> 3019 |  |  | 0.295 Ac. <br> 12850 | 0 | 0.295 Ac. <br> 12.850 | $\begin{aligned} & 0.07 \mathrm{AC.} \\ & 3019 \end{aligned}$ | 0.365 Ac. | PARCEL TOTAL FROM DeEd |  |  |
|  |  |  |  |  | 2 |  |  | TSRE | $\begin{gathered} 0.08 \mathrm{Ac} . \\ 3,580 \\ \hline \end{gathered}$ |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 |  | RMR Service Center, LLC | 5051 | 1095 | 1 |  | 0.10 Ac . |  |  | 0.96 Ac | 0 | 0.96 Ac | 0.10 Ac . | 1.06 Ac. | Parcel total from deed |  |  |
|  |  |  |  |  | 2 |  |  | TCE | 0.05 Ac . |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 |  | State of West Virginia Department of |  |  | 1 |  |  | PE |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | 2 |  |  | PE |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 23 |  | 84 Properties, LLC | R9 | 865 | 1 |  | 0.29 Ac. |  |  | 4.18 Ac. | 0 | 4.18 Ac . | 0.32 Ac . | 4.50 Ac . | Parcel total from deed |  |  |
|  |  |  | 5064 | 498 | 2 |  |  | PDE | 0.03 Ac . |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 |  | Robert B. Orders, Jr. | 5024 | 4133 | 1 |  | 0.934 Ac . |  |  | 0.03 | 0.13 Ac . | 0.16 Ac | 0.934 Ac . | 1.094 Ac . | PARCEL TOTAL FROM deed |  |  |
|  |  |  |  |  | 2 |  |  | TSRE | 0.06 Ac. |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 |  | James L. Hern | 92 | 2282 | 1 |  | 8.95 Ac . |  |  | 21.64 Ac . | 9.32 Ac . | 31.05 Ac . | 9.04 Ac. | 40.0 Ac . | Parcel total from deed |  |  |
|  |  |  | 5006 | 980 | 2 |  | 0.09 Ac . |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | 3 |  |  | TSRE | 0.18 Ac. |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 |  | Richard H. Lilly, Alex H. Lilly and Joseph E. Lilly | R5007 | 9139 |  |  | 0.237 Ac . |  |  |  | 35.988 Ac. | 35.988 Ac . | 0.237 Ac . | 36.225 Ac. | PARCEL TOTAL FROM DeEd |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 |  | Minnie Gillenwater | 5010 | 2577 |  |  | 5.37 Ac . |  |  | 1.56 Ac . | 5.01 Ac . | 6.57 Ac . | 5.37 Ac . | 11.94 Ac . | Parcel total from deed |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 |  | Unknown (Private Drive) |  |  |  |  | $\begin{array}{\|c\|} \hline 0.007 \mathrm{Ac} . \\ 307 \\ \hline \end{array}$ |  |  |  |  |  | $\begin{gathered} 0.007 \mathrm{AC.} \\ 307 \\ \hline \end{gathered}$ |  | PARCEL TOTAL UNABLE TO DETERMINE |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 29 |  | Darick Shane Houck | 5000 | 9979 |  |  | $\begin{array}{\|c\|} \hline 0.029 \mathrm{AC} \\ 1.249 \\ \hline \end{array}$ |  |  | 13.742 Ac . | 0 | 13.742 Ac . | $\begin{gathered} \hline 0.029 \mathrm{AC} . \\ 1.249 \\ \hline \end{gathered}$ | 13.771 Ac. | Parcel total from deed |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Parcelno. | $\left.\right\|_{\text {SHEET NO }} ^{\substack{\text { PLAN }}}$ | titie holder | RECORDED |  | AREA - SQ. FT. (UNLESS OTHERWISE NOTED) |  |  |  |  |  |  |  |  |  | remarks | R/W DEED RECORD |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | deed book | page no. | tract no. | C/A | non-c/A | EASEMENT |  | remaining |  |  | total taken | parcel total |  | ¢ DEED | page no. |
|  |  |  |  |  |  |  |  | TPPE | AREA | Left | RIGHT | total |  |  |  |  |  |
| 30 |  | James Daniel and Tammy Daniel | 5065 | 7504 |  |  | 0.97 Ac . |  |  | 0.91 Ac . | 0 | 0.91 Ac . | 0.97 Ac . | 1.88 Ac . | PARCEL TOTAL CALCULATED |  |  |
|  |  | AKA James P. Daniel and Tammy Daniel | 5009 | 9270 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 |  | Charlotte L. Painter | 5003 | 9161 |  |  |  |  |  |  |  |  |  | 1.35 Ac . | PARCEL TOTAL CALCULATED |  |  |
| - |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 32 |  | Scott A. Hensley and Regina Beth Hensley | 5050 | 4935 |  |  | 7.27 Ac . |  |  | 1.17 Ac . | 0.91 Ac. | 2.08 Ac. | 7.27 Ac . | 9.346 Ac . | Parcel total from deed |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 33 |  | Richard Canterbury | 5021 | 2709 |  |  | 1.36 Ac . |  |  | 0 | $\begin{gathered} \hline 0.37 \mathrm{Ac.} \\ 16.117 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 0.37 \mathrm{Ac} . \\ 16.117 \\ \hline \end{gathered}$ | 1.36 Ac . | 1.73 Ac. | PARCEL TOTAL CALCULATED |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 34 |  | William G. Bihler and Wendy U. Bihler | 5019 | 963 | 1 |  | $\begin{aligned} & \hline 0.62 \mathrm{Ac} . \\ & 26.875 \\ & \hline \end{aligned}$ |  |  | 0 | 1.41 Ac . | 1.41 Ac . | $\begin{aligned} & \hline 0.62 \mathrm{Ac} . \\ & 26.875 \\ & \hline \end{aligned}$ | 2.030 Ac. | PARCEL TOTAL FROM DeEd |  |  |
|  |  |  |  |  | 2 |  |  | TSRE | $\begin{gathered} 0.04 \mathrm{Ac} \\ 1.708 \\ \hline \end{gathered}$ |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 |  | Kathy Green | 5048 | 3517 |  |  | $\begin{gathered} 0.04 \mathrm{Ac} . \\ 1.708 \\ \hline \end{gathered}$ |  |  | $\begin{gathered} \hline 0.96 \mathrm{Ac} . \\ 41.818 \end{gathered}$ | 0 | $\begin{gathered} 0.96 \mathrm{Ac} . \\ 41.818 \\ \hline \end{gathered}$ | $\begin{gathered} 0.04 \mathrm{AC.} \\ 1.708 \\ \hline \end{gathered}$ | 1.0 Ac . | PARCEL TOTAL FROM DEED |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 36 |  | Roy Rogers Tanner, Jr | 5062 | 1649 |  |  | 1.75 Ac . |  |  | 4.40 Ac . | 0 | 4.40 Ac . | 1.75 Ac . | 6.15 Ac . | PARCEL Total from deed |  |  |
|  |  | AKA Roy Rogers Tanner, Jr. | 5062 | 7261 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 37 |  | Donna Jean Lucas | 5033 | 4688 |  |  | 17.72 Ac. |  |  | 104.66 Ac. | 17.30 Ac . | 121.96 Ac . | 17.72 Ac . | 139.68 Ac. | parcel total from deed |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 38 |  | Frank A. Lacek and Ruth Lacek | 551 | 557 |  |  | 0.002 Ac. 93 |  |  | 5.438 Ac . | 0 | 5.438 Ac . | 0.002 Ac. 93 | 5.44 Ac . | Parcel total from deed |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 39 |  | Unknown (Private Drive) |  |  |  |  |  |  |  |  |  |  |  |  | total take |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 |  | Unknown (Private Drive) |  |  |  |  | $\begin{gathered} 0.006 \text { Ac. } \\ 281 \\ \hline \end{gathered}$ |  |  |  |  |  |  | $\begin{array}{\|c\|} \hline 0.006 \mathrm{Ac} . \\ 281 \\ \hline \end{array}$ | Parcel total unable to determine |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 41 |  | Daryl R. Williams | 5013 | 6382 |  |  | 0.03 AC. <br> 1.307 |  |  | 0 | $\begin{gathered} \hline 0.102 \mathrm{Ac} . \\ 4.443 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 0.102 \mathrm{Ac} . \\ 4.443 \\ \hline \end{gathered}$ | 0.03 Ac. <br> 1.307 | 0.132 Ac . | PARCEL TOTAL FROM DEED |  |  |

## Appendix E - Hydraulic Analysis



WV Flood Map


WV Flood Map





| PEAK DISCHARGE COMPUTATION FORM 4-1 |  |  |  |
| :---: | :---: | :---: | :---: |
| CALCULATED BY: $\quad$ JCS CHECKED BY: JWC | $\begin{array}{ll} \text { DATE: } & \frac{41112018}{} \\ \text { DATE: } & 411201218 \\ \hline \end{array}$ | PROJECTNAME: BEAVER - SOUTH EISENHOWER DR. |  |
|  |  | Little Beaver Creek DESIGN RETURN P | Sta 306+77 <br> RIOD: 50 YEARS |
| RATIONAL METHOD | $\begin{gathered} \text { TR } 55 \\ 5 \text { acres }-16,000 \text { acres } \end{gathered}$ |  | USGS METHOD <br> 0.1 square miles $-8,371$ square miles |
| TIME OF CONCENTRATION OVERLANDFLOW SHEET FLOW | INFO FROM WORKSHEET 4-1 |  |  |
|  | $\mathrm{CN}=$ | 64.5 |  |
|  | 24 hr $\mathrm{P}=$ | 4.55 | REGION RANGES: |
| $\mathrm{T}_{\text {tsh }}=22.8 \mathrm{Min}$. | S $=$ Runoff Depth $\mathrm{Q}=$ | $5.50$ | North: $0.13 \mathrm{mi}^{2}$ to $1,516 \mathrm{mi}^{2}$ <br> South: $0.10 \mathrm{mi}^{2}$ to $8,371 \mathrm{mi}^{2}$ |
| SHALLOW CONCENTRATED FLOW | INFO FROM WORKSHEET 4-2 |  | East: $0.22 \mathrm{mi}^{2}$ to $1,486 \mathrm{mi}^{2}$ |
| $\mathrm{T}_{\text {tsc }}=1.0 \mathrm{Min}$. | $\mathrm{T}_{\mathrm{c}}=4.11 \mathrm{hr}$. |  | REGION: |
| CHANNEL FLOV 0 | INITIAL ABSTRATION (Table 4-13) |  | FROM MAP 4.9 |
| $\mathrm{T}_{\text {toh }}=1.2 \mathrm{Min}$. | $\begin{aligned} 1_{\mathrm{a}}= & 1.10 \\ \mathrm{Ia}_{\mathrm{a}} / \mathrm{P}= & 0.242 \end{aligned}$ |  | EASTERN $\square$ |
| $\mathrm{T}_{\mathrm{c}}=\mathrm{T}_{\text {tsh }}+\mathrm{T}_{\text {tsc }}+\quad 0$ |  |  | CENTRAL |
| Note: all three flow segements may not be present. | U̇İT PEAK DİSCHARGE qu |  |  |
|  | USE TC AND I I / P WITH CHART 4-8 |  | WESTERN $\square$ |
| Rainfall litensity i= 3.5 inhr | $\mathrm{qu}=115.3$ | $\mathrm{cts}^{2} \mathrm{mi2} / \mathrm{in}$ |  |
| C A CA | POND AND SWA | AMP AREAS | EQUATION: |
| See Atachment | Percent of watershed$=0 \%$ |  | from table 4-15 OR TABLE 4-16 |
| Total 9998.8 | (Table 4.8) Factor $\mathrm{F}_{\mathrm{p}}=$ | - 1 | Eqn: $Q(50)=250 A^{0.007}$ |
|  | PEAK DISCHARGE |  |  |
| $\begin{aligned} & \text { Weighted Coefficient "C" }=\quad \text { \#REF! } \\ & C=\Sigma(C A) / \Sigma A \end{aligned}$ | $\mathrm{q}_{\mathrm{p}}=\mathrm{q}_{u}\left(\mathrm{~A}\right.$ in $\left.\mathrm{mi}^{2}\right) Q \mathrm{~F}_{\mathrm{p}}$ |  |  |
| Q = \#REFI cfs | $q_{p}=2203.3$ |  | Q $=2147.9 \mathrm{cfs}$ |
|  |  |  |  |
| $Q(50)=2203 \mathrm{cfs}$ |  | . |  |



RUNOFF CURVE NUMBER DETERMINATION

| No. | Desc | Type | c | Acres | CxA |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | residential area, Daniels | D/C | 85 | 173.6 | 14756 |
| 2 | residential area, large lots | C | 79 | 70.7 | 5585.3 |
| 3 | residential area, large lots | C | 75 | 19.9 | 1492.5 |
| 4 | residential, pasture | B \& C | 74 | 108.6 | 8036.4 |
| 5 | golf course |  | 80 | 141.7 | 11336 |
| 6 | farm, residential, trailer park | B | 74 | 48.2 | 3566.8 |
| 7 | residential area, Daniels Elem., pasture | C | 86 | 18.1 | 1556.6 |
| 8 | residential area | C | 83 | 205.9 | 17089.7 |
| 9 | residential area | C | 77 | 128.8 | 9917.6 |
| 10 | residential area, farmland | C | 82 | 94.7 | 7765.4 |
| 11 | grass, brush, bare soil, former motorcycle track | C | 87 | 29.3 | 2549.1 |
| 12 | grass, brush, bare soil, Aspen excavation area | B | 82 | 23.9 | 1959.8 |
| 13 | residential | C | 81 | 90.2 | 7306.2 |
| 14 | farm | C | 82 | 50.7 | 4157.4 |
| 15 | residential area | C | 80 | 295.4 | 23632 |
| 16 | residential area, Shady Spring High School | C | 83 | 287.9 | 23895.7 |
| 17 | residential area | B\&C | 80 | 55.3 | 4424 |
| 18 | residential area | C | 80 | 131.4 | 10512 |
| 19 | residential area, White Oak | D | 84 | 95.1 | 7988.4 |
| 20 | residential area | D | 86 | 260.6 | 22411.6 |
| 21 | residential area | C | 79 | 13.4 | 1058.6 |
| 22 | pasture in Glade Springs | D | 86 | 31.5 | 2709 |
| 23 | residential area, Glade Springs | C | 79 | 764.7 | 60411.3 |
| 24 | pasture | B \& C | 79 | 52.4 | 4139.6 |
| 25 | pasture, good condition | D | 80 | 28.7 | 2296 |
| 26 | pasture, good condition | D | 80 | 14.7 | 1176 |
| 27 | brush, weeds, grass | B | 56 | 6.1 | 341.6 |
| 28 | pasture | B | 69 | 26.7 | 1842.3 |
| 29 | residential, large lots |  | 84 | 54.50 | 4578 |
| 30 | residential, pasture | B | 72 | 21.70 | 1562.4 |
| 31 | residential, pasture, Crow | B | 74 | 79.10 | 5853.4 |
| 32 | remaining wooded areas | B | 55 | 5775.30 | 317641.5 |
|  |  |  |  | 9198.80 | 593548.20 |



| TIME OF CONCENTRATION |  |  |  | PRoJECT NAME: BEAVER - SOUTH EISENHOWER DR. |  |  |  |  |  |  |  | PROJECT \# X 341 -WWAN-6.2202 |  |  |  | 1 of 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SHEET FLOW |  |  |  |  | Shallow Concentrated flow |  |  |  |  | PIPE \& DITCH FLOW |  |  |  | REMARKS |
|  | $\begin{gathered} \text { Z } \\ \stackrel{\rightharpoonup}{E} \\ \hline \end{gathered}$ |  |  |  | s. Slope |  |  | 5. Slope | velocity | $\begin{gathered} \text { Lefow } \\ \text { Length } \end{gathered}$ |  | velocity |  |  | Toal 1 ime of Conc |  |
|  | , |  | ${ }_{4}$ | in | futt | min |  | futt | tusec | A | min | fisec | ${ }^{\text {H }}$ | min | min |  |
|  |  | 0.8 | 100 | 2.51 | 0.088 | ${ }_{23} 3$ | 25 | 0.0780 | 0.70 | 300 | 7.2 | 2.77 | 3907.00 | 23.5 | 54.04 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 3.84 | 7867.00 | 34.2 | 88.2 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 44 | 78000 | 29.7 | 117.9 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 26 | 62000 | 39.4 | 157.3 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 445 | 108100 | 6.3 | 163.6 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 3.85 | 7339.00 | ${ }^{31.8}$ | 1954 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 5.28 | 2904.00 | 9.2 | 204.6 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 5.45 | 575.00 | 17.6 | 2222 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 4.35 | 3907.00 | 15.0 | 237.2 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 8.46 | 3960.00 | ${ }^{7.8}$ | 245.0 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 10.09 | 1014.00 | 1.7 | 246.6 | see channels |



| PEAK DISCHARGE COMPUTATION FORM 4-1 |  |  |  |
| :---: | :---: | :---: | :---: |
| CALCULATED BY: CHECKED BY: $\frac{\text { JCS }}{\text { JWC }}$ | $\begin{array}{ll} \hline \text { DATE: } & 4 / 11 / 2018 \\ \cline { 2 - 3 } \\ \cline { 2 - 3 } & 4 / 11 / 2018 \\ \hline \end{array}$ |  |  |
| AREA NUMBER: 1 <br> LOCATION DESCRIPTION: Beaver WV (Little Beaver Creek) <br> DRAINAGE AREA $=$ $\qquad$ 9276.30 AC $14.49 \mathrm{mi}^{2}$ |  |  |  |
| $\begin{aligned} & \text { RATONALOL NETHOD } \\ & 1 \text { acre } 200 \text { acres } \end{aligned}$ | $\begin{gathered} \text { TR - } 55 \\ 5 \text { acres }-16,000 \text { acres } \end{gathered}$ |  | USGS METHOD <br> 0.1 square miles $-8,371$ square miles |
| TIME OF CONCENTRATION OVERLAND FLOW SHEET FLOW | INFO FROM WORKSHEET 4-1 |  | REGION RANGES: <br> North: $0.13 \mathrm{mi}^{2}$ to $1,516 \mathrm{mi}^{2}$ South: East: Ea $0.22 \mathrm{mi}^{2}$ 2 <br> REGION: |
|  | $\mathrm{CN}=$ | 64.5 |  |
|  | $24 \mathrm{hr} \mathrm{P} \mathrm{=}$ | 4.07 |  |
| $\mathrm{T}_{\text {tsh }}=22.8 \mathrm{Min}$. | $\begin{array}{r} S= \\ \text { Runoff Depth } Q= \end{array}$ | $\begin{aligned} & 5.4 \\ & .1 .04 \end{aligned}$ |  |
| SHALLOW CONCENTRATED FLOW$T_{\text {tsc }}=1.0 \mathrm{Min} .$ | INFO FROM WORKSHEET 4-2 |  |  |
|  | $\mathrm{T}_{\mathrm{c}}=4.15 \mathrm{hr}$. |  |  |
| CHANNEL FLOV | INITIAL ABSTRATION (Table 4-13) |  | FROM MAP 4-9 |
| ch $=1.2 \mathrm{Min}$. | $\begin{array}{rlr} \mathrm{I}_{\mathrm{a}} & 1.10 & 10 \\ \mathrm{I}_{\mathrm{a}} / \mathrm{P} & = & 0.270 \end{array}$ |  | EASTERN $\square$ |
| $\begin{aligned} & T_{C}=T_{\text {tsh }}+T_{\text {tsc }}+\quad 0 \\ & \text { Note: all three flow segements may not be present. } \end{aligned}$ |  |  | CENTRAL |
|  | UNIT PEAK DISCHARGE qu |  | $\square$ |
|  | USE TC AND I a/P WITH CHART 4-8$\mathrm{qu}=111.5 \quad \mathrm{cfs} / \mathrm{mi2} / \mathrm{in}$ |  | WESTERN $\square$ |
| Rainfall Intensity $\mathrm{i}=3.5 \mathrm{in} \mathrm{mr}$ |  |  |  |  |  |
| C A CA | POND AND SWAMP AREAS |  | EQUATION: |
| See Atachment | $\begin{array}{r} \text { Percent of watershed } \\ =0 \% \end{array}$ |  | FROM TABLE 4-15 OR TABLE 4-16 |
| Total $\overline{9276.3}$ | (Table 4-8) Factor $\mathrm{F}_{\mathrm{p}}=$ | 1 | Eqn: $\mathrm{Q}(25)=206 \mathrm{~A}^{0.816}$ |
|  | PEAK DISCHARGE |  |  |
| $\begin{gathered} \text { Weighted Coefficient "C" }=\quad \text { *REF! } \\ C=\Sigma(C A) / \Sigma A \end{gathered}$ | $q_{p}=q_{u}\left(\mathrm{~A}\right.$ in mi $\left.{ }^{2}\right) Q F_{p}$ |  |  |
| $Q=$ \#REF! cfs | $\mathrm{q}_{\mathrm{p}}=1680.3$ |  | Q $=1825.15$ cfs |
|  |  |  |  |
| Q(25) $=1680 \mathrm{cfs}$ |  |  |  |



| PEAK DISCHARGE COMPUTATION FORM 4-1 |  |  |  |
| :---: | :---: | :---: | :---: |
| CALCULATED BY: $\quad$ JCS CHECKED BY: | DATE: $\frac{4 / 112018}{\text { DATE: }} \frac{4112018}{}$ <br>   | PROJECT NAME: $\frac{\text { BEAVER - SOUTH EISENHOWER DR. }}{\text { STATE PROJECT NUMBER: }} \quad \mathrm{x} 341$-ZWAY-6.22 02 |  |
|  |  | Little Beaver Creek | t Airport Road Sta 79+76 <br> RIOD: 100 YEARS |
| RATIONAL METHOD 1 acre - 200 acres | $\begin{gathered} \text { TR }-55 \\ 5 \text { acres }-16,000 \text { acres } \end{gathered}$ |  | USGS METHOD 0.1 square miles $-8,371$ square miles |
| TIME OF CONCENTRATION OVERLAND FLOW SHEET FLOW | INFO FROM WORKSHEET 4-1 |  | REGION RANGES: <br> North: $0.13 \mathrm{mi}^{2}$ to $1,516 \mathrm{mi}^{2}$ <br> South: $0.10 \mathrm{mi}^{2}$ to $8,371 \mathrm{mi}^{2}$ <br> East: $0.22 \mathrm{mi}^{2}$ to $1,486 \mathrm{mi}^{2}$ <br> REGION: |
|  | $\mathrm{CN}=$$24 \mathrm{hr}=$$\mathrm{S}=$Runoff Depth $\mathrm{Q}=$ | 64.5 |  |
|  |  | 5.06 |  |
| $\mathrm{T}_{\text {tsh }}=22.8 \mathrm{Min}$. |  | $\begin{aligned} & 5.49 \\ & 1.66 \end{aligned}$ |  |
| SHALLOW CONCENTRATED FLOW | INFO FROM WORKSHEET 4-2 |  |  |
| CHANNEL FLOV | $\mathrm{T}_{\mathrm{c}}=4.15 \mathrm{hr}$. |  |  |
|  | INITIAL ABSTRATION (Table 4-13) |  | FROM MAP 4-9 |
| $\mathrm{T}_{\text {tch }}=1.2 \mathrm{Min}$. | $\begin{array}{r} 1_{a}= \\ \mathrm{I}_{\mathrm{a}} / \mathrm{P} \end{array}$ | $\begin{gathered} 1.10 \\ 0.217 \end{gathered}$ | EASTERN $\square$ |
| $\begin{aligned} & T_{\mathrm{C}}=T_{\text {tsh }}+\mathrm{T}_{\text {ssc }}+\quad 0 \\ & \text { Note: all three fow segements may not be present. } \end{aligned}$ |  |  | CENTRAL |
|  | UNIT PEAK DISCHARGE qu |  |  |
|  | USE TC AND I a / P WITH CHART 4-8 |  | WESTERN $\square$ |
| Rainfall Intensity $\mathrm{i}=$ | qu $=116.9 \mathrm{cfs} / \mathrm{mi2} / \mathrm{in}$ |  |  |
| CSee Attachment | POND AND SWAMP AREAS |  | EQUATION: |
|  | Percent of watershed$=0 \%$ |  | FROM TABLE 4-15 OR TABLE 4-16 |
| Total 9276.3 | (Table 4-8) Factor $\mathrm{F}_{\mathrm{p}}=$ | 1 | Eqn: $Q(100)=297 \mathrm{~A}^{0.800}$ |
|  | PEAK DISC | HARGE |  |
| $\begin{gathered} \text { Weighted Coefficient "C" }=\quad \text { *REF! } \\ C=\Sigma(C A) / \Sigma A \end{gathered}$ | $\mathrm{q}_{\mathrm{p}}=\mathrm{q}_{\mathrm{u}}\left(\mathrm{A}\right.$ in mi $\left.{ }^{2}\right) Q F_{\mathrm{p}}$ |  |  |
| $Q=$ \#REF! cfs | $q_{p}=$ | 2811.9 | $Q \quad=2521.2 \mathrm{cfs}$ |
|  |  |  |  |
| $\mathbf{Q}(100)=2812 \mathrm{cfs}$ |  |  |  |

RUNOFF CURVE NUMBER DETERMINATION



| time of concentration |  |  |  | Project name: beaver - SOUTH EISENHOWER DR. |  |  |  |  |  |  |  | PROJECT \# X 341 -ZWAN-6. 2202 |  |  |  | 1 of 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INLETID |  | HEET FLOW |  |  |  |  | SHALLOW CONCENTRATED FLOW |  |  |  |  | PIPE \& DITCH FLOW |  |  |  | REMARKS |
|  | $\begin{gathered} \frac{2}{2} \\ \vdots \\ \hline \end{gathered}$ |  |  |  | s, Slope |  | $\underset{\substack{\text { surface } \\ \text { coefecerent }}}{ }$ | S. Slope | velociny | ${ }_{\text {L }}^{\text {L L fongh }}$ |  | Vebocit | ${ }_{\text {L }}^{\text {L finow }}$ Lengh |  | Toal Time of Cone |  |
|  | , | , | ${ }_{4}$ | in | tuft | min |  | futt | tfsec | H | min | ttsec | 4 | min | min |  |
|  |  | 0.8 | 100 | 2.51 | ${ }^{0.088}$ | ${ }^{23} 3$ | 2.5 | 0.0780 | 0.70 | 300 | 7.2 | 2.77 | 3907.00 | 23.5 | 54.04 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | ${ }_{3} 34$ | 7887.00 | 34.2 | ${ }_{88}{ }^{2}$ | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 44 | 78000 | 29.7 | 117.9 | see chamels |
|  |  |  |  |  |  |  |  |  |  |  |  | ${ }^{26}$ | 62000 | 394 | 157.3 | see chamels |
|  |  |  |  |  |  |  |  |  |  |  |  | 445 | 18100 | ${ }^{6} 3$ | 163.6 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 3.85 | 733900 | 31.8 | 195.4 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 5.28 | 2904.00 | 9.2 | 204.6 | see chamnels |
|  |  |  |  |  |  |  |  |  |  |  |  | 5.45 | 575.00 | 17.5 | 222.2 | see chamels |
|  |  |  |  |  |  |  |  |  |  |  |  | 4.35 | 3907.00 | 15.0 | 237.2 | see chamnels |
|  |  |  |  |  |  |  |  |  |  |  |  | 8.46 | 3860.00 | ${ }^{7.8}$ | 245.0 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 10.9 | 1014.00 | 1.7 | 246.6 | see crannels |
|  |  |  |  |  |  |  |  |  |  |  |  | 6.72 | 200.00 | 0.5 | 247.1 | see cramels |
|  |  |  |  |  |  |  |  |  |  |  |  | 10.27 | 90000 | 1.5 | 248.6 | see channels |
|  |  |  |  |  |  |  |  |  |  |  |  | 10.45 | 30000 | 0.5 | 24.1 | see channels |

Unit Peak Discharge Equation (Table 4-14) pg 4-63
$\mathbf{2 5 Y R}$

| $\mathbf{I} / \mathbf{P}$ | $\mathbf{C}_{\mathbf{0}}$ | $\mathbf{C}_{\mathbf{1}}$ | $\mathbf{C}_{\mathbf{2}}$ |
| :---: | :---: | :---: | :---: |
| 0.1 | 2.553 | -0.615 | -0.164 |
| 0.30 | 2.465 | -0.623 | -0.17 |
| 0.35 | 2.419 | -0.616 | 3.9 |
| 0.40 | 2.364 | -0.599 | 1.11 |
| 0.45 | 2.292 | -0.570 | 0.48 |
| 0.50 | 2.202 | -0.516 | 0.11 |
| $\mathbf{I a} / \mathbf{P}$ | $\mathbf{C}_{\mathbf{0}}$ | $\mathbf{C}_{\mathbf{1}}$ | $\mathbf{C}_{\mathbf{2}}$ |
| 0.1 | 2.553 | -0.615 | -0.164 |
| 0.30 | 2.465 | -0.623 | -0.17 |
| 0.35 | 2.419 | -0.616 | -0.088 |
| 0.40 | 2.364 | -0.599 | -0.056 |
| 0.45 | 2.292 | -0.570 | -0.023 |
| 0.50 | 2.202 | -0.516 | -0.013 |


$T_{c}=4.15$
$1 \mathrm{a} / \mathrm{P}=0.217$
$l \begin{array}{lc}a=0.1 & 128.88 \\ a=0 . & 108.44\end{array}$
$\mathrm{a}=0.3$
$\mathrm{la}=0.2172 \mathrm{qu} \quad 116.90$
$T_{c}=4.15$
$\mathrm{a} / \mathrm{P}=0.242$
$\begin{array}{ll}\mathrm{a}=0.1 & 128.88\end{array}$
$\mathrm{la}=0.2415 \quad \mathrm{qu}$


