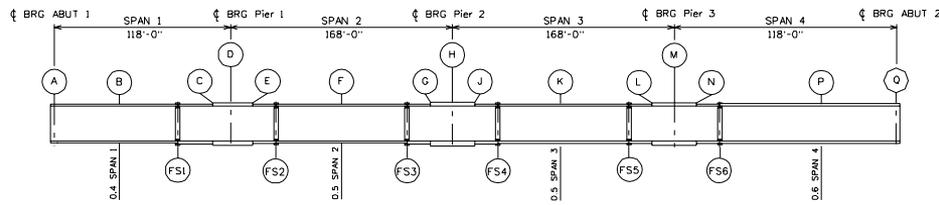


INTERIOR GIRDERS										NON-COMPOSITE (GIRDER ONLY)		COMPOSITE FOR NEGATIVE MOMENT (GIRDER AND REINFORCEMENT STEEL)		3/4 COMPOSITE FOR POSITIVE MOMENT (GIRDER AND CONCRETE WITH 3/4 MODULAR RATIO)		1/4 COMPOSITE FOR POSITIVE MOMENT (GIRDER AND CONCRETE WITH 1/4 MODULAR RATIO)		DESIGN SERVICE MOMENT AND SHEAR				LLDF						
SPAN	SECTION LOCATIONS	TOP FLG WIDTH (IN)	TOP FLG (IN)	DEPTH (IN)	WEB THICKNESS (IN)	WEB STRENGTH (KSI)	S-TOP F/LG (IN)	S-BOTTOM (IN)	S-TOP (IN)	S-BOTTOM (IN)	S-TOP F/LG (IN)	S-BOTTOM (IN)	DL1 MOMENT (K-FT)	DL1 SHEAR (K)	DL2 MOMENT (K-FT)	DL2 SHEAR (K)	MOMENT	SHEAR										
1	A	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	0	18	0.794	1.045		
1	B	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	1310	68	350	0.794	1.045	
1	PS1	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	7	68	16	17	0.794	1.045
1	C	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	D	20	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	139	139	363	36	0.794	1.045
1	E	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	F	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	G	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	H	20	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	139	139	363	36	0.794	1.045
1	I	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	J	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	K	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	L	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	M	20	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	139	139	363	36	0.794	1.045
1	N	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	O	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	P	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045
1	Q	14	1	1	1	1	1	1	1	1	60	0	5623	50	1187	1250	1808	1414	3884	1628	12179	794	102	102	226	26	0.794	1.045

DESIGN MOMENTS AND SHEARS (LL-1 HAVE A LLDF = 1.0)									
SPAN	SECTION LOCATIONS	H20 TRUCK		HS20 TRUCK/LANE		3S2 TRUCK		TYPE 3 TRUCK	
		LL-1 MOMENT (K-FT)	LL-1 SHEAR (K)						
1	A	0	27	0	39	0	67	0	56
1	B	1110	45	1798	39	1568	28	1292	27
1	PS1	838	26	1371	62	1160	51	959	43
1	C	667	43	1564	84	1142	67	825	52
1	D	788	48	2623	102	1348	78	974	58
1	E	470	43	1338	66	1142	67	974	58
1	F	684	39	702	71	890	60	771	46
1	G	1198	24	2038	39	1735	31	1407	26
1	FS3	817	37	1279	68	1123	56	936	43
1	H	613	42	1543	84	1058	61	764	50
1	I	736	46	3095	102	1272	76	914	57
1	J	817	37	1038	68	1123	56	936	43
1	FS4	684	39	1643	84	1058	61	764	50
1	K	1198	24	2038	39	1735	31	1407	26
1	FS5	684	39	1052	71	890	60	771	46
1	L	470	43	1338	66	1142	67	974	58
1	M	788	48	2623	102	1348	78	974	58
1	N	667	43	1564	84	1142	67	825	52
1	PS6	838	26	1371	62	1160	51	959	43
1	FS6	838	26	1371	62	1160	51	959	43
1	P	1110	45	1798	39	1568	28	1292	27
1	Q	0	27	0	39	0	67	0	56

LOAD RATING FACTOR				
RATING	H20	HS20	3S2	TYPE 3
INVENTORY (IRF)	2.59	1.36	1.81	2.17
OPERATING (ORF)	4.32	2.26	3.01	3.61

LOAD RATING (TONS)				
RATING	H20	HS20	3S2	TYPE 3
INVENTORY (IR)	51.9	48.8	65.0	54.2
OPERATING (OR)	86.4	81.4	108.4	90.3



- Notes:
- If significant section loss has occurred, recalculate the girder section properties to reflect those losses.
 - DL1 moment and shear is due to weight of steel girders, crossframes and details, structural deck concrete, haunches and stay-in-place forms. These force effects are resisted by the composite girder.
 - DL2 moment and shear is due to weight of special concrete overlay, parapets and future wearing surface. These force effects are resisted by the composite girder.
 - LL-1 moments and shears provided are critical (maximum) forces at the specific location indicated.

Flexure rating of an interior beam at 0.5L of Span 2 with an HS20 Rating Vehicle.

- Applied moment and section properties:

M_u	-	7,922 K-FT (AASHTO Standard Specification eq. 10-129c)
LLDF	-	0.725 (AASHTO LRFD live load distribution factor)
F_y	=	50 KSI
M_{DL1}	=	1,731 K-FT
M_{DL2}	-	473 K-FT
M_{LL+I}	-	2,038 K-FT (live load moment based on one lane)
S_b stl	-	1,332 IN^3
S_b 3n	=	1,729 IN^3
S_b n	=	1,904 IN^3

- Convert live load moment:

$$M_{LL+I} = \text{LLDF} (M_{LL+I}^*)$$

$$M_{LL+I} = 0.725 (2,038) = 1,478 \text{ K-FT}$$

- Calculate inventory rating factor based on strength:

$$\text{IRF} = \frac{M_u - 1.3(M_{DL1}) - 1.3(M_{DL2})}{2.17(M_{LL+I})}$$

$$\text{IRF} = \frac{7,922 - 1.3(1,731) - 1.3(473)}{2.17(1,478)} = 1.58$$

- Calculate inventory rating factor based on serviceability:

$$\text{IRF} = \frac{0.95F_y - (f_b)_{DL1} - (f_b)_{DL2}}{1.67(f_b)_{LL+I}}$$

$$(f_b)_{DL1} = \frac{M}{S_b} = \frac{1,731(12)}{1,332} = 15.6 \text{ KSI}$$

$$(f_b)_{DL2} = \frac{473(12)}{1,729} = 3.3 \text{ KSI}$$

$$(f_b)_{LL+I} = \frac{1,478(12)}{1,904} = 9.3 \text{ KSI}$$

$$\text{TRF} = \frac{0.95(50) - (15.6) - (3.3)}{1.67(9.3)} = 1.84 \text{ (does not control)}$$

- Calculate operating rating factor:

$$\text{ORF} = \frac{5}{3} (\text{IRF})$$

$$\text{ORF} = \frac{5}{3} (1.58) = 2.63$$

- Calculate rating: (HS20 truck weighs 36 Tons)

$$\text{IR} = 1.58 (36) = 56.9 \text{ Tons}$$

$$\text{OR} = 2.98 (36) = 107.3 \text{ Tons}$$

Flexure rating of an interior beam at Pier 2 with an HS20 Rating Vehicle.

- Applied moment and section properties:

F_y	=	70 KSI
M_{DL1}	-	4,796 K-FT
M_{DL2}	-	1,196 K-FT
M_{LL+I}^*	-	3,095 K-FT (live load moment based on one lane)
S_b stl	-	2,549 IN^3
S_b neg	-	2,686 IN^3
F_{cr}	-	70 KSI (AASHTO Standard Specification section 10.48.2)
R_b	=	1.0 (AASHTO Standard Specification eq. 10-103b)
LLDF	-	0.762 (AASHTO LRFD live load distribution factor)

- Convert live load moment:

$$M_{LL+I} = \text{LLDF} (M_{LL+I}^*)$$

$$M_{LL+I} = 0.762 (3,095) = 2,358 \text{ K-FT}$$

- Calculate nominal bending stress

$$F_{bn} = R_b (F_{cr})$$

$$F_{bn} = 1.0 (70 \text{ KSI}) = 70 \text{ KSI}$$

- Calculate bending stress in bottom flange:

$$(f_b) = \frac{M}{S_b}$$

$$(f_b)_{DL1} = \frac{4,796(12)}{2,549} = 22.6 \text{ KSI}$$

$$(f_b)_{DL2} = \frac{1,196(12)}{2,686} = 5.3 \text{ KSI}$$

$$(f_b)_{LL+I} = \frac{2,358(12)}{2,686} = 10.5 \text{ KSI}$$

- Calculate inventory rating factor based on strength:

$$\text{IRF} = \frac{F_{bn} - 1.3(f_b)_{DL1} - 1.3(f_b)_{DL2}}{2.17(f_b)_{LL+I}}$$

$$\text{IRF} = \frac{70 - 1.3(22.6) - 1.3(5.3)}{2.17(10.5)} = 1.48$$

- Calculate inventory rating factor based on serviceability:

$$\text{TRF} = \frac{0.95F_y - (f_b)_{DL1} - (f_b)_{DL2}}{1.67(f_b)_{LL+I}}$$

$$IRF = \frac{0.95(70) - (22.6) - (5.3)}{1.67(10.5)} = 2.20 \text{ (does not control)}$$

- Calculate operating rating factor:

$$ORF = \frac{5}{3} (IRF)$$

$$ORF = \frac{5}{3} (1.48) = 2.47$$

- Calculate rating: (HS20 truck weighs 36 Tons)

$$IR = 1.48 (36) = 53.3 \text{ Tons}$$

$$OR = 2.47 (36) = 88.9 \text{ Tons}$$

$$IRF = \frac{562 - 1.3(152) - 1.3(38)}{2.17(107)} = 1.36$$

- Calculate operating rating factor:

$$ORF = \frac{5}{3} (IRF)$$

$$ORF = \frac{5}{3} (1.36) = 2.27$$

- Calculate rating: (HS20 truck weighs 36 Tons)

$$IR = 1.36 (36) = 48.8 \text{ Tons}$$

$$OR = 2.27 (36) = 81.4 \text{ Tons}$$

Shear Rating for an interior beam at Pier 2 with an HS20 Rating Vehicle.

- Applied shear and design data for section:

$$V_{DL1} = 152 \text{ K}$$

$$V_{DL2} = 38 \text{ K}$$

$$V_{LL-H}^R = 102 \text{ K (live load shear based on one lane)}$$

$$V_n = 562 \text{ K}$$

$$LLDF = 1.045 \text{ (AASHTO LRFD live load distribution factor)}$$

- Convert live load shear:

$$V_{LL-H} = LLDF (V_{LL-H}^R)$$

$$V_{LL-H} = 1.045 (102 \text{ K}) = 107 \text{ K}$$

- Calculate inventory rating factor

$$IRF = \frac{V_n - 1.3(V)_{DL1} - 1.3(V)_{DL2}}{2.17(V)_{LL-H}}$$

The following rating calculation reflects a section loss of 1/8 IN in the bottom flange and 1/16 IN in the web at Pier 2 (Section 1.1) for Rating Example No. 1.

Flexure rating of an interior beam at Pier 2 with an HS20 Rating Vehicle.

- Applied moment and section properties:

$$\begin{aligned}
 F_y &= 70 \text{ KSI} \\
 M_{DL1} &= 4,796 \text{ K-FT} \\
 M_{DL2} &= 1,196 \text{ K-FT} \\
 M_{LL1}^* &= 3,095 \text{ K-FT (live load moment based on one lane)} \\
 S_b \text{ stl} &= 2,386 \text{ IN}^3 \text{ (Reduced Section)} \\
 S_b \text{ neg} &= 2,499 \text{ IN}^3 \text{ (Reduced Section)} \\
 F_c &= 70 \text{ KSI (AASHTO Standard Specification section 10.48.2)} \\
 R_b &= 1.0 \text{ (AASHTO Standard Specification eq. 10-103b)} \\
 LLDF &= 0.762 \text{ (AASHTO LRFD live load distribution factor)}
 \end{aligned}$$

- Convert live load moment:

$$M_{LL1} = LLDF (M_{LL1}^*)$$

$$M_{LL1} = 0.762 (3,095) = 2,358 \text{ K-FT}$$

- Calculate nominal bending stress

$$F_b = R_b (F_c)$$

$$F_b = 1.0 (70 \text{ KSI}) = 70 \text{ KSI}$$

- Calculate bending stress in bottom flange:

$$(f_b) = \frac{M}{S_b}$$

$$(f_b)_{DL1} = \frac{4,796(12)}{2,386} = 241 \text{ KSI}$$

$$(f_b)_{DL2} = \frac{1,196(12)}{2,499} = 5.7 \text{ KSI}$$

$$(f_b)_{LL1} = \frac{2,358(12)}{2,499} = 11.3 \text{ KSI}$$

- Calculate inventory rating factor based on strength:

$$IRF = \frac{F_b - 1.3(f_b)_{DL1} - 1.3(f_b)_{DL2}}{2.17(f_b)_{LL1}}$$

$$IRF = \frac{70 - 1.3(241) - 1.3(5.7)}{2.17(11.3)} = 1.27$$

- Calculate inventory rating factor based on serviceability:

$$IRI = \frac{0.95F_y - (f_b)_{DL1} - (f_b)_{DL2}}{1.67(f_b)_{LL1}}$$

$$IRF = \frac{0.95(70) - (241) - (5.7)}{1.67(11.3)} = 1.94 \text{ (does not control)}$$

- Calculate operating rating factor:

$$ORF = \frac{5}{3} (IRF)$$

$$ORF = \frac{5}{3} (1.27) = 2.12$$

- Calculate rating: (HS20 truck weighs 36 Tons)

$$IR = 1.27 (36) = 45.7 \text{ Tons}$$

$$OR = 2.12 (36) = 76.3 \text{ Tons}$$

Shear Rating for an interior beam at Pier 2 with an HS20 Rating Vehicle.

- Applied shear and design data for section:

$$\begin{aligned}
 V_{DL1} &= 152 \text{ K} \\
 V_{DL2} &= 38 \text{ K} \\
 V_{LL1}^* &= 102 \text{ K (live load shear based on one lane)} \\
 V_b &= 475 \text{ K (Reduced Capacity)} \\
 LLDF &= 1.045 \text{ (AASHTO LRFD live load distribution factor)}
 \end{aligned}$$

- Convert live load shear:

$$V_{LL1} = LLDF (V_{LL1}^*)$$

$$V_{LL1} = 1.045 (102 \text{ K}) = 107 \text{ K}$$

- Calculate inventory rating factor

$$IRF = \frac{V_b - 1.3(V)_{DL1} - 1.3(V)_{DL2}}{2.17(V)_{LL1}}$$

$$IRF = \frac{475 - 1.3(152) - 1.3(38)}{2.17(107)} = 0.98$$

- Calculate operating rating factor:

$$ORF = \frac{5}{3} (IRF)$$

$$ORF = \frac{5}{3} (0.98) = 1.63$$

- Calculate rating: (HS20 truck weighs 36 Tons)

$$IR = 0.98 (36) = 35.3 \text{ Tons}$$

$$OR = 1.63 (36) = 58.7 \text{ Tons}$$

Bending rating of an interior beam at 0.6L of Span 5 with an HS25 Rating Vehicle.

- Applied moment, section properties and design data:

$$\begin{aligned}
 M_{DL1} &= 4,261 \text{ K-FT} \\
 M_{DL2} &= 1,161 \text{ K-FT} \\
 M_{LL-H} &= 3,984 \text{ K-FT (live load moment based on one lane)} \\
 CF &= 1.38 \text{ (conversion factor based on grid analysis)} \\
 S_{bstl} &= 3,522 \text{ IN}^3 \\
 S_{bsn} &= 4,052 \text{ IN}^3 \\
 S_{bn} &= 4,414 \text{ IN}^3 \\
 F_{tn} &= 70 \text{ KSI (actual member capacity)} \\
 F_y &= 70 \text{ KSI} \\
 d &= 13.156 \text{ FT} \\
 R &= 272.75 \text{ FT} \\
 H &= 6.38 \text{ FT} \\
 S_y dg &= 168 \text{ IN}^3 \text{ (} 24 \text{ IN} \times 1 \frac{3}{4} \text{ IN)}
 \end{aligned}$$

- Convert live load moment:

$$\begin{aligned}
 M_{LL-H} &= CF(M_{LL-H}) \\
 M_{LL-H} &= 1.38(3,984) = 5,498 \text{ K-FT}
 \end{aligned}$$

- Calculate lateral bending moments:

$$\begin{aligned}
 M_w &= \frac{M(d^3)}{12(R)(H)} \\
 (M_w)_{DL1} &= \frac{4,261(13.156)^3}{12(272.75)(6.38)} = 35.3 \text{ K-FT} \\
 (M_w)_{DL2} &= \frac{1,161(13.156)^3}{12(272.75)(6.38)} = 9.6 \text{ K-FT} \\
 (M_w)_{LL-H} &= \frac{5,498(13.156)^3}{12(272.75)(6.38)} = 45.6 \text{ K-FT}
 \end{aligned}$$

- Calculate primary bending stress in bottom flange:

$$\begin{aligned}
 (f_b)_{DL1} &= \frac{M}{S_b} \\
 (f_b)_{DL1} &= \frac{4,261(12)}{3,522} = 14.5 \text{ KSI} \\
 (f_b)_{DL2} &= \frac{1,161(12)}{4,052} = 3.4 \text{ KSI} \\
 (f_b)_{LL-H} &= \frac{5,498(12)}{4,414} = 14.9 \text{ KSI}
 \end{aligned}$$

- Calculate lateral bending stress in bottom flange:

$$\begin{aligned}
 (f_w) &= \frac{M_w}{S_{ydg}} \\
 (f_w)_{DL1} &= \frac{35.3(12)}{168} = 2.5 \text{ KSI} \\
 (f_w)_{DL2} &= \frac{9.6(12)}{168} = 0.7 \text{ KSI} \\
 (f_w)_{LL} &= \frac{45.6(12)}{168} = 3.3 \text{ KSI}
 \end{aligned}$$

- Calculate inventory rating factor based on strength:

The controlling rating factor will be given by the lesser of IRF_1 or IRF_2 .

$$\begin{aligned}
 IRF_1 &= \frac{F_{tn} - 1.3(f_b)_{DL1} - 1.3(f_b)_{DL2}}{2.17(f_b)_{LL-H}} \\
 IRF_2 &= \frac{F_y - 1.3(f_b + f_w)_{DL1} - 1.3(f_b + f_w)_{DL2}}{2.17(f_b + f_w)_{LL-H}}
 \end{aligned}$$

$$IRF_1 = \frac{70 - 1.3(14.5) - 1.3(3.4)}{2.17(14.9)} = 1.45 \text{ (does not co)}$$

$$IRF_2 = \frac{70 - 1.3(14.5 + 2.5) - 1.3(3.4 + 0.7)}{2.17(14.9 + 3.3)} = 1.08$$

$$TRF = 1.08$$

- Calculate operating rating factor:

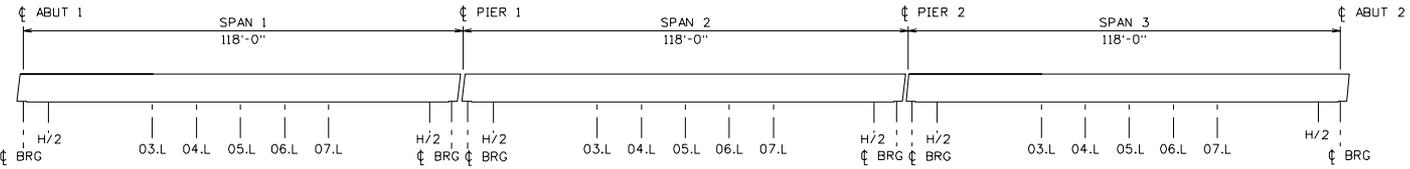
$$ORF = \frac{5}{3}(IRF)$$

$$ORF = \frac{5}{3}(1.08) = 1.80$$

- Calculate rating: (HS25 truck weights 45 Tons)

$$IR = 1.08(45) = 48.6 \text{ Tons}$$

$$OR = 1.80(36) = 81 \text{ Tons}$$



INTERIOR BEAMS B2 & B3

BEAM SECTION PROPERTIES									
SPAN	LOCATION	SECTION MODULUS TO THE TOP AND BOTTOM FLANGES				SECTION MODULUS TO THE TOP AND BOTTOM PRESTRESSING STRANDS			
		NONCOMPOSITE		COMPOSITE		NONCOMPOSITE		COMPOSITE	
		Stp (IN ²)	Stp (IN ²)	Stp (IN ²)	Stp (IN ²)	Stp (IN ²)	Stp (IN ²)	Stp (IN ²)	Stp (IN ²)
1	BEARING	14,300	15,586	49,567	21,644	16,731	16,640	66,023	22,629
	H/2	14,300	15,586	49,567	21,644	18,884	16,640	84,951	22,629
	0.3L	14,300	15,586	49,567	21,644	56,407	16,640	43,089	22,629
	0.4L	14,300	15,586	49,567	21,644	22,809	16,640	27,666	22,629
	0.5L	14,300	15,586	49,567	21,644	22,809	16,640	27,666	22,629
	0.6L	14,300	15,586	49,567	21,644	22,809	16,640	27,666	22,629
	0.7L	14,300	15,586	49,567	21,644	56,407	16,640	43,089	22,629
2	BEARING	14,300	15,586	49,567	21,644	16,731	16,640	66,023	22,629
	H/2	14,300	15,586	49,567	21,644	16,731	16,640	66,023	22,629
	0.3L	14,300	15,586	49,567	21,644	16,731	16,640	66,023	22,629
	0.4L	14,300	15,586	49,567	21,644	87,328	16,640	49,724	22,629
	0.5L	14,300	15,586	49,567	21,644	22,998	16,640	31,300	22,629
	0.6L	14,300	15,586	49,567	21,644	22,998	16,640	31,300	22,629
	0.7L	14,300	15,586	49,567	21,644	87,328	16,640	49,724	22,629
3	BEARING	14,300	15,586	49,567	21,644	16,731	16,640	66,023	22,629
	H/2	14,300	15,586	49,567	21,644	16,731	16,640	66,023	22,629
	0.3L	14,300	15,586	49,567	21,644	16,731	16,640	66,023	22,629
	0.4L	14,300	15,586	49,567	21,644	22,809	16,640	27,666	22,629
	0.5L	14,300	15,586	49,567	21,644	22,809	16,640	27,666	22,629
	0.6L	14,300	15,586	49,567	21,644	22,809	16,640	27,666	22,629
	0.7L	14,300	15,586	49,567	21,644	56,407	16,640	43,089	22,629

SECTION CAPACITY										
SPAN	LOCATION	f _c (psi)	CONCRETE TENSION (PSI)	CONCRETE COMPRESSION CASE 1 (PSI)	CONCRETE COMPRESSION CASE 2 (PSI)	FLEXURAL STRENGTH (K-F T)	H20 SHEAR STRENGTH (KIPS)	HS20 SHEAR STRENGTH (KIPS)	3S2 SHEAR STRENGTH (KIPS)	TYPE 3 SHEAR STRENGTH (KIPS)
H/2	7,000	-502	4,200	2,800	3,217	468	467	456	462	
0.3L	7,000	-502	4,200	2,800	10,662	211	232	213	218	
0.4L	7,000	-502	4,200	2,800	11,055	192	192	208	192	
0.5L	7,000	-502	4,200	2,800	11,055	192	192	208	192	
0.6L	7,000	-502	4,200	2,800	11,055	192	192	208	192	
0.7L	7,000	-502	4,200	2,800	10,662	211	232	213	218	
2	BEARING	7,000	-502	4,200	2,800	4,842	468	447	456	462
	H/2	7,000	-502	4,200	2,800	4,842	425	437	415	421
	0.3L	7,000	-502	4,200	2,800	4,842	424	436	412	418
	0.4L	7,000	-502	4,200	2,800	9,986	210	213	237	200
	0.5L	7,000	-502	4,200	2,800	10,589	194	191	191	191
	0.6L	7,000	-502	4,200	2,800	10,589	194	191	191	191
	0.7L	7,000	-502	4,200	2,800	9,986	210	213	237	200
3	BEARING	7,000	-502	4,200	2,800	4,842	424	436	412	418
	H/2	7,000	-502	4,200	2,800	4,842	425	437	415	421
	0.3L	7,000	-502	4,200	2,800	4,842	424	436	412	418
	0.4L	7,000	-502	4,200	2,800	11,424	192	192	209	192
	0.5L	7,000	-502	4,200	2,800	11,427	192	192	192	192
	0.6L	7,000	-502	4,200	2,800	11,424	192	192	209	192
	0.7L	7,000	-502	4,200	2,800	11,031	214	234	214	220

DESIGN MOMENTS AND AXIAL LOADS (LL+I MOMENTS HAVE A LLDF = 1.0)													
SPAN	LOCATION	DEAD LOAD		PRESTRESS		H20 TRUCK		HS20 TRUCK/LANE		3S2 TRUCK		TYPE 3 TRUCK	
		DL1 (K-F T)	DL2 (K-F T)	AXIAL (KIP)	MOMENT (K-F T)	M (-) (K-F T)	M (+) (K-F T)	M (-) (K-F T)	M (+) (K-F T)	M (-) (K-F T)	M (+) (K-F T)	M (-) (K-F T)	M (+) (K-F T)
1	BEARING	0	6	305	413	18	-	29	-3	22	21	21	21
	H/2	322	51	1,908	1,760	155	-13	258	-23	228	-22	184	184
	0.3L	4,812	36	1,908	2,178	161	-15	1,636	-238	1,185	-185	1,185	
	0.4L	4,013	361	1,908	1,607	100	180	1,79	-317	1,574	-360	1,981	1,981
	0.5L	3,140	340	1,908	2,607	1,077	-225	1,741	-396	1,532	-375	1,251	1,251
	0.6L	3,013	273	1,908	2,607	864	-269	1,553	-475	1,366	-450	1,114	1,114
	0.7L	2,832	161	1,908	2,378	770	-314	1,313	-555	1,055	-526	876	876
2	BEARING	0	-365	1,908	1,760	149	-509	248	-1,444	187	-855	149	149
	H/2	322	-365	1,908	1,760	149	-509	248	-1,444	187	-855	149	149
	0.3L	4,812	305	1,908	413	144	564	243	1,682	229	-949	170	170
	0.4L	4,013	305	1,908	413	145	-579	256	-1,722	244	-975	179	179
	0.5L	3,140	352	1,908	327	148	-572	240	-1,639	213	-963	173	173
	0.6L	3,013	305	1,908	327	148	-572	240	-1,639	213	-963	173	173
	0.7L	2,832	305	1,908	327	148	-572	240	-1,639	213	-963	173	173
3	BEARING	0	-473	305	414	145	-579	256	-1,722	244	-975	179	179
	H/2	322	-473	305	414	145	-579	256	-1,722	244	-975	179	179
	0.3L	4,812	305	1,174	1,185	166	-553	237	-1,639	156	-931	169	169
	0.4L	4,013	24	1,174	1,411	758	-361	1,183	-735	1,015	-608	856	856
	0.5L	3,140	91	1,174	2,439	892	-289	1,416	-735	1,229	-487	1,022	1,022
	0.6L	3,013	113	1,174	2,439	892	-289	1,416	-735	1,229	-487	1,022	1,022
	0.7L	2,832	24	1,174	2,411	758	-361	1,183	-735	1,015	-608	856	856

DESIGN SHEAR (LL+I SHEARS HAVE A LLDF = 1.0)							
SPAN	LOCATION	DL1 (KIPS)	DL2 (KIPS)	H20 TRUCK (KIPS)	HS20 TRUCK (KIPS)	3S2 TRUCK (KIPS)	TYPE 3 TRUCK (KIPS)
H/2	102	14	45	75	67	53	
0.3L	43	4	30	48	40	37	
0.4L	22	4	24	38	31	28	
0.5L	0	4	25	40	34	31	
0.6L	0	8	30	38	30	27	
0.7L	43	11	35	59	53	43	
2	BEARING	102	22	46	84	75	57
	H/2	102	22	46	84	75	57
	0.3L	108	25	47	87	77	58
	0.4L	106	19	47	83	74	57
	0.5L	102	18	45	80	71	56
	0.6L	43	8	30	51	45	38
	0.7L	44	4	25	44	35	31
3	BEARING	106	19	47	83	74	57
	H/2	102	18	45	80	71	56
	0.3L	43	8	30	51	45	38
	0.4L	22	4	25	44	35	31
	0.5L	0	4	25	44	35	31
	0.6L	22	4	25	44	35	31
	0.7L	43	8	30	51	45	38

LRFD LIVE LOAD DISTRIBUTION FACTORS

SPAN	LOCATION	MOMENT LLDF		SHEAR LLDF	
		ONE LANE	TWO LANES	ONE LANE	TWO LANES
1	BEARING	0.812	0.716	0.812	0.700
	H/2	0.812	0.716	0.812	0.700
	0.3L	0.812	0.716	0.812	0.700
	0.4L	0.812	0.716	0.812	0.700
	0.5L	0.812	0.716	0.812	0.700
	0.6L	0.812	0.716	0.812	0.700
	0.7L	0.812	0.716	0.812	0.700
2	BEARING	0.812	0.716	0.812	0.700
	H/2	0.812	0.716	0.812	0.700
	0.3L	0.812	0.716	0.812	0.700
	0.4L	0.812	0.716	0.812	0.700
	0.5L	0.812	0.716	0.812	0.700
	0.6L	0.812	0.716	0.812	0.700
	0.7L	0.812	0.716	0.812	0.700
3	BEARING	0.812	0.716	0.812	0.700
	H/2	0.812	0.716	0.812	0.700
	0.3L	0.812	0.716	0.812	0.700
	0.4L	0.812	0.716	0.812	0.700
	0.5L	0.812	0.716	0.812	0.700
	0.6L	0.812	0.716	0.812	0.700
	0.7L	0.812	0.716	0.812	0.700

SPAN	LOCATION	H20 TRUCK						HS20 TRUCK/LANE											
		STRESSES			FLEXURE			SHEAR			STRESSES			FLEXURE			SHEAR		
		IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF	DRF	IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF	DRF				
1	BEARING	145.98	1224.30	815.83	59.20	98.82	-	-	87.79	736.26	490.50	35.60	59.43	-	-				
	H/2	41.70	133.31	89.61	10.00	16.69	4.00	6.67	25.05	80.08	53.83	6.01	10.03	2.23	3.73				
	0.3L	3.15	12.83	9.80	3.78	6.31	2.85	4.76	1.94	6.13	3.94	2.34	3.91	2.02	3.18				
	0.4L	2.88	12.83	8.88	3.44	5.74	2.63	4.40	1.85	6.98	5.49	2.13	3.55	2.42	4.05				
	0.5L	2.54	11.65	8.83	3.44	5.75	4.32	7.21	1.57	6.83	5.46	2.13	3.55	2.64	4.40				
	0.6L	3.15	12.83	10.19	3.99	6.87	3.94	4.91	3.96	8.07	6.33	2.48	4.14	1.75	2.91				
	H/2	4.47	13.30	13.78	5.18	8.65	5.29	3.83	2.83	10.98	8.43	3.29	5.49	1.55	2.59				
2	BEARING	5.36	6.80	6.45	5.33	6.90	3.80	6.34	1.89	2.40	2.28	1.88	3.14	1.94	3.24				
	H/2	3.46	13.04	9.28	4.31	7.19	-	-	1.17	4.42	3.15	1.46	2.44	-	-				
	PIER 1	-	-	-	4.14	6.91	-	-	-	-	-	1.39	2.32	-	-				
	BEARING	4.55	12.91	9.17	4.25	7.10	-	-	1.59	4.50	3.20	1.48	2.48	-	-				
	H/2	9.74	8.91	7.77	8.39	3.41	5.69	3.41	5.69	2.72	10.92	8.47	3.17	5.29	2.01				
	0.3L	4.26	17.08	13.75	4.96	8.28	2.69	4.49	2.72	10.92	8.47	3.17	5.29	1.64	3.19				
	0.4L	3.48	14.29	11.14	4.22	7.05	3.68	6.14	2.19	9.00	7.02	2.66	4.44	2.04	3.40				
3	BEARING	3.06	13.04	10.33	3.99	6.54	4.50	7.51	1.93	8.73	6.52	2.47	4.13	2.89	4.83				
	H/2	3.48	14.29	11.14	4.22	7.05	3.68	6.14	2.19	9.00	7.02	2.66	4.44	2.04	3.40				
	0.3L	4.26	17.08	13.75	4.96	8.28	2.69	4.49	2.72	10.92	8.47	3.17	5.29	1.64	2.74				
	H/2	8.99	8.17	6.89	4.30	8.17	3.41	5.69	3.45	3.14	4.65	1.88	3.14	2.01	3.35				
	PIER 2	4.55	12.91	9.17	4.25	7.10	-	-	1.59	4.50	3.20	1.48	2.47	-	-				
	BEARING	3.48	13.03	9.27	4.31	6.91	-	-	-	1.18	4.42	3.14	1.39	2.32	-				
	H/2	5.69	7.07	6.59	5.34	8.32	3.79	6.33	2.01	2.50	2.32	1.88	3.15	1.94	3.23				
3	BEARING	4.57	17.07	13.16	5.40	9.02	2.30	3.83	2.90	10.83	8.35	3.43	5.72	1.56	2.60				
	H/2	3.22	12.76	10.00	4.16	6.95	2.92	4.87	2.00	7.92	6.28	2.68	4.31	1.74	2.90				
	0.3L	2.60	10.84	8.73	3.59	6.00	4.31	7.20	1.61	6.70	3.40	2.32	3.71	2.63	4.39				
	0.4L	2.72	11.09	8.78	3.59	5.99	3.81	6.35	1.68	6.86	3.43	2.22	3.70	2.41	4.02				
	0.5L	2.79	12.65	8.82	3.65	5.99	3.81	6.35	1.68	6.86	3.43	2.22	3.70	2.41	4.02				
	0.6L	2.72	11.09	8.78	3.59	5.99	3.81	6.35	1.68	6.86	3.43	2.22	3.70	2.41	4.02				
	H/2	40.87	132.39	89.18	10.05	16.77	3.99	6.66	24.55	79.52	53.57	6.03	10.07	2.23	3.72				
BEARING	148.14	1238.18	824.92	59.91	100.01	-	-	88.68	741.19	493.81	35.87	59.87	-	-					

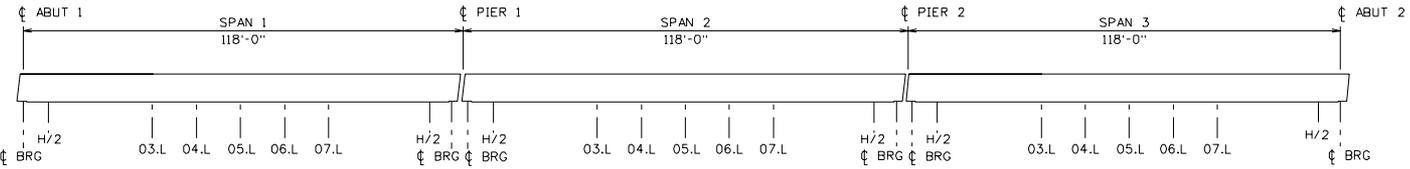
CONTROLLING RATING FACTOR

	H20	HS20	3S2	TYPE 3
IRF	2.10	1.45	1.40	1.78
DRF	3.51	2.42	2.33	2.97

CONTROLLING RATING TONS

	H20	HS20	3S2	TYPE 3
IR	42.0	52.1	50.2	44.5
DR	70.1	87.0	83.8	74.3

SPAN	LOCATION	3S2 TRUCK						TYPE 3 TRUCK											
		STRESSES			FLEXURE			SHEAR			STRESSES			FLEXURE			SHEAR		
		IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF	DRF	IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF	DRF				
1	BEARING	98.40	833.87	455.39	40.31	67.29	-	-	123.41	1035.04	659.54	50.05	83.54	-	-				
	H/2	28.42	90.84	61.07	6.81	11.87	2.60	4.33	16.75	122.68	75.74	8.45	14.11	3.31	5.52				
	0.3L	2.20	8.96	6.91	2.64	4.41	2.13	3.55	2.72	11.06	8.54	3.26	5.44	3.32	4.32				
	0.4L	1.84	12.72	9.87	3.74	6.17	2.15	3.59	3.76	7.63	6.23	2.63	4.83	2.99	5.32				
	0.5L	1.79	7.77	6.21	2.42	4.04	3.11	5.19	2.19	9.51	6.00	2.96	4.95	3.44	5.74				
	0.6L	2.22	9.17	7.19	2.82	4.70	2.18	3.65	2.73	11.24	8.82	3.46	5.77	2.34	3.91				
	H/2	3.22	12.62	9.69	3.78	6.17	1.51	2.51	3.03	15.20	11.66	4.55	7.60	1.83	2.92				
2	BEARING	3.19	4.05	3.84	3.18	5.30	2.24	3.73	4.34	6.50	5.22	4.32	7.20	3.03	5.06				
	H/2	2.06	7.75	5.51	2.56	4.27	-	-	2.80	10.55	7.51	3.49	5.82	-	-				
	PIER 1	-	-	-	2.46	4.10	-	-	-	-	-	3.35	5.59	-	-				
	BEARING	2.70	7.68	5.45	2.52	4.21	-	-	-	3.68	10.44	7.42	3.44	5.74	-				
	H/2	5.78	5.29	4.32	3.17	5.30	2.07	3.45	3.78	7.88	7.21	5.88	4.32	7.21	4.56				
	0.3L	3.17	12.72	9.87	3.74	6.17	2.15	3.59	3.76	11.06	8.54	3.26	4.38	2.99	5.32				
	0.4L	2.52	10.37	8.08	3.06	5.11	2.54	4.23	3.03	12.47	9.72	3.88	6.15	2.87	4.79				
3	BEARING	2.23	9.51	7.54	2.88	4.77	3.65	6.10	2.67	11.36	9.00	3.41	5.70	3.99	6.66				
	H/2	3.22	12.62	9.69	3.78	6.17	1.51	2.51	3.03	15.20	11.66	4.55	7.60	1.83	2.92				
	0.3L	2.52	10.37	8.08	3.06	5.11	2.54	4.23	3.03	12.47	9.72	3.88	6.15	2.87	4.79				
	0.4L	2.17	12.72	9.87	3.70	6.17	2.15	3.59	3.76	15.09	11.71	4.38	7.32	1.99	3.37				
	0.5L	2.54	4.85	6.89	2.91	4.85	2.07	3.45	2.72	6.61	6.89	3.96	6.61	2.93	4.56				
	H/2	2.70	7.66	5.17	2.52	4.21	-	-	3.68	10.44	9.17	3.44	5.74	-	-				
	PIER 2	-	-	-	2.46	4.10	-	-	-	-	-	3.35	5.59	-	-				
3	BEARING	2.06	7.74	5.27	2.56	4.27	-	-	2.81	10.54	9.27	3.49	5.82	-	-				
	H/2	3.39	4.21	6.59	3.18	5.31	2.23	3.73	4.61	5.72	6.59	4.32	7.22	3.02	5.05				
	0.3L	3.33	12.46	9.60	3.94	6.58	1.51	2.52	4.02	11.50	11.56	4.75	7.93	1.93	3.22				
	0.4L	2.27	9.00	7.11	2.94	4.90	2.19	3.65	2.78	11.04	8.72	3.60	6.01	2.32	3.88				
	0.5L	1.83	7.89	6.23	2.43	4.22	3.10	5.18	2.24	12.47	9.72	3.88	6.15	2.87	4.79				
	0.6L	1.90	7.75	6.14	2.51	4.19	3.25	5.43	3.33	9.52	7.54	3.08	5.14	3.34	5.57				
	H/2	2.26	8.84	6.85	2.76	4.60	2.13	3.56	2.79	10.91	8.46	3.40	5.68	2.59	4.33				
BEARING	21.84	90.24	62.84	6.84	11.42	2.59	4.33	34.54	110.88	84.54	75.87	84.49	14.88	3.30	5.52				



EXTERIOR BEAMS B1 & B4

BEAM SECTION PROPERTIES									
SPAN	LOCATION	SECTION MODULUS TO THE TOP AND BOTTOM FLANGES				SECTION MODULUS TO THE TOP AND BOTTOM PRESTRESSING STRANDS			
		NON-COMPOSITE		COMPOSITE		NON-COMPOSITE		COMPOSITE	
		Stp (IN ⁴)	Sgt (IN ⁴)	Stp (IN ⁴)	Sgt (IN ⁴)	Stp (IN ⁴)	Sgt (IN ⁴)	Stp (IN ⁴)	Sgt (IN ⁴)
1	BEARING	14,300	15,586	53,263	21,884	16,731	16,640	71,991	22,861
	H/2	14,300	15,586	53,263	21,884	18,884	16,640	94,226	22,861
	0.3L	14,300	15,586	53,263	21,884	56,407	16,640	42,786	22,861
	0.4L	14,300	15,586	53,263	21,884	22,809	16,640	27,833	22,861
	0.5L	14,300	15,586	53,263	21,884	22,809	16,640	27,833	22,861
	0.6L	14,300	15,586	53,263	21,884	27,998	16,640	27,833	22,861
	0.7L	14,300	15,586	53,263	21,884	56,407	16,640	42,786	22,861
2	H/2	14,300	15,586	53,263	21,884	18,884	16,640	94,226	22,861
	BEARING	14,300	15,586	53,263	21,884	16,731	16,640	71,991	22,861
	PIER 1	14,300	15,586	53,263	21,884	16,731	16,640	71,991	22,861
	H/2	14,300	15,586	53,263	21,884	18,728	16,640	92,298	22,861
	0.3L	14,300	15,586	53,263	21,884	87,328	16,640	49,131	22,861
	0.4L	14,300	15,586	53,263	21,884	27,998	16,640	31,230	22,861
	0.5L	14,300	15,586	53,263	21,884	22,809	16,640	27,833	22,861
3	0.6L	14,300	15,586	53,263	21,884	27,998	16,640	31,230	22,861
	0.7L	14,300	15,586	53,263	21,884	87,328	16,640	49,131	22,861
	H/2	14,300	15,586	53,263	21,884	18,728	16,640	92,298	22,861
	BEARING	14,300	15,586	53,263	21,884	16,731	16,640	71,991	22,861
	PIER 2	14,300	15,586	53,263	21,884	16,731	16,640	71,991	22,861
	H/2	14,300	15,586	53,263	21,884	18,728	16,640	92,298	22,861
	0.3L	14,300	15,586	53,263	21,884	56,407	16,640	42,786	22,861

SECTION CAPACITY										
SPAN	LOCATION	f'c (psi)	CONCRETE TENSION (PSI)	CONCRETE CASE 1 (PSI)	CONCRETE CASE 2 (PSI)	FLEXURAL STRENGTH (K-F-T)	H2O SHEAR STRENGTH (KIPS)	HS20 SHEAR STRENGTH (KIPS)	3S2 SHEAR STRENGTH (KIPS)	TYPE 3 SHEAR STRENGTH (KIPS)
H/2	7,000	-502	4,200	2,800	3,242	482	458	469	476	
0.3L	7,000	-502	4,200	2,800	10,738	214	233	214	219	
0.4L	7,000	-502	4,200	2,800	11,132	192	192	206	192	
0.5L	7,000	-502	4,200	2,800	11,134	192	192	192	192	
0.6L	7,000	-502	4,200	2,800	11,132	192	192	206	192	
0.7L	7,000	-502	4,200	2,800	10,738	214	233	214	219	
2	BEARING	7,000	-502	4,200	2,800	-5,286	482	458	469	476
	PIER 1	7,000	-502	4,200	2,800	-5,286	356	356	356	356
	BEARING	7,000	-502	4,200	2,800	-5,286	436	448	426	431
	H/2	7,000	-502	4,200	2,800	-5,286	447	422	422	429
	0.3L	7,000	-502	4,200	2,800	10,056	212	244	237	203
	0.4L	7,000	-502	4,200	2,800	10,650	193	191	191	191
	0.5L	7,000	-502	4,200	2,800	10,668	191	191	191	191
3	0.6L	7,000	-502	4,200	2,800	10,660	193	191	191	191
	0.7L	7,000	-502	4,200	2,800	10,056	212	214	237	203
	H/2	7,000	-502	4,200	2,800	-5,286	447	422	422	429
	BEARING	7,000	-502	4,200	2,800	-5,286	436	448	426	431
	PIER 2	7,000	-502	4,200	2,800	-5,286	356	356	356	356
	BEARING	7,000	-502	4,200	2,800	-5,286	482	485	471	478
	0.3L	7,000	-502	4,200	2,800	11,113	216	235	215	220

DESIGN MOMENTS AND AXIAL LOADS (LL+I MOMENTS HAVE A LLDf = 1.0)																
SPAN	LOCATION	DEAD LOAD		PRESTRESS	H2O TRUCK	HS20 TRUCK/LANE				3S2 TRUCK				TYPE 3 TRUCK		
		DL1 (K-F-T)	DL2 (K-F-T)			M (+) (K-F-T)	M (-) (K-F-T)	M (+) (K-F-T)	M (-) (K-F-T)	M (+) (K-F-T)	M (-) (K-F-T)	M (+) (K-F-T)	M (-) (K-F-T)	M (+) (K-F-T)	M (-) (K-F-T)	
1	BEARING	0	6	303	413	18	-1	29	-3	26	-2	21	-2			
	H/2	343	6	303	165	-13	-268	-23	228	-225	184	-16	184			
	0.3L	2,806	371	303	1,718	1,021	-135	1,650	-239	1,463	-275	1,185	-166			
	0.4L	3,212	396	303	2,607	1,100	-180	1,779	-317	1,574	-300	1,281	-222			
	0.5L	3,147	372	303	2,499	1,077	-228	1,741	-386	1,533	-375	1,251	-277			
	0.6L	3,212	299	303	2,607	964	-269	1,553	-475	1,366	-450	1,114	-333			
	0.7L	2,806	177	303	2,378	770	-514	1,213	-555	1,055	-525	876	-388			
2	H/2	343	-400	303	1,760	144	-664	144	-664	144	-664	144	-664			
	BEARING	0	-473	0	303	413	144	-664	243	-1,662	229	-949	170	-697		
	PIER 1	0	-473	0	303	413	144	-664	243	-1,662	229	-949	170	-697		
	BEARING	0	-471	352	327	145	-579	256	-1,722	244	-975	179	-716			
	H/2	339	-409	1,174	1,185	166	-553	237	-1,439	156	-931	169	-684			
	0.3L	2,743	26	1,174	2,141	756	-361	1,183	-735	1,015	-608	856	-446			
	0.4L	3,147	99	1,174	2,499	892	-289	1,416	-735	1,229	-487	1,022	-357			
3	0.5L	3,281	124	1,174	2,499	934	-289	1,480	-735	1,280	-366	1,072	-288			
	0.6L	3,147	99	1,174	2,499	892	-289	1,416	-735	1,229	-487	1,022	-357			
	H/2	2,743	26	1,174	2,141	756	-361	1,183	-735	1,015	-608	856	-444			
	H/2	339	-410	1,174	1,185	166	-553	237	-1,439	156	-931	169	-684			
	BEARING	0	-471	352	327	148	-572	240	-1,640	213	-963	173	-707			
	PIER 2	0	-473	0	303	414	144	-664	243	-1,662	228	-949	170	-697		
	BEARING	0	-475	305	414	144	-664	243	-1,662	228	-949	170	-697			

DESIGN SHEAR (LL+I SHEARS HAVE A LLDf = 1.0)									
SPAN	LOCATION	DL1 (KIPS)	DL2 (KIPS)	H2O TRUCK (KIPS)	H2O T/L (KIPS)	HS20 TRUCK (KIPS)	3S2 TRUCK (KIPS)	TYPE 3 TRUCK (KIPS)	TYPE 3 TRUCK (KIPS)
H/2	108	4	30	45	26	67	34		
0.3L	46	4	40	48	40	34			
0.4L	23	0	24	38	31	28			
0.5L	6	4	25	34	34	31			
0.6L	23	8	30	50	44	37			
0.7L	46	13	35	59	53	43			
2	H/2	108	24	46	78	70	55		
	BEARING	115	25	47	87	77	58		
	PIER 1	113	21	47	83	74	57		
	BEARING	107	20	45	80	71	55		
	0.3L	46	8	30	51	45	38		
	0.4L	23	4	24	36	31	28		
	0.5L	6	0	24	36	30	27		
3	0.6L	23	4	25	44	36	31		
	H/2	108	24	46	78	70	55		
	0.7L	46	8	35	51	45	38		
	H/2	107	20	45	80	71	55		
	BEARING	113	21	47	83	74	57		
	PIER 2	117	25	47	87	77	58		
	BEARING	111	16	45	76	67	53		

LRFD LIVE LOAD DISTRIBUTION FACTORS							
SPAN	LOCATION	MOMENT LLDF			SHEAR LLDF		
		ONE LANE	TWO LANES	ONE LANE	TWO LANES		
1	BEARING	0.484	0.704	0.701	0.849		
	H/2	0.484	0.704	0.701	0.849		
	0.3L	0.484	0.704	0.701	0.849		
	0.4L	0.484	0.704	0.701	0.849		
	0.5L	0.484	0.704	0.701	0.849		
	0.6L	0.484	0.704	0.701	0.849		
	0.7L	0.484	0.704	0.701	0.849		
	H/2	0.484	0.704	0.701	0.849		
	PIER 1	0.484	0.704	0.701	0.849		
	BEARING	0.484	0.704	0.701	0.849		
2	BEARING	0.484	0.704	0.701	0.849		
	H/2	0.484	0.704	0.701	0.849		
	0.3L	0.484	0.704	0.701	0.849		
	0.4L	0.484	0.704	0.701	0.849		
	0.5L	0.484	0.704	0.701	0.849		
	0.6L	0.484	0.704	0.701	0.849		
	0.7L	0.484	0.704	0.701	0.849		
	H/2	0.484	0.704	0.701	0.849		
	PIER 2	0.484	0.704	0.701	0.849		
	BEARING	0.484	0.704	0.701	0.849		
3	BEARING	0.484	0.704	0.701	0.849		
	H/2	0.484	0.704	0.701	0.849		
	0.3L	0.484	0.704	0.701	0.849		
	0.4L	0.484	0.704	0.701	0.849		
	0.5L	0.484	0.704	0.701	0.849		
	0.6L	0.484	0.704	0.701	0.849		
	0.7L	0.484	0.704	0.701	0.849		
	H/2	0.484	0.704	0.701	0.849		
	BEARING	0.484	0.704	0.701	0.849		

H20 TRUCK													HS20 TRUCK/LANE																	
SPAN	LOCATION	STRESSES						FLEXURE			SHEAR			STRESSES						FLEXURE			SHEAR							
		IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF	IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF								
1	BEARING	170.20	1517.42	1010.90	68.37	114.12	4.72	19.07	3.86	6.45	29.03	98.81	66.50	6.86	11.46	2.14	3.58	102.35	912.54	607.93	41.12	68.63	-	-	-	-	-	-		
	H/2	48.32	184.50	110.70	11.42	19.07	3.86	6.45	29.03	98.81	66.50	6.86	11.46	2.14	3.58	102.35	912.54	607.93	41.12	68.63	-	-	-	-	-	-	-	-		
	0.3L	2.29	10.35	11.82	4.72	7.07	3.73	4.51	4.85	2.04	8.65	7.41	3.61	4.48	1.80	3.17	4.48	2.92	4.38	3.61	4.48	1.80	3.17	4.48	1.80	3.17	4.48	1.80	3.17	
	0.4L	2.71	13.03	10.53	3.83	6.40	3.62	6.04	1.67	6.05	6.51	2.37	3.96	4.29	2.29	3.62	4.29	2.29	3.62	4.29	2.29	3.62	4.29	2.29	3.62	4.29	2.29	3.62	4.29	
	0.5L	2.54	12.87	10.43	2.83	6.39	4.76	6.88	1.57	7.83	6.45	2.37	3.96	4.29	2.29	3.62	4.29	2.29	3.62	4.29	2.29	3.62	4.29	2.29	3.62	4.29	2.29	3.62	4.29	
	0.6L	4.84	15.00	12.08	2.46	7.44	2.76	4.60	2.01	9.31	7.77	4.52	6.24	2.74	4.62	1.84	2.74	4.62	1.84	2.74	4.62	1.84	2.74	4.62	1.84	2.74	4.62	1.84	2.74	
	0.7L	4.73	20.34	15.85	5.83	9.74	2.16	3.61	3.00	12.84	10.06	3.70	6.18	1.45	2.42	3.10	1.86	3.10	1.86	3.10	1.86	3.10	1.86	3.10	1.86	3.10	1.86	3.10	1.86	
	H/2	6.84	9.53	7.72	6.70	11.05	3.66	6.12	2.41	2.50	2.65	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	
	PIER 1	2.27	15.11	10.77	5.42	9.05	-	-	-	1.45	5.12	3.65	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94	1.84	2.94
	BEARING	5.61	14.36	10.65	5.35	8.93	-	-	-	1.96	5.22	3.71	1.77	2.96	-	-	-	1.77	2.96	-	-	-	-	-	-	-	-	-	-	
2	BEARING	11.83	9.52	8.04	6.15	10.27	3.27	5.46	4.95	3.22	3.72	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	
	H/2	5.61	14.36	10.65	5.35	8.93	-	-	-	1.96	5.22	3.71	1.77	2.96	-	-	-	1.77	2.96	-	-	-	-	-	-	-	-	-	-	
	0.3L	11.83	9.52	8.04	6.15	10.27	3.27	5.46	4.95	3.22	3.72	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	1.87	3.22	
	0.4L	4.51	19.98	15.83	5.99	9.33	-	-	-	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88
	0.5L	3.61	16.55	13.22	4.37	7.89	-	-	-	2.77	7.18	1.97	8.47	2.71	4.61	1.92	3.57	4.61	1.92	3.57	4.61	1.92	3.57	4.61	1.92	3.57	4.61	1.92	3.57	
	0.6L	3.61	16.55	13.22	4.37	7.89	-	-	-	2.77	7.18	1.97	8.47	2.71	4.61	1.92	3.57	4.61	1.92	3.57	4.61	1.92	3.57	4.61	1.92	3.57	4.61	1.92	3.57	
	0.7L	4.51	19.98	15.83	5.99	9.33	-	-	-	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88	4.22	2.88
	H/2	11.32	9.52	8.04	6.15	10.26	3.23	5.46	4.22	2.88	12.77	10.12	3.57	5.96	1.54	2.25	3.21	3.57	5.96	1.54	2.25	3.21	3.57	5.96	1.54	2.25	3.21	3.57		
	PIER 2	5.61	14.36	10.65	5.35	8.93	-	-	-	1.96	5.22	3.71	1.77	2.96	-	-	-	1.77	2.96	-	-	-	-	-	-	-	-	-	-	
	BEARING	4.28	15.10	10.77	2.28	8.81	-	-	-	1.45	5.12	3.65	1.84	2.94	-	-	-	1.84	2.94	-	-	-	-	-	-	-	-	-	-	
3	BEARING	7.26	8.25	7.68	6.71	11.20	3.66	6.11	2.56	2.91	2.71	2.37	3.95	1.85	3.10	-	-	2.37	3.95	1.85	3.10	-	-	-	-	-	-	-		
	H/2	7.26	8.25	7.68	6.71	11.20	3.66	6.11	2.56	2.91	2.71	2.37	3.95	1.85	3.10	-	-	2.37	3.95	1.85	3.10	-	-	-	-	-	-	-		
	0.3L	4.85	19.96	15.71	6.09	10.17	2.16	3.61	3.08	12.66	9.97	4.87	6.45	1.45	2.43	3.14	4.87	6.45	1.45	2.43	3.14	4.87	6.45	1.45	2.43	3.14	4.87	6.45		
	0.4L	4.32	17.72	11.84	4.86	7.78	2.74	4.97	2.05	9.14	7.41	2.89	8.53	1.63	2.73	3.14	2.89	8.53	1.63	2.73	3.14	2.89	8.53	1.63	2.73	3.14	2.89			
	0.5L	2.61	12.40	10.30	4.01	6.69	4.11	6.86	1.61	7.67	6.37	2.48	4.13	2.51	4.19	-	-	2.48	4.13	2.51	4.19	-	-	-	-	-	-			
	0.6L	2.77	12.78	10.40	4.01	6.69	3.60	6.01	1.71	7.30	6.43	2.48	4.14	2.78	3.80	-	-	2.48	4.14	2.78	3.80	-	-	-	-	-	-			
	0.7L	4.32	17.72	11.84	4.86	7.78	4.43	7.10	2.10	8.14	7.25	2.74	4.58	1.91	3.21	-	-	2.74	4.58	1.91	3.21	-	-	-	-	-	-			
	H/2	4.735	16.335	10.17	11.48	19.16	3.86	6.45	28.44	98.11	66.17	6.89	11.51	2.14	3.57	-	-	6.89	11.51	2.14	3.57	-	-	-	-	-	-	-		
	BEARING	172.72	1534.61	1022.41	69.19	115.49	-	-	-	103.39	918.64	612.03	41.42	69.14	-	-	-	41.42	69.14	-	-	-	-	-	-	-	-	-	-	

CONTROLLING RATING FACTOR				
	H20	HS20	3S2	TYPE 3
IRF	2.22	1.17	1.51	1.93
DRF	3.71	2.32	2.51	3.21

CONTROLLING RATING TONS				
	H20	HS20	3S2	TYPE 3
IR	44.5	42.3	54.2	48.1
DR	74.2	83.7	90.4	80.4

3S2 TRUCK													TYPE 3 TRUCK															
SPAN	LOCATION	STRESSES						FLEXURE			SHEAR			STRESSES						FLEXURE			SHEAR					
		IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF	IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF	IRF TENSION	IRF COMP CASE 1	IRF COMP CASE 2	IRF	DRF						
1	BEARING	115.90	1033.26	688.36	46.55	77.71	4.94	1.99	3.32	143.89	1282.84	854.63	57.80	96.48	-	-	-	143.89	1282.84	854.63	57.80	96.48	-	-	-	-	-	-
	H/2	32.93	112.10	75.44	7.79	13.00	2.50	4.17	40.84	139.04	93.57	9.66	16.12	3.19	5.33	-	-	40.84	139.04	93.57	9.66	16.12	3.19	5.33	-	-	-	-
	0.3L	2.70	12.44	9.44	3.66	4.44	3.49	3.32	2.84	12.32	10.19	3.69	5.10	4.41	2.03	-	-	2.84	12.32	10.19	3.69	5.10	4.41	2.03	-	-	-	-
	0.4L	1.89	9.10	5.45	2																							

Rating of an interior beam at 0.5L of Span 1 with an HS20 Rating Vehicle.

- Applied moment, section properties and design data:

$$\begin{aligned}
 M_{DL1} &= 3,348 \text{ K-ft} \\
 M_{DL2} &= 372 \text{ K-ft} \\
 M_{FT+T}^R &= 1,741 \text{ K-ft (live load moment based on one lane)} \\
 P &= 1,208 \text{ K (effective prestress after losses)} \\
 S_{\text{flange N.C.}} &= 14,300 \text{ IN}^3 \\
 S_{\text{ho flange N.C.}} &= 15,586 \text{ IN}^3 \\
 S_{\text{flange Comp.}} &= 53,263 \text{ IN}^3 \\
 S_{\text{ho flange Comp.}} &= 21,884 \text{ IN}^3 \\
 A_{\text{beam}} &= 908 \text{ IN}^2 \\
 Ecc. &= 25.89 \text{ IN} \\
 f_c' &= 7,000 \text{ PSI} \\
 LLDF &= 0.704 \text{ (AASHTO LRFD live load distribution factor)} \\
 \phi M_h &= 11,134 \text{ K-ft}
 \end{aligned}$$

- Convert live load moment:

$$\begin{aligned}
 M_{FT+T} &= T.L.D.R.(M_{FT+T}^R) \\
 M_{FT+T} &= 0.704(1,741) = 1,226 \text{ K-ft}
 \end{aligned}$$

Concrete Stresses

- Concrete tension (bottom of precast beam)

$$\begin{aligned}
 F_t &= \frac{M_{DL1}}{S_{\text{flange N.C.}}} + \frac{M_{DL2}}{S_{\text{ho flange N.C.}}} \\
 F_t &= \frac{3,348(12)}{15,586} (1) + \frac{372(12)}{21,884} (1) = 2.78 \text{ KSI}
 \end{aligned}$$

$$\Gamma_p = P \left[\frac{1}{A_{\text{beam}}} + \frac{Ecc.}{S_{\text{ho flange N.C.}}} \right]$$

$$F_p = 1,208 \left[\frac{1}{908} + \frac{25.89}{15,586} \right] = 3.34 \text{ KSI}$$

$$\begin{aligned}
 F_{T+T} &= \frac{M_{DL1}}{S_{\text{ho flange Comp}}} \\
 F_{T+T} &= \frac{1,226(12)}{21,884} (-1) = -0.67 \text{ KSI} \\
 TRF &= -6\sqrt{f_c'} - (F_t + F_p + F_s) \\
 &= -6\sqrt{7,000} \left(\frac{1}{1,000} \right) - (-2.78 + 3.34 + 0) \\
 TRF &= -0.67 \quad 1.57
 \end{aligned}$$

- Concrete compression (top of precast beam)

$$\begin{aligned}
 F_c &= \frac{M_{DL1}}{S_{\text{flange N.C.}}} + \frac{M_{DL2}}{S_{\text{ho flange Comp.}}} \\
 F_c &= \frac{3,348(12)}{14,300} + \frac{372(12)}{53,263} = 2.89 \text{ KSI}
 \end{aligned}$$

$$F_p = P \left[\frac{1}{A_{\text{beam}}} - \frac{Ecc.}{S_{\text{ho flange N.C.}}} \right]$$

$$\Gamma_p = 1,208 \left[\frac{1}{908} - \frac{25.89}{14,300} \right] = -0.86 \text{ KSI}$$

$$\begin{aligned}
 F_{T+T} &= \frac{M_{DL1}}{S_{\text{flange Comp}}} \\
 F_{T+T} &= \frac{1,226(12)}{53,263} = 0.28 \text{ KSI}
 \end{aligned}$$

Case 1

$$\begin{aligned}
 TRF &= 0.6f_c' - (F_t + F_p + F_s) \\
 TRF &= \frac{4.2 - (2.89 + -0.86 + 0)}{0.28} = 7.83
 \end{aligned}$$

Case 2

$$\begin{aligned}
 TRF &= \frac{0.4f_c' - 0.5(F_t + F_p + F_s)}{I_i} \\
 TRF &= \frac{2.8 - 0.5(2.89 + -0.86 + 0)}{0.28} = 6.45
 \end{aligned}$$

Positive Flexure

$$\begin{aligned}
 TRF &= \frac{\phi M_h - [1.3(M_{DL1} + 1.3(M_{DL2} + M_s))]}{2.17(M_{DL1})} \\
 TRF &= \frac{11,134 - [1.3(3,348) + 1.3(372) + 0]}{2.17(1,226)} = 2.37 \\
 ORF &= \frac{\phi M_h - [1.3(M_{DL1} + 1.3(M_{DL2} + M_s))]}{1.3(M_{DL1})} \\
 ORF &= \frac{11,134 - [1.3(3,348) + 1.3(372) + 0]}{1.3(1,226)} = 3.95
 \end{aligned}$$

Rating of an interior beam at Right Bearing (Pier 1) of Span with an HS20 Rating Vehicle.

- Applied moment, section properties and design data:

$$\begin{aligned}
 M_{DL1} &= 0 \text{ K-ft} \\
 M_{DL2} &= -475 \text{ K-ft} \\
 M_{FT+T}^R &= -1,662 \text{ K-ft (live load moment based on or lane)} \\
 P &= 303 \text{ K (effective prestress after losses)} \\
 S_{\text{flange N.C.}} &= 14,300 \text{ IN}^3 \\
 S_{\text{ho flange N.C.}} &= 15,586 \text{ IN}^3 \\
 S_{\text{flange Comp.}} &= 53,263 \text{ IN}^3 \\
 S_{\text{ho flange Comp.}} &= 21,884 \text{ IN}^3 \\
 A_{\text{beam}} &= 908 \text{ IN}^2 \\
 Ecc. &= 16.38 \text{ IN} \\
 f_c' &= 7,000 \text{ PSI} \\
 LLDF &= 0.704 \text{ (AASHTO LRFD live load distribution factor)} \\
 \phi M_h &= -5,286 \text{ K-ft}
 \end{aligned}$$

- Convert live load moment:

$$M_{LL+T} = I.L.D.F(M^*_{TL+T})$$

$$M_{LL+T} = 0.704(-1,662) = -1,170 \text{ K-FT}$$

Concrete Stresses

- Concrete tension (top of precast beam)

$$F_t = \frac{M_{DL1}}{S_{\text{flange}t.c.}} + \frac{M_{DL2}}{S_{\text{flange}c.c.}}$$

$$F_t = \frac{0(12)}{14,300} + \frac{-475(12)}{53,263} = -0.11 \text{ KSI}$$

$$F_p - P \left[\frac{1}{A_{\text{beam}}} - \frac{E_{cc}}{S_{\text{flange}t.c.}} \right]$$

$$F_p - 303 \left[\frac{1}{908} - \frac{16.38}{14,300} \right] = -0.01 \text{ KSI}$$

$$F_{LL+T} = \frac{M_{LL+T}}{S_{\text{flange}c.c.}}$$

$$F_{LL+T} = \frac{-1,170(12)}{53,263} = -0.26 \text{ KSI}$$

$$I.R.F. = \frac{-6\sqrt{F_c} (F_t + F_p + F_s)}{F_t}$$

$$I.R.F. = \frac{-6\sqrt{7,000} \left(\frac{1}{1,000} \right) (-0.11 + 0.01 + 0)}{-0.26} = 1.45$$

- Concrete compression (bottom of precast beam)

$$F_c = \frac{M_{DL1}}{S_{\text{flange}t.c.}} + \frac{M_{DL2}}{S_{\text{flange}c.c.}}$$

$$F_c = \frac{0(12)}{15,586}(-1) + \frac{-475(12)}{21,884}(-1) = 0.26 \text{ KSI}$$

$$F_p - P \left[\frac{1}{A_{\text{beam}}} + \frac{E_{cc}}{S_{\text{flange}t.c.}} \right]$$

$$F_p - 303 \left[\frac{1}{908} + \frac{16.38}{15,586} \right] = 0.65 \text{ KSI}$$

$$F_{LL+T} = \frac{M_{LL+T}}{S_{\text{flange}c.c.}}$$

$$F_{LL+T} = \frac{1,170(12)}{21,884}(-1) = -0.64 \text{ KSI}$$

Case 1

$$I.R.F. = \frac{0.6f_c (F_t + F_p + F_s)}{F_t}$$

$$I.R.F. = \frac{4.2 (0.26 + 0.65 + 0)}{0.64} = 5.12$$

Case 2

$$I.R.F. = \frac{0.4f_c (-0.5(F_t + F_p + F_s))}{F_t}$$

$$I.R.F. = \frac{2.8 - 0.5(0.26 + 0.65 + 0)}{0.64} = 3.65$$

Negative Flexure

$$I.R.F. = \frac{\phi A_n [-1.3(M)_{DL1} + 1.3(M)_{DL2} + M_s]}{2.17(M)_{LL+T}}$$

$$I.R.F. = \frac{-5,286 - [1.3(0) + 1.3(-475) + 0]}{2.17(-1,170)} = 1.84$$

$$O.R.F. = \frac{\phi A_n [-1.3(M)_{DL1} + 1.3(M)_{DL2} + M_s]}{1.3(M)_{LL+T}}$$

$$O.R.F. = \frac{5,286 [1.3(0) + 1.3(-475) + 0]}{1.3(-1,170)} = -3.07$$

Shear Rating for an interior beam in Span 1 with an Rating Vehicle.

- Applied shear and design data at 0.7L:

$$V_{DL1} = 46 \text{ K}$$

$$V_{DL2} = 13 \text{ K}$$

$$V^*_{LL+T} = 59 \text{ K (live load shear based on one lane)}$$

$$\phi V_n = 233 \text{ K}$$

$$I.L.D.F. = 0.849 \text{ (AASHTO I.RFD live load distributive factor)}$$

- Convert live load shear:

$$V_{LL+T} = I.L.D.F(V^*_{LL+T})$$

$$V_{LL+T} = 0.849(59) = 50 \text{ K}$$

$$I.R.F. = \frac{\phi V_n - [1.3(V)_{DL1} + 1.3(V)_{DL2} + V_s]}{2.17(V)_{LL+T}}$$

$$I.R.F. = \frac{233 - [1.3(46) + 1.3(13) + 0]}{2.17(50)} = 1.45$$

$$O.R.F. = \frac{\phi V_n - [1.3(V)_{DL1} + 1.3(V)_{DL2} + V_s]}{1.3(V)_{LL+T}}$$

$$O.R.F. = \frac{233 [1.3(46) + 1.3(13) + 0]}{1.3(50)} = 2.42$$

- Applied shear and design data at H/2 from Pic 1:

$$V_{DL1} = 108 \text{ K}$$

$$V_{DL2} = 24 \text{ K}$$

$$V^*_{LL+T} = 84 \text{ K (live load shear based on one lane)}$$

$$\phi V_n = 458 \text{ K}$$

LLDF = 0.849 (AASHTO LRFD live load distribution factor)

- Convert live load shear:

$$V_{L+T} = LLDF(V_{LL+T})$$

$$V_{L+T} = 0.849(84) = 71 \text{ K}$$

$$IRF = \frac{\phi V_n}{2.17(V_{LL1})} [1.3(V_{LL1}) + 1.3(V_{LL2}) + V_3]$$

$$IRF = \frac{458 [1.3(108) + 1.3(24) + 0]}{2.17(71)} = 1.86$$

$$ORF = \frac{\phi V_n - [1.3(V_{LL1}) + 1.3(V_{LL2}) + V_3]}{1.3(V_{LL1})}$$

$$ORF = \frac{458 [1.3(108) + 1.3(24) + 0]}{1.3(71)} = 3.10$$

Rating of an exterior beam at 0.5L of Span 1 with an HS20 Rating Vehicle.

- Applied moment, section properties and design data:

M_{DL1} = 3,140 K-FT

M_{DL2} = 340 K-FT

M_{LL+T} = 1,741 K-FT (live load moment based on one lane)

P = 1,208 K (effective prestress after losses)

$S_{flange N.C.}$ = 14,300 IN^3

$S_{b flange N.C.}$ = 15,586 IN^3

$S_{flange Comp.}$ = 49,567 IN^3

$S_{b flange Comp.}$ = 21,644 IN^3

A_{beam} = 908 IN^2

$Ecc.$ = 25.89 IN

f'_c = 7,000 PSI

LLDF = 0.812 (AASHTO LRFD live load distribution factor)

ϕM_n = 11,058 K-FT

- Convert live load moment:

$M_{LL+T} = LLDF(M_{LL+T})$

$M_{LL+T} = 0.812(1,741) = 1,414 \text{ K-FT}$

Concrete Stresses

- Concrete tension (bottom of precast beam)

$$f_t = \frac{M_{DL1}}{S_{flange N.C.}} - \frac{M_{DL2}}{S_{b flange Comp.}}$$

$$f_t = \frac{3,140(12)}{15,586} (-1) + \frac{340(12)}{21,644} (-1) = -2.61 \text{ KSI}$$

$$F_p = P \left[\frac{1}{A_{beam}} - \frac{Ecc.}{S_{b flange N.C.}} \right]$$

$$F_p = 1,208 \left[\frac{1}{908} + \frac{25.89}{15,586} \right] = 3.34 \text{ KSI}$$

$$F_{T+T} = \frac{M_{LL+T}}{S_{b flange Comp.}}$$

$$F_{LL+T} = \frac{1,414(12)}{21,644} (-1) = -0.78 \text{ KSI}$$

$$TRF = \frac{-6\sqrt{f'_c} - (F_d + F_p + F_t)}{F_t}$$

$$IRF = \frac{-6\sqrt{7,000} \left(\frac{1}{1,000} \right) - (-2.61) - 3.34 + 0}{-0.78} = 1.57$$

- Concrete compression (top of precast beam)

$$F_d = \frac{M_{DL1}}{S_{flange N.C.}} + \frac{M_{DL2}}{S_{b flange Comp.}}$$

$$F_d = \frac{3,140(12)}{14,300} + \frac{340(12)}{49,567} = 2.72 \text{ KSI}$$

$$F_p = P \left[\frac{1}{A_{beam}} - \frac{Ecc.}{S_{flange N.C.}} \right]$$

$$F_p = 1,208 \left[\frac{1}{908} - \frac{25.89}{14,300} \right] = -0.86 \text{ KSI}$$

$$F_{T+T} = \frac{M_{LL+T}}{S_{flange Comp.}}$$

$$F_{LL+T} = \frac{1,414(12)}{49,567} = 0.34 \text{ KSI}$$

Case 1

$$IRF = \frac{0.6f'_c - (F_d + F_p + F_t)}{F_t}$$

$$TRF = \frac{4.2 (2.72 - 0.86 + 0)}{0.34} = 6.83$$

Case 2

$$IRF = \frac{0.4f'_c - 0.5(L_d + L_p + L_t)}{F_t}$$

$$TRF = \frac{2.8 (0.5(2.72) - 0.86 + 0)}{0.34} = 5.46$$

Positive Flexure

$$TRF = \frac{\phi M_n - [1.3(M_{DL1}) + 1.3(M_{DL2}) + M_3]}{2.17(M_{LL+T})}$$

$$TRF = \frac{11,058 - [1.3(3,140) + 1.3(340) + 0]}{2.17(1,414)} = 2.13$$

$$ORF = \frac{\phi M_n - [1.3(M_{DL1}) + 1.3(M_{DL2}) + M_3]}{1.3(M_{LL+T})}$$

$$\text{ORF} = \frac{11058 [1.3(3140) + 1.3(340)(0)]}{1.3(1,414)} = 3.55$$

Rating of an exterior beam at Right Bearing (Pier 1) of Span 1 with an HS20 Rating Vehicle.

- Applied moment, section properties and design data:

$$\begin{aligned} M_{DL1} &= 0 \text{ K-FT} \\ M_{DL2} &= -433 \text{ K-FT} \\ M_{LL+T} &= -1,662 \text{ K-FT (live load moment based on one lane)} \\ P &= 303 \text{ K (effective prestress after losses)} \\ S_{\text{flange N.C.}} &= 14,300 \text{ IN}^3 \\ S_{\text{b flange N.C.}} &= 15,586 \text{ IN}^3 \\ S_{\text{flange Comp.}} &= 49,567 \text{ IN}^3 \\ S_{\text{b flange Comp.}} &= 21,644 \text{ IN}^3 \\ A_{\text{beam}} &= 908 \text{ IN}^2 \\ \text{Ecc.} &= 16.38 \text{ IN} \\ f'_c &= 7,000 \text{ PSI} \\ \text{LLDF} &= 0.812 \text{ (AASHTO LRFD live load distribution factor)} \\ \phi M_u &= -4,842 \text{ K-FT} \end{aligned}$$

- Convert live load moment:

$$M_{LL+T} = \text{LLDF}(M_{LL+T})$$

$$M_{LL+T} = 0.812(-1,662) = -1,350 \text{ K-FT}$$

Concrete Stresses

- Concrete tension (top of precast beam)

$$f_t = \frac{M_{DL1}}{S_{\text{flange N.C.}}} + \frac{M_{DL2}}{S_{\text{flange Comp.}}}$$

$$f_t = \frac{0(12)}{14,300} + \frac{-433(12)}{49,567} = -0.10 \text{ KSI}$$

$$f_b = P \left[\frac{1}{A_{\text{beam}}} + \frac{\text{Ecc.}}{S_{\text{flange N.C.}}} \right]$$

$$F_p = 303 \left[\frac{1}{908} + \frac{16.38}{14,300} \right] = 0.01 \text{ KSI}$$

$$F_{LL+T} = \frac{M_{LL+T}}{S_{\text{flange Comp.}}}$$

$$F_{LL+T} = \frac{-1,350(12)}{49,567} = -0.33 \text{ KSI}$$

$$\text{LRFD} = -6\sqrt{f'_c} - (F_p + F_p + F_p) \\ f_t$$

$$\text{TRF} = \frac{-6\sqrt{7,000} \left(\frac{1}{1,000} \right) (-0.10 + 0.01 + 0)}{-0.33} = 1.17$$

- Concrete compression (bottom of precast beam)

$$f_c = \frac{M_{DL1}}{S_{\text{flange N.C.}}} + \frac{M_{DL2}}{S_{\text{flange Comp.}}}$$

$$f_c = \frac{0(12)}{15,586} + \frac{-433(12)}{21,644} = -0.24 \text{ KSI}$$

$$F_p = P \left[\frac{1}{A_{\text{beam}}} + \frac{\text{Ecc.}}{S_{\text{flange N.C.}}} \right]$$

$$F_p = 303 \left[\frac{1}{908} + \frac{16.38}{15,586} \right] = 0.65 \text{ KSI}$$

$$f_{LL+T} = \frac{M_{LL+T}}{S_{\text{flange Comp.}}}$$

$$f_{LL+T} = \frac{-1,350(12)}{21,644} = -0.75 \text{ KSI}$$

Case 1

$$\text{IRF} = \frac{0.6f'_c - (F_t + F_p + F_p)}{f_t}$$

$$\text{TRF} = \frac{4.2 - (0.24 + 0.65 + 0)}{0.75} = 4.42$$

Case 2

$$\text{IRF} = \frac{0.4f'_c - 0.5(f_{t1} + f_{t2} + f_{t3})}{f_t}$$

$$\text{TRF} = \frac{2.8 - 0.5(0.24 + 0.65 + 0)}{0.75} = 3.15$$

Negative Flexure

$$\text{LRFD} = \phi M_u [1.3(M_{DL1} + 1.3(M_{DL2} + M_u)] \\ 2.17(M_{LL+T})$$

$$\text{TRF} = \frac{-4,842 - [1.3(0) + 1.3(-433) + 0]}{2.17(-1,350)} = 1.46$$

$$\text{ORF} = \frac{\phi M_u - [1.3(M_{DL1} + 1.3(M_{DL2} + M_u)] \\ 1.3(M_{LL+T})$$

$$\text{ORF} = \frac{4,842 - [1.3(0) + 1.3(-433) + 0]}{1.3(-1,350)} = 2.44$$

Shear Rating for an exterior beam in Span 1 with an IIS20 Rating Vehicle.

- Applied shear and design data at 0.7L:

$$\begin{aligned} V_{DL1} &= 43 \text{ K} \\ V_{DL2} &= 11 \text{ K} \\ V_{LL+1}^* &= 59 \text{ K (live load shear based on one lane)} \\ \phi V_n &= 232 \text{ K} \\ LLLDF &= 0.812 \text{ (AASHTO LRFD live load distribution factor)} \end{aligned}$$

- Convert live load shear:

$$V_{LL+1} = 0.812(59) = 48 \text{ K}$$

$$IRF = \frac{\phi V_n}{2.17(V_{DL1} + 1.3(V_{DL2} + V_s))} = \frac{232 - [1.3(43) + 1.3(11) + 0]}{2.17(48)} = 1.55$$

$$ORF = \frac{\phi V_n - [1.3(V_{DL1} + 1.3(V_{DL2} + V_s))]}{1.3(V_{LL+1})} = \frac{232 - [1.3(43) + 1.3(11) + 0]}{1.3(48)} = 2.59$$

$$ORF = \frac{232 - [1.3(43) + 1.3(11) + 0]}{1.3(48)} = 2.59$$

- Applied shear and design data at H/2:

$$\begin{aligned} V_{DL1} &= 102 \text{ K} \\ V_{DL2} &= 22 \text{ K} \\ V_{LL+1}^* &= 84 \text{ K (live load shear based on one lane)} \\ \phi V_n &= 447 \text{ K} \\ LLLDF &= 0.812 \text{ (AASHTO LRFD live load distribution factor)} \end{aligned}$$

- Convert live load shear:

$$V_{LL+1} = LLLDF(V_{LL+1}^*)$$

$$V_{LL+1} = 0.812(84) = 68 \text{ K}$$

$$IRF = \frac{\phi V_n}{2.17(V_{DL1} + 1.3(V_{DL2} + V_s))} = \frac{447 - [1.3(102) + 1.3(22) + 0]}{2.17(68)} = 1.94$$

$$ORF = \frac{\phi V_n - [1.3(V_{DL1} + 1.3(V_{DL2} + V_s))]}{1.3(V_{LL+1})} = \frac{447 - [1.3(102) + 1.3(22) + 0]}{1.3(68)} = 3.24$$

$$ORF = \frac{447 - [1.3(102) + 1.3(22) + 0]}{1.3(68)} = 3.24$$